Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)

LiDAR Surveys and Flood Mapping of Himogaan River





University of the Philippines Training Center for Applied Geodesy and Photogrammetry University of the Philippines Cebu

APRIL 2017

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)



© University of the Philippines Diliman and University of the Philippines Cebu 2017

Published by the UP Training Center for Applied Geodesy and Photogrammetry (TCAGP) College of Engineering University of the Philippines – Diliman Quezon City 1101 PHILIPPINES

This research project is supported by the Department of Science and Technology (DOST) as part of its Grants-in-Aid (GIA) Program and is to be cited as:

E.C. Paringit and J.R. Sinogaya (eds.) (2017), LiDAR Surveys and Flood Mapping of Himogaan River, Quezon City: University of the Philippines Training Center on Applied Geodesy and Photogrammetry-159pp.

The text of this information may be copied and distributed for research and educational purposes with proper acknowledgement. While every care is taken to ensure the accuracy of this publication, the UP TCAGP disclaims all responsibility and all liability (including without limitation, liability in negligence) and costs which might incur as a result of the materials in this publication being inaccurate or incomplete in any way and for any reason.

For questions/queries regarding this report, contact:

Jonnifer Sinogaya, PhD.

Project Leader, Phil-LiDAR 1 Program University of the Philippines Cebu Cebu City, Cebu, Philippines 6000 E-mail: jrsinogaya@yahoo.com

Enrico C. Paringit, Dr. Eng.

Program Leader, Phil-LiDAR 1 Program University of the Philippines Diliman Quezon City, Philippines 1101 E-mail: ecparingit@up.edu.ph

National Library of the Philippines ISBN: 978-621-430-105-8

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)

TABLE OF CONTENTS

	···· V
LIST OF TABLES	vii
CHAPTER 1: OVERVIEW OF THE PROGRAM AND HIMOGAAN RIVER	1
1.1 Background of the Phil-LiDAR 1 Program	1
1.2 Overview of the Himogaan River Basin	1
CHAPTER 2: LIDAR ACQUISITION IN HIMOGAAN FLOODPLAIN	3
2.1 Flight Plans	3
2.2 Ground Base Station	5
2.3 Flight Missions	12
2.4 Survey Coverage	13
CHAPTER 3: LIDAR DATA PROCESSING FOR HIMOGAAN FLOODPLAIN	16
3.1 Overview of LiDAR Data Pre-Processing	16
3.2 Transmittal of Acquired LiDAR Data	16
3 3 Trajectory Computation	17
3.4 LiDAR Point Cloud Computation	19
3 5 LiDAR Data Quality Checking	20
3.6 LiDAR Point Cloud Classification and Rasterization	2/
3.7 LiDAR Image Processing and Orthonhotograph Rectification	26
3.7 EDAK Image Processing and Orthophotograph Rectification	20 20
3.0 Mosaicking of Blocks	20
2.10 Calibration and Validation of Mosaicked LiDAR Digital Elevation Model	29
2.11 Integration of Dathymatric Data into the LiDAR Digital Terrain Model	5Z
3.11 Integration of Bathymetric Data into the LIDAR Digital Terrain Model	35
3.12 Fedlure Extraction of Distring Sectors / Dougland	37
3.12.1 Quality Checking of Digitized Features Boundary	37
3.12.2 Height Extraction	37
3.12.3 Feature Attribution	37
3.12.4 Final Quality Checking of Extracted Features	39
CHAPTER 4: DATA VALIDATION SURVEY AND MEASUREMENTS IN THE HIMOGAAN RIVER BASIN	40
4.1 Summary of Activities	40
4.2 Control Survey	41
4.3 Baseline Processing	45
4.4 Network Adjustment	45
4.5 Cross-section, Bridge As-Built, and Water Level Marking	47
4.6 Validation Points Acquisition Survey	52
4.7 Bathymetric Survey	E /
	54
CHAPTER 5: FLOOD MODELING AND MAPPING	54
CHAPTER 5: FLOOD MODELING AND MAPPING	54 58 58
CHAPTER 5: FLOOD MODELING AND MAPPING 5.1 Data Used for Hydrologic Modeling 5.1.1 Hydrometry and Rating Curves	54 58 58
CHAPTER 5: FLOOD MODELING AND MAPPING 5.1 Data Used for Hydrologic Modeling 5.1.1 Hydrometry and Rating Curves 5.1.2 Precipitation	58 58 58 58
CHAPTER 5: FLOOD MODELING AND MAPPING	58 58 58 58 58
CHAPTER 5: FLOOD MODELING AND MAPPING	54 58 58 58 58 58 59 61
CHAPTER 5: FLOOD MODELING AND MAPPING	54 58 58 58 58 59 61 62
CHAPTER 5: FLOOD MODELING AND MAPPING	54 58 58 58 58 59 61 62 66
CHAPTER 5: FLOOD MODELING AND MAPPING	54 58 58 58 58 59 61 62 66 68
CHAPTER 5: FLOOD MODELING AND MAPPING	54 58 58 58 59 61 62 66 68 69
CHAPTER 5: FLOOD MODELING AND MAPPING	54 58 58 58 59 61 62 66 68 69 71
 CHAPTER 5: FLOOD MODELING AND MAPPING 5.1 Data Used for Hydrologic Modeling 5.1.1 Hydrometry and Rating Curves 5.1.2 Precipitation 5.1.3 Rating Curves and River Outflow 5.2 RIDF Station 5.3 HMS Model 5.4 Cross-section Data 5.5 Flo 2D Model 5.6 Results of HMS Calibration 5.7 Calculated outflow hydrographys and discharge values for different Rainfall Return Period 5.7.1 Hydrograph using the Rainfall Runoff Model 	54 58 58 58 59 61 62 66 68 69 71 71
 CHAPTER 5: FLOOD MODELING AND MAPPING 5.1 Data Used for Hydrologic Modeling 5.1.1 Hydrometry and Rating Curves 5.1.2 Precipitation 5.1.3 Rating Curves and River Outflow 5.2 RIDF Station 5.3 HMS Model 5.4 Cross-section Data 5.5 Flo 2D Model 5.6 Results of HMS Calibration 5.7 Calculated outflow hydrographys and discharge values for different Rainfall Return Period 5.7.1 Hydrograph using the Rainfall Runoff Model 5.7.2 Discharge data using Dr. Horritts's recommended hydrologic method 	54 58 58 58 59 61 62 66 68 69 71 71 73
 CHAPTER 5: FLOOD MODELING AND MAPPING 5.1 Data Used for Hydrologic Modeling 5.1.1 Hydrometry and Rating Curves 5.1.2 Precipitation 5.1.3 Rating Curves and River Outflow 5.2 RIDF Station 5.3 HMS Model 5.4 Cross-section Data 5.5 Flo 2D Model 5.6 Results of HMS Calibration 5.7 Calculated outflow hydrographys and discharge values for different Rainfall Return Period 5.7.1 Hydrograph using the Rainfall Runoff Model 5.7.2 Discharge data using Dr. Horritts's recommended hydrologic method 	54 58 58 58 58 59 61 62 66 66 68 69 71 71 73 73
 CHAPTER 5: FLOOD MODELING AND MAPPING	54 58 58 58 59 61 62 66 68 69 71 71 73 77 78
 CHAPTER 5: FLOOD MODELING AND MAPPING 5.1 Data Used for Hydrologic Modeling 5.1.1 Hydrometry and Rating Curves 5.1.2 Precipitation 5.1.3 Rating Curves and River Outflow 5.2 RIDF Station 5.3 HMS Model 5.4 Cross-section Data 5.5 Flo 2D Model 5.6 Results of HMS Calibration 5.7 Calculated outflow hydrographys and discharge values for different Rainfall Return Period 5.7.1 Hydrograph using the Rainfall Runoff Model 5.7.2 Discharge data using Dr. Horritts's recommended hydrologic method 5.5 River Analysis (RAS) Model Simulation 5.6 Flow Depth and Flood Hazard 5.8 Inventory of Areas Exposed to Flooding of Affected Areas 	54 58 58 58 59 61 62 66 68 69 71 71 73 77 78 84
 CHAPTER 5: FLOOD MODELING AND MAPPING 5.1 Data Used for Hydrologic Modeling 5.1.1 Hydrometry and Rating Curves 5.1.2 Precipitation 5.1.3 Rating Curves and River Outflow 5.2 RIDF Station 5.3 HMS Model 5.4 Cross-section Data 5.5 Flo 2D Model 5.6 Results of HMS Calibration 5.7 Calculated outflow hydrographys and discharge values for different Rainfall Return Period 5.7.1 Hydrograph using the Rainfall Runoff Model 5.7.2 Discharge data using Dr. Horritts's recommended hydrologic method 5.5 River Analysis (RAS) Model Simulation 5.6 Flow Depth and Flood Hazard 5.8 Inventory of Areas Exposed to Flooding of Affected Areas 5.9 Flood Validation 	54 58 58 58 59 61 62 66 68 69 71 73 73 77 78 84 91
CHAPTER 5: FLOOD MODELING AND MAPPING	54 58 58 58 59 61 62 66 68 69 71 73 73 77 78 84 91
CHAPTER 5: FLOOD MODELING AND MAPPING 5.1 Data Used for Hydrologic Modeling 5.1.1 Hydrometry and Rating Curves 5.1.2 Precipitation 5.1.3 Rating Curves and River Outflow 5.2 RIDF Station 5.3 HMS Model 5.4 Cross-section Data 5.5 Flo 2D Model 5.6 Results of HMS Calibration 5.7 Calculated outflow hydrographys and discharge values for different Rainfall Return Period 5.7.1 Hydrograph using the Rainfall Runoff Model 5.7.2 Discharge data using Dr. Horritts's recommended hydrologic method. 5.5 River Analysis (RAS) Model Simulation 5.6 Results of Areas Exposed to Flooding of Affected Areas 5.9 Flood Validation REFERENCES	54 58 58 58 59 61 62 66 68 69 71 73 73 73 73 78 84 91 91
CHAPTER 5: FLOOD MODELING AND MAPPING	54 58 58 58 59 61 62 66 68 69 71 71 73 77 78 84 91 91 95
CHAPTER 5: FLOOD MODELING AND MAPPING	54 58 58 58 58 59 61 62 66 68 69 71 73 73 77 78 91 95 95
CHAPTER 5: FLOOD MODELING AND MAPPING 5.1 Data Used for Hydrologic Modeling 5.1.1 Hydrometry and Rating Curves 5.1.2 Precipitation 5.1.3 Rating Curves and River Outflow 5.2 RIDF Station 5.3 HMS Model 5.4 Cross-section Data 5.5 Flo 2D Model 5.6 Results of HMS Calibration 5.7 Calculated outflow hydrographys and discharge values for different Rainfall Return Period 5.7.1 Hydrograph using the Rainfall Runoff Model 5.7.2 Discharge data using Dr. Horritts's recommended hydrologic method 5.5 River Analysis (RAS) Model Simulation 5.6 Flow Depth and Flood Hazard 5.8 Inventory of Areas Exposed to Flooding of Affected Areas 5.9 Flood Validation REFERENCES Annex 1. Optech Technical Specifications Annex 2. NAMRIA Certificates of Reference Points Used Annex 3. Baseling Processing Panoetts	54 58 58 58 59 61 62 66 68 69 71 71 73 73 77 78 91 91 95 95 98
CHAPTER 5: FLOOD MODELING AND MAPPING 5.1 Data Used for Hydrologic Modeling 5.1.1 Hydrometry and Rating Curves 5.1.2 Precipitation 5.1.3 Rating Curves and River Outflow 5.2 RIDF Station 5.3 HMS Model 5.4 Cross-section Data 5.5 Flo 2D Model 5.6 Results of HMS Calibration 5.7 Calculated outflow hydrographys and discharge values for different Rainfall Return Period 5.7.1 Hydrograph using the Rainfall Runoff Model 5.7.2 Discharge data using Dr. Horritts's recommended hydrologic method 5.5 Flove Phand Flood Hazard 5.6 Flow Depth and Flood Hazard 5.8 Inventory of Areas Exposed to Flooding of Affected Areas 5.9 Flood Validation REFERENCES Annex 1. Optech Technical Specifications Annex 2. NAMRIA Certificates of Reference Points Used Annex 3. Baseline Processing Reports.	54 58 58 58 59 61 62 66 68 69 71 71 73 77 78 84 91 91 95 98 102
CHAPTER 5: FLOOD MODELING AND MAPPING 5.1 Data Used for Hydrologic Modeling 5.1.1 Hydrometry and Rating Curves 5.1.2 Precipitation 5.1.3 Rating Curves and River Outflow 5.2 RIDF Station 5.3 HMS Model 5.4 Cross-section Data 5.5 Flo 2D Model 5.6 Results of HMS Calibration 5.7 Calculated outflow hydrographys and discharge values for different Rainfall Return Period 5.7.1 Hydrograph using the Rainfall Runoff Model 5.7.2 Discharge data using Dr. Horritts's recommended hydrologic method. 5.5 River Analysis (RAS) Model Simulation 5.6 Flow Depth and Flood Hazard 5.8 Inventory of Areas Exposed to Flooding of Affected Areas. 5.9 Flood Validation REFERENCES Annex 1. Optech Technical Specifications Annex 2. NAMRIA Certificates of Reference Points Used. Annex 4. The LIDAR Survey Team Composition. Annex 5. Data Trancfer Shoet for Himograpn Elocodalain	54 58 58 58 59 61 62 66 68 69 71 73 71 73 77 78 91 91 95 98 102 104
 CHAPTER 5: FLOOD MODELING AND MAPPING 5.1 Data Used for Hydrologic Modeling 5.1.1 Hydrometry and Rating Curves 5.1.2 Precipitation 5.1.3 Rating Curves and River Outflow 5.2 RIDF Station 5.3 HMS Model 5.4 Cross-section Data 5.5 Flo 2D Model 5.6 Results of HMS Calibration 5.7 Calculated outflow hydrographys and discharge values for different Rainfall Return Period 5.7.1 Hydrograph using the Rainfall Runoff Model 5.7.2 Discharge data using Dr. Horritts's recommended hydrologic method 5.8 River Analysis (RAS) Model Simulation 5.6 Flow Depth and Flood Hazard 5.8 Inventory of Areas Exposed to Flooding of Affected Areas 5.9 Flood Validation REFERENCES Annex 1. Optech Technical Specifications Annex 2. NAMRIA Certificates of Reference Points Used Annex 3. Baseline Processing Reports. Annex 4. The LiDAR Survey Team Composition. 	54 58 58 58 59 61 62 66 68 69 71 73 73 77 78 91 91 95 98 102 104 105

Annex 7. Flight Status	116
Annex 8. Mission Summary Report	125
Annex 9. Himogaan Model Basin Parameters	150
Annex 10. Himogaan Model Reach Parameters	152
Annex 11. Himogaan-Tanao Field Validation	153
Annex 12. Educational Institutions affected in Himogaan-Tanao Floodplain	158
Annex 13. Medical Institutions affected in Himogaan-Tanao Floodplain	158
Annex 14. UPC Phil-LiDAR Team Composition	159

LIST OF FIGURES

Figure 1. Map of the Himogaan river basin (in brown) Figure 2. Flight plan and base stations used for Himogaan floodplain Figure 2. GPS set up over NGW 50 in Saray Negros Occidental (a) NAMPIA	1 4
reference point NGW-50 (b) as recovered by the field team.	6
Figure 4. GPS set-up over NGW-58 in Brgy. Jonobjonob, Sitio Labarca, Escalante,	
Negros Occidental. It is on top of embedded benchmark NW-100.	7
Figure 5. GPS set-up over NGW-63 in Brgy. Lemery, Calatrava, Negros Occidental	
and NAMRIA reference point NGW-63 (b) as recovered by the field team.	8
Figure 6. GPS set-up over CBU-327 in Barangay Poblacion, San Remigio, Cebu, on	
the bridge adjacent to San Remigio Public Cemetery, and NAMRIA reference	
point CBU-327 (b) as recovered by the field team	9
Figure 7. GPS set-up over NW-123 in Cadiz, Negros Occidental going to San Carlos,	
along the national road (a) and NAMRIA reference point NW-123 (b) as recovered	
by the field team	10
Figure 8. GPS set-up over CU-621A in Barangay Tambongan, San Remigio, Cebu	
(a) as CU-621 (b) as recovered by the field team	11
Figure 9. Actual LiDAR data acquisition for Himogaan floodplain.	15
Figure 10. Schematic Diagram for Data Pre-Processing Component	16
Figure 11. Smoothed Performance Metric Parameters of a Himogaan Flight 1431P.	17
Figure 12. Solution Status Parameters of Himogaan Flight 1431P.	18
Figure 13. Best Estimated Trajectory for Himogaan floodplain.	19
Figure 14. Boundary of the processed LiDAR data over Himogaan Floodplain	20
Figure 15. Image of data overlap for Himogaan floodplain	21
Figure 16. Density map of merged LiDAR data for Himogaan floodplain.	22
Figure 17. Elevation difference map between flight lines for Himogaan floodplain	23
Figure 18. Quality checking for a Himogaan flight 1431P using the Profile Tool of QT Modeler	24
Figure 19. Tiles for Himogaan floodplain (a) and classification results (b) in TerraScan	25
Figure 20. Point cloud before (a) and after (b) classification	25
Figure 21. The production of last return DSM (a) and DTM (b), first return DSM (c) and	
secondary DTM (d) in some portion of Himogaan floodplain	26
Figure 22. Himogaan floodplain with available orthophotographs.	27
Figure 23. Sample orthophotograph tiles for Himogaan floodplain	27
Figure 24. Portions in the DTM of Himogaan Floodplain – a paddy field before	
(a) and after (b) data retrieval; bridges before (c) and after (d) manual editing;	
and a road before (e) and after (f) data retrieval	29
Figure 25. Map of Processed LiDAR Data for Himogaan Floodplain	31
Figure 26. Map of Himogaan Flood Plain with validation survey points in green	33
Figure 27. Correlation plot between calibration survey points and LiDAR data	34
Figure 28. Correlation plot between validation survey points and LiDAR data.	35
Figure 29. Map of Himogaan Flood Plain with bathymetric survey points shown in blue	36
Figure 30. QC blocks for Himogaan building features.	37
Figure 31. Extracted features for Himogaan floodplain	39
Figure 32. Himogaan survey extent	41
Figure 33. GNSS Network of Himogaan River Field Survey	42
Figure 34. GNSS base receiver setup, Trimble [®] SPS 852, at NGW-50 in Himogaan Bridge,	
Brgy. Paraiso, Sagay City, Negros Occidental	43
Figure 35. GNSS base receiver setup, Trimble [®] SPS 852, at NW-100 in Danao Bridge,	
Brgy. Jonobjonob, Escalante City, Negros Occidental	44
Figure 36. GNSS base receiver setup, Trimble [®] SPS 852, over NW-130 in Troso Bridge,	
Brgy. Daga, Cadiz City, Negros Occidental	44
Figure 37. (A) Cross-Section Survey and (B) Bridge As-Built survey at Himogaan Bridge	
in Sagay City	47
Figure 38. Location map of Himogaan bridge cross-section	48
Figure 39. Himogaan bridge cross-section diagram	49
Figure 40. Himogaan Bridge Data Form	50
Figure 41. Water Level Mark at the pier of Himogaan Bridge	51
Figure 42. (A) Occupied base station, NGW-50 in Himogaan Bridge, Sagay City and	
(B) Installation of GNSS Receiver Trimble [®] SPS 882 in front of a van	52
Figure 43. LiDAR ground validation survey from Brgy. Poblacion Toboso to Brgy. VI Manapla	53
Figure 44. Set up on a paddle boat for the Bathymetric Survey at the Himogaan	

River upstream	54
Figure 45. Bathymetric points gathered from Himogaan River	55
Figure 46. Riverbed profile of Himogaan River	56
Figure 47. Riverbed profile of Himogaan River	57
Figure 48. Location map of Himogaan HEC-HMS model used for calibration	58
Figure 49. Cross-Section Plot of Himogaan Bridge	59
Figure 50. Rating Curve at Himogaan Bridge, Paraiso, Sagay City	60
Figure 51. Rainfall and outflow data at Himogaan used for modeling	60
Figure 52. Location of Iloilo RIDF station relative to Himogaan River Basin	61
Figure 53. Synthetic storm generated for a 24-hr period rainfall for various return periods	61
Figure 54. Soil map of Himogaan River Basin	63
Figure 55. Land cover map of Himogaan River Basin	64
Figure 56. Slope Map of Himogaan River Basin	65
Figure 57. The Himogaan River Basin model generated using HEC-HMS	66
Figure 58. River cross-section of Himogaan River generated through Arcmap HEC GeoRAS tool	67
Figure 59. Screenshot of subcatchment with the computational area to be modeled	
in FLO-2D GDS Pro	68
Figure 60. Generated 100-year rain return hazard map from FLO-2D Mapper	68
Figure 61. Generated 100-year rain return flow depth map from FLO-2D Mapper	69
Figure 62. Outflow Hydrograph of Himogaan produced by the HEC-HMS model compared	
with observed outflow	69
Figure 63. Outflow hydrograph at Himogaan Station generated using Iloilo RIDF simulated	
in HEC-HMS	72
Figure 64. Himogaan and Tanao river (1) generated discharge using 5-, 25-, and 100-year	
Iloilo and Mactan stations' rainfall intensity-duration-frequency (RIDF) in HEC-HMS	73
Figure 65. Himogaan and Tanao river (2) generated discharge using 5-, 25-, and 100-year	
Iloilo and Mactan stations' rainfall intensity-duration-frequency (RIDF) in HEC-HMS	73
Figure 66. Himogaan and Tanao river (3) generated discharge using 5-, 25-, and 100-year	
Iloilo and Mactan stations' rainfall intensity-duration-frequency (RIDF) in HEC-HMS	74
Figure 67. Himogaan and Tanao river (4) generated discharge using 5-, 25-, and 100-year	
Iloilo and Mactan stations' rainfall intensity-duration-frequency (RIDF) in HEC-HMS	74
Figure 68. Himogaan and Tanao river (5) generated discharge using 5-, 25-, and 100-year	
Iloilo and Mactan stations' rainfall intensity-duration-frequency (RIDF) in HEC-HMS	75
Figure 69. Sample output of Himogaan RAS Model	77
Figure 70. 5-year Flood Hazard Map for Himogaan Floodplain	78
Figure 71. 5-year Flood Depth Map for Himogaan Floodplain	79
Figure 72. 25-year Flood Hazard Map for Himogaan Floodplain	80
Figure 73. 25-year Flow Depth Map for Himogaan Floodplain	81
Figure 74. 100-year Flood Hazard Map for Himogaan Floodplain	82
Figure 75. 100-year Flow Depth Map for Himogaan Floodplain	83
Figure 76. Affected Areas in Cadiz City, Negros Occidental during 5-Year	
Rainfall Return Period	84
Figure 77. Affected Areas in Sagay City, Negros Occidental during 5-Year	
Rainfall Return Period	86
Figure 78. Affected Areas in Cadiz City, Negros Occidental during 25-Year	
Rainfall Return Period	87
Figure 79. Affected Areas in Sagay City, Negros Occidental during 25-Year	
Rainfall Return Period	88
Figure 80. Affected Areas in Cadiz City, Negros Occidental during 100-Year	
Rainfall Return Period	89
Figure 81. Affected Areas in Sagay City, Negros Occidental during 100-Year	
Rainfall Return Period	90
Figure 82. Validation points for 5-year Flood Depth Map of Himogaan Floodplain	92
Figure 83. Flood map depth vs. actual flood depth	92

LIST OF TABLES

Table 1. Flight planning parameters for Aquarius LiDAR system Table 2. Flight planning parameters for Pegasus LiDAR system Table 3. Details of the recovered NAMRIA horizontal control point NGW-50 used as base	. 3 . 3
station for the LiDAR Acquisition.	. 6
Table 4. Details of the recovered NAMRIA horizontal control point NGW-58 used as base	
station for the LiDAR Acquisition Table 5. Details of the recovered NAMRIA horizontal control point NGW-63 used as base	. 7
station for the LiDAR Acquisition.	. 8
Table 6. Details of the recovered NAMRIA horizontal control point CBU-327 used as base station for the LiDAR acquisition	. 9
Table 7. Details of the recovered NAMRIA bench mark point NW-123 with processed	
coordinates used as base station for the LIDAR Acquisition.	10
Table 8. Details of the recovered NAMIRIA benchmark point CU-621 with processed	11
Coordinates used as base station for the LIDAR acquisition	11 12
Table 9. Ground control points used during LIDAR Data Acquisition	12
Table 10. Flight missions for LIDAR data acquisition in filmogaan hoodplain	12
Table 12. List of cities and municipalities covered during Himogaan floodulain survey	1/
Table 12. Self-Calibration Results values for Himograan flights	10
Table 13. Self-Calibration Results values for Himogaan floodplain	20
Table 15. Himogaan classification results in TerraScan	20
Table 16. LiDAR blocks with its corresponding area	24 28
Table 17. Shift Values of each LiDAR Block of Himogaan floodnlain	30
Table 18 Calibration Statistical Measures	34
Table 19. Validation Statistical Measures	35
Table 20. Quality Checking Ratings for Himogaan Building Features.	36
Table 21. Building Features Extracted for Himogaan Floodplain	37
Table 22. Total Length of Extracted Roads for Himogaan Floodplain.	37
Table 23. Number of Extracted Water Bodies for Himogaan Floodplain	37
Table 24. List of references and control points occupied in Himogaan River survey	43
Table 25. Baseline Processing Report for Himogaan River Survey	45
Table 26. Control Point Constraints	46
Table 27. Adjusted Grid Coordinates	46
Table 28. Adjusted Geodetic Coordinates	47
Table 29. Reference and control points used and its location	47
Table 30. RIDF values for Iloilo Rain Gauge computed by PAGASA	61
Table 31. Range of Calibrated Values for Himogaan	70
Table 32. Summary of the Efficiency Test of Himogaan HMS Model	71
Table 33. Peak values of the Himogaan HEC-HMS Model outflow using the Iloilo RIDF	72
Table 34. Summary of Himogaan and Tanao river (1) discharge generated in HEC-HMS	75
Table 35. Summary of Himogaan and Tanao river (2) discharge generated in HEC-HMS	75
Table 36. Smmary of Himogaan and Tanao river (3) discharge generated in HEC-HMS	75
Table 37. Summary of Himogaan and Tanao river (4) discharge generated in HEC-HMS	76
Table 38. Summary of Himogaan and Tanao river (5) discharge generated in HEC-HMS	76
Table 39. Validation of river discharge estimates	76
Table 40. Affected Areas in Cadiz City, Negros Occidental during 5-Year	
Rainfall Return Period	84
Table 41. Affected Areas in Sagay City, Negros Occidental during 5-Year	
Rainfall Return Period	85
Table 42. Affected Areas in Cadiz City, Negros Occidental during 25-Year	
Rainfall Return Period	86
Table 43. Affected Areas in Sagay City, Negros Occidental during 25-Year	
Rainfall Return Period	87
Table 44. Affected Areas in Cadiz City, Negros Occidental during 100-Year	_
Raintall Return Period	88
Table 45. Affected Areas in Sagay City, Negros Occidental during 100-Year	<u> </u>
Rainfall Return Period	90
Table 46. Area covered by each warning level with respect to the rainfall scenario	91
Table 47. Actual Flood Depth vs Simulated Flood Depth in Himogaan	93
Table 48. Summary of Accuracy Assessment in the Himogaan River Basin Survey	93

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)

CHAPTER 1: OVERVIEW OF THE PROGRAM AND HIMOGAAN RIVER

Enrico C. Paringit, Dr. Eng. and Jonnifer Sinogaya, PhD.

1.1 Background of the Phil-LiDAR 1 Program

The University of the Philippines Training Center for Applied Geodesy and Photogrammetry (UP-TCAGP) launched a research program entitled "Nationwide Hazard Mapping using LiDAR" or Phil-LiDAR 1, supported by the Department of Science and Technology (DOST) Grant-in-Aid (GiA) Program. The program was primarily aimed at acquiring a national elevation and resource dataset at sufficient resolution to produce information necessary to support the different phases of disaster management. Particularly, it targeted to operationalize the development of flood hazard models that would produce updated and detailed flood hazard maps for the major river systems in the country.

Also, the program was aimed at producing an up-to-date and detailed national elevation dataset suitable for 1:5,000 scale mapping, with 50 cm and 20 cm horizontal and vertical accuracies, respectively. These accuracies were achieved through the use of the state-of-the-art Light Detection and Ranging (LiDAR) airborne technology procured by the project through DOST.

1.1 Himogaan River Basin

Himogaan River Basin is located in the province of Negros Occidental located at the north of Negros Island. The watershed is traversed by Himogaan River that serves as the main stream of base flow and direct runoff of water within the basin. The location of the Himogaan River Basin is as shown in Figure 1.



Figure 1. Map of the Himogaan river basin (in brown)

The Himogaan River Basin is located in the province of Negros Occidental located at the north of Negros Island. The floodplain and drainage area of 126.41 km2 and 108.31 km2 respectively covers Sagay City and Cadiz City. The DENR RBCO identified it to have an estimated 543 million cubic meter annual run-off with an average terrain elevation above sea level -99 meters.

Its main stem, Himogaan river is part of the river systems in Visayas Region. According to the 2010 census of National Statistics Office, there is a total of 45,991 people residing in the immediate vicinity of the river which is distributed among four (4) barangays, namely: Himogaan Baybay, Tigalawan, Cabahug and Paraiso. Its primary economic activities include sugar cane planting and other related activities to sugar cane production and distribution and fishing in coastal areas. The river also serves as a tourist spot because of its navigable length and depth. The recent flooding events were due to the presence of active low pressure areas that occurred in the whole Western Visayas causing intermittent rains. In 2011, the worst hit was in Sagay City where the floods displaced more than 1, 000 families after the Himogaan River overflowed due to incessant rains. The river once again overflowed in 2012 submerging several houses in Barangay Paraiso

The floodplain is 100% covered with LiDAR data which compromises 5 blocks. The LiDAR data was calibrated then mosaicked with an RMSE of 0.09 and then bathy burned. The bathy survey conducted reached a total length of 15.68 km starting from Fabrica, Sagay City up to the river mouth with 13533 points surveyed. There are 11473 buildings, 317.58km roads, 277 waterbodies and 13 bridges digitized based from the LiDAR data. Feature Extraction Attribution was conducted and among the building features, 11123 of them are Residential, 158 are schools and 5 are Medical Institutions.

The flood hazard map produced covers the 22.18 km2, 25.38 km2, 28 km2 for the 5-year, 25-year, and 100 year rainfall return period in Cadiz City which affects 4 barangays and in Sagay City which affects 8 barangays. A flood depth validation was conducted using 271 randomly generated points which is spread throughout the 6 ranges namely 0m-0.2m, 0.21m-0.5m, 0.51m-1m, 1.01m-2m, 2.10m-5m, 5m+ depth using the 25-yr rainfall flood depth map. It yielded a 0.403m RMSE.

A rating curve was developed at Himogaan Bridge, Sagay City, Negros Occidental, which shows the relationship between the observed water levels at Himogaan Bridge and outflow of the watershed at this location. This rating curve equation, expressed as Q = 66.291e0.5476x, was used to compute the river outflow at Himogaan Bridge for the calibration of the HEC-HMS model. The resulting outflow was used to simulate the flooded areas using HEC-RAS. The simulated model will be an integral part in determining the real-time flood inundation extent of the river after it has been automated and uploaded on the DREAM website.

CHAPTER 2: LIDAR ACQUISITION IN HIMOGAAN FLOODPLAIN

Engr. Louie P. Balicanta, Engr. Christopher Cruz, Lovely Gracia Acuña, Engr. Gerome Hipolito, Ms. Jasmine T. Alviar, and Mr. Darryl M. Austria

2.1 Flight Plans

Plans were made to acquire LiDAR data within the delineated priority area for Himogaan floodplain in Negros Occidental. These missions were planned for 14 lines and ran for at most four and a half (4.5) hours including take-off, landing and turning time. The flight planning parameters for the LiDAR system are found in Table 1 and Table 2. Figure 2 shows the flight plan for Himogaan floodplain.

Block Name	Flying Height (m AGL)	Overlap (%)	Field of View (θ)	Pulse Repe- tition Fre- quency (PRF) (kHz)	Scan Frequency (Hz)	Average Speed (kts)	Average Turn Time (Minutes)
BLK44 A	600	30	36	70	50	120	5
BLK44 E	600	30	36	70	50	120	5
BLK 44 E_ addi- tional	600	30	36	70	50	120	5
BLK44 D	600	30	36	70	50	120	5

Table 1. Flight planning parameters for Aquarius LiDAR system

Table 2. Flight planning parameters for Pegasus LiDAR system

Block Name	Flying Height (m AGL)	Overlap (%)	Field of View (θ)	Pulse Repetition Frequency (PRF) (kHz)	Scan Frequency (Hz)	Average Speed (kts)	Average Turn Time (Minutes)
BLK44 D	1000	30	50	200	30	130	5
BLK44 E	1000	30	50	200	30	130	5
BLK44 F	1000	30	50	200	30	130	5
BLK44 G	1000	30	50	200	30	130	5
Bantayan Island	1200	30	50	200	30	130	5



Figure 2. Flight plan and base stations used for Himogaan floodplain.

2.2 Ground Base Station

The project team was able to recover four(4) NAMRIA reference points: NGW-50, NGW-58, NGW-63, and CBU-327, which are of second (2nd) order accuracy. The team also recovered two (2) benchmarks NW-123 and CU-621. These benchmarks were used as vertical reference points and were also established as ground control points. The certification for the NAMRIA reference points and benchmarks are found in Annex 2 while the baseline processing reports for the established control points are found in Annex 3. These were used as base stations during flight operations for the entire duration of the survey (April to July 2014 and April 2016). Base stations were observed using dual frequency GPS receivers, TRIMBLE SPS 852 and SPS 985. Flight plans and location of base stations used during the aerial LiDAR acquisition in Himogaan floodplain are shown in Figure 2.

Figure 3 to Figure 8 shows the recovered NAMRIA control station within the area. In addition, Table 3 to Table 8 show the details about the following NAMRIA control stations and established points, while Table 9 shows the list of all ground control points occupied during the acquisition with the corresponding dates of utilization.



Figure 3. GPS set-up over NGW-50 in Sagay, Negros Occidental (a) NAMRIA reference point NGW-50 (b) as recovered by the field team.

Table 3. Details of the recovered NAMRIA horizontal control point NGW-50 used as base station for the
LiDAR Acquisition.

Station Name	NGW-50		
Order of Accuracy	2 nd		
Relative Error (Horizontal Positioning)	1 in 50,000		
Geographic Coordinates, Philippine Refer- ence of 1992 Datum (PRS 92)	Latitude Longitude Ellipsoidal Height	10° 53' 26.84456" 123° 21' 06.66798" 15.386 meters	
Grid Coordinates, Philippine Transverse Mer-	Easting	538465.927 m	
cator Zone 5 (PTM Zone 5 PRS 92)	Northing	1204272.594 m	
Geographic Coordinates, World Geodetic System 1984 Datum (WGS 84)	Latitude Longitude Ellipsoidal Height	10° 53' 26.84456" North 123° 21' 06.66798" East 15.386 meters	
Grid Coordinates, Universal Transverse Mer-	Easting	538452.463 meters	
cator Zone 51 North (UTM 51N PRS 1992)	Northing	1203851.077 meters	



Figure 4. GPS set-up over NGW-58 in Brgy. Jonobjonob, Sitio Labarca, Escalante, Negros Occidental. It is on top of embedded benchmark NW-100.

Table 4. Details of the recovered NAMRIA horizontal control point NGW-58 used as base station for the
LiDAR Acquisition.

Station Name	NG	GW-58		
Order of Accuracy	2 nd			
Relative Error (horizontal positioning)	1 in 50,000			
Geographic Coordinates, Philippine Ref- erence of 1992 Datum (PRS 92)	Latitude Longitude Ellipsoidal Height	10° 49′ 16.43235″ 123° 29′ 11.51295″ 8.72200 m		
Grid Coordinates, PTM	Easting Northing	553202.195 m 1196599.363 m		
Geographic Coordinates, World Geodetic System 1984 Datum (WGS 84)	Latitude Longitude Ellipsoidal Height	10° 49′ 12.14178″ 123° 29′ 16.71871″ 68.25600 m		
Grid Coordinates, Universal Transverse Mercator Zone 51 North (UTM 51N PRS 1992)	Easting Northing	553,183.57 1,196,180.53		



Figure 5. GPS set-up over NGW-63 in Brgy. Lemery, Calatrava, Negros Occidental and NAMRIA reference point NGW-63 (b) as recovered by the field team.

Table 5. Details of the recovered NAMRIA horizontal control point NGW-63 used as base station for the
LiDAR Acquisition.

Station Name	NGV	V-63
Order of Accuracy	2r	nd
Relative Error (horizontal positioning)	1 in 5	0,000
Geographic Coordinates, Philippine Reference of 1992 Datum (PRS 92)	Latitude Longitude Ellipsoidal Height	10° 38′ 30.18023″ 123° 29′ 18.57332″ 10.15500 m
Grid Coordinates, Philippine Transverse Mercator Zone 5 (PTM Zone 5 PRS 92)	Easting Northing	553448.18 m 1176744.618 m
Geographic Coordinates, World Geodetic System 1984 Datum (WGS 84)	Latitude Longitude Ellipsoidal Height	10° 38′ 25.93535″ 123° 29′ 23.79491″ 70.11800 m
Grid Coordinates, Universal Transverse Mercator Zone 51 North (UTM 51N PRS 1992)	Easting Northing	553429.47 m 1176332.74 m



Figure 6. GPS set-up over CBU-327 in Barangay Poblacion, San Remigio, Cebu, on the bridge adjacent to San Remigio Public Cemetery, and NAMRIA reference point CBU-327 (b) as recovered by the field team.

Table 6. Details of the recovered NAMRIA horizontal control point CBU-327 used as base station for the
LiDAR acquisition.

Station Name	(CBU-327
Order of Accuracy		2nd
Relative Error (horizontal positioning)	1	in 50,000
Geographic Coordinates, Philippine Reference of 1992 Datum (PRS 92)	Latitude Longitude Ellipsoidal Height	11° 4′ 30.20546″ 123° 56′ 10.33433″ 3.541 m
Grid Coordinates, Philippine Transverse Merca- tor Zone 5 (PTM Zone 5 PRS 92)	Easting Northing	602289.857 m 1224791.193 m
Geographic Coordinates, World Geodetic Sys- tem 1984 Datum (WGS 84)	Latitude Longitude Ellipsoidal Height	11° 4′ 25.88934″ 123° 56′ 15.51412″ 63.574 m
Grid Coordinates, Universal Transverse Merca- tor Zone 51 North (UTM 51N PRS 1992)	Easting Northing	602254.06 m 1224362.49 m



- (a)
- Figure 7. GPS set-up over NW-123 in Cadiz, Negros Occidental going to San Carlos, along the national road (a) and NAMRIA reference point NW-123 (b) as recovered by the field team.

Table 7. Details of the recovered	NAMRIA bench ma	ark point NW-123 wi	th processed	coordinates used	as
	base station for th	e LiDAR Acquisition.			

Station Name	NW-123		
Order of Accuracy	2 nd		
Relative Error (Horizontal Positioning)	1	in 50,000	
Geographic Coordinates, Philippine Refer- ence of 1992 Datum (PRS 92)	Latitude Longitude Ellipsoidal Height	10° 54' 55.44193" 123° 19' 39.85851" 29.402 meters	
Geographic Coordinates, World Geodetic System 1984 Datum (WGS 84)	Latitude Longitude Ellipsoidal Height	10° 54' 51.11386" North 123° 19' 45.05716" East 88.320 meters	
Grid Coordinates, Universal Transverse Mer- cator Zone 51 North (UTM 51N PRS 1992)	Easting Northing	535814.201 meters 1206569.167 meters	



Figure 8. GPS set-up over CU-621A in Barangay Tambongan, San Remigio, Cebu (a) as CU-621 (b) as recovered by the field team.

Table 8. Details of the recovered NAMRIA benchmark point CU-621 with processed coordinates used asbase station for the LiDAR acquisition.

Station Name	C	CU-621A
Order of Accuracy		2 nd
Relative Error (Horizontal Positioning)	1	in 50,000
Geographic Coordinates, Philippine Reference of 1992 Datum (PRS 92)	Latitude Longitude Ellipsoidal Height	11° 01′ 11.40721″ 123° 55′ 20.28470″ 15.65695 meters
Geographic Coordinates, World Geodetic System 1984 Datum (WGS 84)	Latitude Longitude Ellipsoidal Height	11° 01′ 07.10388″ North 123° 55′ 25.46947″ East 75.791 meters
Grid Coordinates, Universal Transverse Mercator Zone 51 North (UTM 51N PRS 1992)	Easting Northing	600754.2895 meters 1218251.478 meters

Date Surveyed	Flight Number	Mission Name	Ground Control Points
May 1, 2014	1411P	1BLK44D121A	NGW-50 and NGW-58
May 6, 2014	1431P	1BLK44GHS126A	NGW-58 and NGW-63
May 6, 2014	1433P	1BLK44FGS126B	NGW-58 and NGW-63
May 7, 2014	1435P	1BLK44DS127A	NGW-58 and NGW-63
July 23, 2014	1745P	1BTYN204A	CBU-327 and CU-621A
April 22, 2016	8453AC	3BLK44AS113A	NGW-50 and NW-123
April 23, 2016	8455AC	3BLK44AS114A	NGW-50 and NW-123
April 24, 2016	8457AC	3BLK44EDS115A	NGW-50 and NW-123

Table 9. Ground control points used during LiDAR Data Acquisition

2.3 Flight Missions

Eight (8) missions were conducted to complete LiDAR data acquisition in Himogaan floodplain, for a total of 33 hours and 3 minutes (33+3) of flying time for RP-C9022 and RP-C9322. All missions were acquired using the Aquarius and Pegasus LiDAR systems. Table 10 shows the total area of actual coverage and the corresponding flying hours per mission, while Table 11 presents the actual parameters used during the LiDAR data acquisition.

Date Sur- Flight		Flight Plan Area	Surveyed	ed within the	Area Sur- veyed Outside the	No. of Images	Flying Hours	
veyed	Number	(km²)	Area (km²)	Floodplain (km²)	Floodplain (km²)	(Frames)	Ŧ	Min
May 1, 2014	1411P	584.55	358.76	60.75	298.01	519	3	47
May 6, 2014	1431P	501.27	217.96	0	217.96	727	4	21
May 6, 2014	1433P	341.79	199.15	4.65	194.5	973	4	29
May 7, 2014	1435P	843.06	303.80	27.01	276.79	NA	4	53
July 23, 2014	1745P	153.44	180.65	0	180.65	762	3	36
April 22, 2016	8453AC	108.13	103.85	30.64	73.21	NA	4	11
April 23, 2016	8455AC	35.96	60.01	11.51	48.5	NA	3	53
April 24, 2016	8457AC	53.08	64.14	3.65	60.49	NA	3	53
Tot	al	2621.28	1488.32	138.21	1350.11	2981	33	3

Table 10. Flight missions for LiDAR data acquisition in Himogaan floodplain.

Flight Number	Flying Height (m AGL)	Overlap (%)	FOV (θ)	PRF (kHz)	Scan Fre- quency (Hz)	Average Speed (kts)	Average Turn Time (Min- utes)
1411P	1200	25	50	200	30	130	5
1431P	800	25	50	200	30	130	5
1433P	800	25	50	200	30	130	5
1435P	800	25	50	200	30	130	5
1745P	1200	30	50	200	30	130	5
8453AC	500	30	36	50	45	125	5
8455AC	500	30	36	50	45	125	5
8457AC	500	60	40	50	40	125	5

Table 11. Actual parameters used during LiDAR data acquisition

2.4 Survey Coverage

Himogaan floodplain is located in the province of Negros Occidental with majority of the floodplain situated within the cities of Sagay and Cadiz. Sagay and Escalante in Negros Occidental, and Bantayan and Madridejos in Cebu are mostly covered by the survey. The list of municipalities and cities surveyed, with at least one (1) square kilometer coverage, is shown in Table 12. The actual coverage of the LiDAR acquisition for Himogaan floodplain is presented in Figure 9.

Province	Municipality/City	Area of Municipality/City	Total Area Surveyed	Percentage of Area Surveyed
		internet party, city	Surveyeu	(%)
	Sagay	304.62	283.92	93.2
	Cadiz	516.18	246.32	47.72
	Escalante	193.4	155.38	80.34
Negros Occidental	Calatrava	344.54	139.66	40.54
	Toboso	118.52	79.12	66.76
	San Carlos	408.97	33.06	8.08
	Manapla	99.18	4.56	4.6
	Bantayan	82.8	74.6	90.1
Cebu	Madridejos	24.33	24.31	99.92
	Santa Fe	32.23	22.85	70.9

Table 12. List of cities and municipalities covered during Himogaan floodplain survey



Figure 9. Actual LiDAR data acquisition for Himogaan floodplain.

CHAPTER 3: LIDAR DATA PROCESSING FOR HIMOGAAN FLOODPLAIN

Engr. Ma. Rosario Concepcion O. Ang, Engr. John Louie D. Fabila, Engr. Sarah Jane D. Samalburo , Engr. Gladys Mae Apat , Engr. Joida F. Prieto , Engr. Ma. Ailyn L. Olanda, Engr. Justine Y. Francisco, Eng. Czarina Jean P. Añonuevo , Franklin D. Maraya, and Chester B. de Guzman

3.1 Overview of LiDAR Data Pre-Processing



Figure 10. Schematic Diagram for Data Pre-Processing Component

The data transmitted by the Data Acquisition Component are checked for completeness based on the list of raw files required to proceed with the pre-processing of the LiDAR data. Upon acceptance of the LiDAR field data, georeferencing of the flight trajectory done in order to obtain the exact location of the LiDAR sensor when the laser was shot. Point cloud georectification is performed to incorporate correct position and orientation for each point acquired. The georectifiedLiDAR point clouds are subject for quality checking to ensure that the required accuracies of the program, which are the minimum point density, vertical and horizontal accuracies, are met. The point clouds are then classified into various classes before generating Digital Elevation Models such as Digital Terrain Model and Digital Surface Model.

Using the elevation of points gathered in the field, the LiDAR-derived digital models are calibrated. Portions of the river that are barely penetrated by the LiDAR system are replaced by the actual river geometry measured from the field by the Data Validation and Bathymetry Component. LiDAR acquired temporally are then mosaicked to completely cover the target river systems in the Philippines. Orthorectification of images acquired simultaneously with the LiDAR data is done through the help of the georectified point clouds and the metadata containing the time the image was captured.

These processes are summarized in the flowchart shown in Figure 10.

3.2 Transmittal of Acquired LiDAR Data

Data transfer sheets for all the LiDAR missions for Himogaan floodplain can be found in Annex 5. Missions flown during the first survey conducted on May 2014 used the Airborne LiDAR Terrain Mapper (ALTM[™] Optech Inc.) Pegasus system while missions acquired during the second survey on May2016 were flown

using the Aquarius system over Sagay, Negros Occidental. The Data Acquisition Component (DAC) transferred a total of 135.84 Gigabytes of Range data, 1.73 Gigabytes of POS data, 326.78 Megabytes of GPS base station data, and 219.9 Gigabytes of raw image data to the data server on May 19, 2014 for the first survey and May 18, 2016 for the second survey. The Data Pre-processing Component (DPPC) verified the completeness of the transferred data. The whole dataset for Himogaan was fully transferred on May 20, 2016, as indicated on the Data Transfer Sheets for Himogaan floodplain.

3.3 Trajectory Computation

The Smoothed Performance Metrics of the computed trajectory for flight 1431P, one of the Himogaan flights, which is the North, East, and Down position RMSE values are shown in Figure 11. The x-axis corresponds to the time of flight, which is measured by the number of seconds from the midnight of the start of the GPS week, which on that week fell on May 06, 2014 00:00AM. The y-axis is the RMSE value for that particular position.



Figure 11. Smoothed Performance Metrics of a Himogaan Flight 1431P.

The time of flight was from 176000 seconds to 187500 seconds, which corresponds to morning of May 06, 2014. The initial spike that is seen on the data corresponds to the time that the aircraft was getting into position to start the acquisition, and the POS system starts computing for the position and orientation of the aircraft. Redundant measurements from the POS system quickly minimized the RMSE value of the positions. The periodic increase in RMSE values from an otherwise smoothly curving RMSE values correspond to the turn-around period of the aircraft, when the aircraft makes a turn to start a new flight line. Figure 11 shows that the North position RMSE peaks at 1.30 centimeters, the East position RMSE peaks at 1. 80 centimeters, and the Down position RMSE peaks at 2.90 centimeters, which are within the prescribed accuracies described in the methodology.



Figure 12. Solution Status Parameters of Himogaan Flight 1431P.

The Solution Status parameters of flight 1431P, one of the Himogaan flights, which are the number of GPS satellites, Positional Dilution of Precision (PDOP), and the GPS processing mode used, are shown in Figure 12. The graphs indicate that the number of satellites during the acquisition did not go down to 5. Majority of the time, the number of satellites tracked was between 5 and 9. The PDOP value also did not go above the value of 3, which indicates optimal GPS geometry. The processing mode stayed at the value of 0 for majority of the survey with some peaks up to 1 attributed to the turns performed by the aircraft. The value of 0 corresponds to a Fixed, Narrow-Lane mode, which is the optimum carrier-cycle integer ambiguity resolution technique available for POSPAC MMS. All of the parameters adhered to the accuracy requirements for optimal trajectory solutions, as indicated in the methodology. The computed best estimated trajectory for all Himogaan flights is shown in Figure 13.



Figure 13. Best Estimated Trajectory for Himogaan floodplain.

3.4 LiDAR Point Cloud Computation

The produced LAS data contains 115 flight lines, the flight lines from Aquarius system contain one channel, while the flight lines from the Pegasus system contain two channels. The summary of the self-calibration results obtained from LiDAR processing in LiDAR Mapping Suite (LMS) software for all flights over Himogaan floodplain are given in Table 13.

	v v	
Parameter	Acceptable Value	Acceptable Value
Boresight Correction stdev	(<0.001degrees)	0.000218
IMU Attitude Correction Roll and Pitch Corrections stdev	(<0.001degrees)	0.000903
GPS Position Z-correction stdev	(<0.01meters)	0.0027

Table 13. Self-Calibration Results values for Himogaan flights.

The optimum accuracy is obtained for all Himogaan flights based on the computed standard deviations of the orientation parameters. Standard deviation values for individual blocks are available in Annex 8. Mission Summary Reports.

3.5 LiDAR Data Quality Checking

The boundary of the processed LiDAR data on top of a SAR Elevation Data over Himogaan Floodplain is shown in Figure 14. The map shows gaps in the LiDAR coverage that are attributed to cloud coverage.



Figure 14. Boundary of the processed LiDAR data over Himogaan Floodplain

The total area covered by the Himogaan missions is 936.05 sq.km that is comprised of seven (7) flight acquisitions grouped and merged into five (5) blocks as shown in Table 14.

LiDAR Blocks	Flight Numbers	Area (sq.km)	
Negros PIKAAD	1411P	475.0	
Negros_bik44D	1435P	475.2	
Nogros Plk44EC	1431P	7 2 2 2	
Negros_bik44FG	1431P	205.7	
Bacolod_Blk44E	8453AC	101.6	
Bacolod_Blk44E_additional	8455AC	54.26	
Bacolod_Blk44D	8457AC	15.29	
TOTAL	930.05 sq.km		

Table 14. List of LiDAR blocks for Himogaan floodplain.

The overlap data for the merged LiDAR blocks, showing the number of channels that pass through a particular location is shown in Figure 15. Since Aquarius system employs one channel, we would expect an average value of 1 (blue) for areas where there is limited overlap, and a value of 2 (yellow) or more (red) for areas with three or more overlapping flight lines. On the other hand, the Pegasus system employs two channels, the average value of 2 (blue) for areas where there is limited overlap, and a value of 3 (yellow) or more (red) for areas with three or more overlapping flight lines.



Figure 15. Image of data overlap for Himogaan floodplain.

The overlap statistics per block for the Himogaan floodplain can be found in Annex 8. One pixel corresponds to 25.0 square meters on the ground. For this area, the minimum and maximum percent overlaps are 27.44% and 47.40% respectively, which passed the 25% requirement.

The pulse density map for the merged LiDAR data, with the red parts showing the portions of the data that satisfy the 2 points per square meter criterion is shown in Figure 16. It was determined that all LiDAR data for Himogaan floodplain satisfy the point density requirement, and the average density for the entire survey area is 3.74 points per square meter.



Figure 16. Pulse density map of merged LiDAR data for Himogaan floodplain.

The elevation difference between overlaps of adjacent flight lines is shown in Figure 17. The default color range is from blue to red, where bright blue areas correspond to portions where elevations of a previous flight line, identified by its acquisition time, are higher by more than 0.20m relative to elevations of its adjacent flight line. Bright red areas indicate portions where elevations of a previous flight line are lower by more than 0.20m relative to elevations of its adjacent flight line. Areas with bright red or bright blue need to be investigated further using Quick Terrain Modeler software.



Figure 17. Elevation difference map between flight lines for Himogaan floodplain.

A screen capture of the processed LAS data from a Himogaan flight 1431P loaded in QT Modeler is shown in Figure 18. The upper left image shows the elevations of the points from two overlapping flight strips traversed by the profile, illustrated by a dashed yellow line. The x-axis corresponds to the length of the profile. It is evident that there are differences in elevation, but the differences do not exceed the 20-centimeter mark. This profiling was repeated until the quality of the LiDAR data becomes satisfactory. No reprocessing was done for this LiDAR dataset.



Figure 18. Quality checking for a Himogaan flight 1431P using the Profile Tool of QT Modeler.

3.6 LiDAR Point Cloud Classification and Rasterization

Pertinent Class	Total Number of Points
Ground	1,160,881,260
Low Vegetation	1,145,108,649
Medium Vegetation	1,776,503,683
High Vegetation	544,946,392
Building	33,829,606

Table 15. Himogaan classification results in TerraScan.

The tile system that TerraScan employed for the LiDAR data and the final classification image for a block in Himogaan floodplain is shown in Figure 21. A total of 1,456 1km by 1km tiles were produced. The number of points classified to the pertinent categories is illustrated in Table 15. The point cloud has a maximum and minimum height of 584.11 meters and 50.48 meters respectively.



Figure 19. Tiles for Himogaan floodplain (a) and classification results (b) in TerraScan.

An isometric view of an area before and after running the classification routines is shown in Figure 20. The ground points are in orange, the vegetation is in different shades of green, and the buildings are in cyan. It can be seen that residential structures adjacent or even below canopy are classified correctly, due to the density of the LiDAR data.



Figure 20. Point cloud before (a) and after (b) classification.

The production of last return (V_ASCII) and the secondary (T_ASCII) DTM, first (S_ASCII) and last (D_ASCII) return DSM of the area in top view display are shown in Figure 23. It shows that DTMs are the representation of the bare earth while on the DSMs, all features are present such as buildings and vegetation.



Figure 21. The production of last return DSM (a) and DTM (b), first return DSM (c) and secondary DTM (d) in some portion of Himogaan floodplain.

3.7 LiDAR Image Processing and Orthophotograph Rectification

The 685 1km by 1km tiles area covered by Himogaan floodplain is shown in Figure 22. After tie point selection to fix photo misalignments, color points were added to smoothen out visual inconsistencies along the seamlines where photos overlap. The Himogaan floodplain has a total of 528.31 sq.km orthophotogaph coverage comprised of 1,248 images. A zoomed in version of sample orthophotographs named in reference to its tile number is shown in Figure 23.


Figure 22. Himogaan floodplain with available orthophotographs.



Figure 23. Sample orthophotograph tiles for Himogaan floodplain.

3.8 DEM Editing and Hydro-Correction

Five (5) mission blocks were processed for Himogaan flood plain. These blocks are composed of Negros and Bacolod blocks with a total area of 930.05 square kilometers. Table 16 shows the name and corresponding area of each block in square kilometers.

LiDAR Blocks	Area (sq.km)
Negros_Blk44D	475.20
Negros_Blk44FG	283.70
Bacolod_Blk44D	15.29
Bacolod_Blk44E	101.6
Bacolod_Blk44E_additional	54.26
TOTAL	930.05 sq.km

Table 16. LiDAR blocks with its corresponding area.

Portions of DTM before and after manual editing are shown in Figure 24. It shows that the paddy field (Figure 24a) has been misclassified and removed during classification process and has to be retrieved to complete the surface (Figure 24b). The bridges (Figure 24c) would be an impedance to the flow of water along the river and have to be removed (Figure 24d) in order to hydrologically correct the river. Another example is a road that has been misclassified (Figure 24e) and has to be retrieved through manual editing (Figure 24f).



Figure 24. Portions in the DTM of Himogaan Floodplain – a paddy field before (a) and after (b) data retrieval; bridges before (c) and after (d) manual editing; and a road before (e) and after (f) data retrieval

3.9 Mosaicking of Blocks

Negros_Blk44AB was used as the reference block at the start of mosaicking because it was referred to a base station with an acceptable order of accuracy. Table 17 shows the area of each LiDAR block and the shift values applied during mosaicking.

Mosaicked LiDAR DTM for Himogaan floodplain is shown in Figure 25. It can be seen that the entire Himogaan floodplain is 100% covered by LiDAR data.

Mission Blacks	Shift Values (meters)				
WISSION BIOCKS	x	У	z		
Negros_Blk44D	0.00	0.00	0.66		
Negros_Blk44FG	0.00	0.00	0.57		
Bacolod_Blk44D	0.00	0.00	1.66		
Bacolod_Blk44E	0.00	0.00	1.39		
Bacolod_Blk44E_additional	0.00	0.00	1.45		

Table 17. Shift Values of each LiDAR Block of Himogaan floodplain.



Figure 25. Map of Processed LiDAR Data for Himogaan Floodplain.

3.10 Calibration and Validation of Mosaicked LiDAR Digital Elevation Model

The extent of the validation survey done by the Data Validation and Bathymetry Component (DVBC) in the Negros Island to collect points with which the LiDAR dataset is validated is shown in Figure 26. A total of 39,705 points were gathered for all the floodplains within the Negros Island wherein the Himogaan is located. Random selection of 80% of the survey points, resulting to 31,385 points, were used for calibration.

A good correlation between the uncalibrated mosaicked LiDAR elevation values and the ground survey elevation values is shown in Figure 27. Statistical values were computed from extracted LiDAR values using the selected points to assess the quality of data and obtain the value for vertical adjustment. The computed height difference between the LiDAR DTM and calibration elevation values is 0.94 meters with a standard deviation of 0.15 meters. Calibration of Himogaan LiDAR data was done by subtracting the height difference value, 0.94 meters, to the mosaicked LiDAR data for Himogaan. Table 18 shows the statistical values of the compared elevation values between LiDAR data and calibration data.



Figure 26. Map of Himogaan Flood Plain with validation survey points in green.



Figure 27. Correlation plot between calibration survey points and LiDAR data.

Calibration Statistical Measures	Value (meters)
Height Difference	0.94
Standard Deviation	0.15
Average	-0.93
Minimum	-1.21
Maximum	0.89

Table 18. Calibration Statistical Measures.

A total of 270 survey points that are within Himogaan flood plain were used for the validation of the calibrated Himogaan DTM. A good correlation between the calibrated mosaicked LiDAR elevation values and the ground survey elevation, which reflects the quality of the LiDAR DTM is shown in Figure 28. The computed RMSE between the calibrated LiDAR DTM and validation elevation values is 0.08 meters with a standard deviation of 0.08 meters, as shown in Table 19.



Figure 28. Correlation plot between validation survey points and LiDAR data.

Validation Statistical Measures	Value (meters)
RMSE	0.08
Standard Deviation	0.08
Average	-0.001
Minimum	-0.18
Maximum	0.31

Table 19. Validation	Statistical	Measures
----------------------	-------------	----------

3.11 Integration of Bathymetric Data into the LiDAR Digital Terrain Model

For bathy integration, only centerline data was available for Himogaan with 13,533 bathymetric survey points. The resulting raster surface produced was done by Inverse Distance Weighted (IDW) interpolation method. After burning the bathymetric data to the calibrated DTM, assessment of the interpolated surface is represented by the computed RMSE value of 0.07 meters. The extent of the bathymetric survey done by the Data Validation and Bathymetry Component (DVBC) in Himogaan integrated with the processed LiDAR DEM is shown in Figure 29.



Figure 29. Map of Himogaan Flood Plain with bathymetric survey points shown in blue.

3.12 Feature Extraction

The features salient in flood hazard exposure analysis include buildings, road networks, bridges and water bodies within the floodplain area with 200 m buffer zone. Mosaicked LiDAR DEM with 1 m resolution was used to delineate footprints of building features, which consist of residential buildings, government offices, medical facilities, religious institutions, and commercial establishments, among others. Road networks comprise of main thoroughfares such as highways and municipal and barangay roads essential for routing of disaster response efforts. These features are represented by a network of road centerlines.

3.12.1 Quality Checking of Digitized Features' Boundary

Himogaan floodplain, including its 200 m buffer, has a total area of 120.29sq km. For this area, a total of 5.0 sq km, corresponding to a total of 1389 building features, are considered for QC. Figure 30 shows the QC blocks for Himogaan floodplain.



Figure 30. QC blocks for Himogaan building features.

Quality checking of Himogaan building features resulted in the ratings shown in Table 20.

			-	
FLOODPLAIN	COMPLETENESS	CORRECTNESS	QUALITY	REMARKS
Himogaan	100.00	100.00	97.98	PASSED

Table 20	Our liter	Charling	Dationa	for lline or one	Duilding C	+···
Table 70.	OUAIIIV	CUECKINE	Rannes	tor Himogaan	BUILDING F	Partires
	Quanty	encerning.		ioi i iiiiogaan	Banangi	catarcor

3.12.2 Height Extraction

Height extraction was done for 12,011 building features in Himogaan floodplain. Of these building features, 538 was filtered out after height extraction, resulting to 11473 buildings with height attributes. The lowest building height is at 2.0 m, while the highest building is at 17.05 m.

3.12.3 Feature Attribution

The feature attribution survey was conducted through a participatory community-based mapping in coordination with the Local Government Units of the Municipality/City. The research associates of Phil-LiDAR 1 team visited local barangay units and interviewed key local personnel and officials who possessed expert knowledge of their local environments to identify and map out features.

Maps were displayed on a laptop and were presented to the interviewees for identification. The displayed map include the orthophotographs, Digital Surface Models, existing landmarks, and extracted feature shapefiles. Physical surveys of the barangay were also done by the Phil-LiDAR 1 team every after interview for validation. The number of days by which the survey was conducted was dependent on the number of features and number of barangays included in the flood plain of the river basin.

Table 21 summarizes the number of building features per type. On the other hand, Table 22 shows the total length of each road type, while Table 23 shows the number of water features extracted per type.

	<u> </u>
Facility Type	No. of Features
Residential	11,123
School	158
Market	3
Agricultural/Agro-Industrial Facilities	11
Medical Institutions	5
Barangay Hall	6
Military Institution	0
Sports Center/Gymnasium/Covered Court	5
Telecommunication Facilities	4
Transport Terminal	3
Warehouse	1
Power Plant/Substation	0
NGO/CSO Offices	1
Police Station	0
Water Supply/Sewerage	0
Religious Institutions	26
Bank	1
Factory	56
Gas Station	1
Fire Station	0
Other Government Offices	13
Other Commercial Establishments	54
N/A	2
Total	11,473

Table 21. Building Features Extracted for Himogaan Floodplain.

Table 22. Total Length of Extracted Roads for Himogaan Floodplain.

Road Network Length (km)						
Floodplain	Barangay Road	City/Municipal Road	Provincial Road	National Road	Others	Total
Himogaan	385.87	0.00	0.00	16.33	11.12	413.32

Table 23. Number of Extracted Water Bodies for Himogaan Floodplain.

	Water Body Type					
Floodplain	Rivers/ Streams	Lakes/ Ponds	Sea	Dam	Fish Pen	Total
Himogaan	20	0	0	0	257	277

A total of 13 bridges and culverts over small channels that are part of the river network were also extracted for the floodplain.

3.12.4 Final Quality Checking of Extracted Features

All extracted ground features were completely given the required attributes. All these output features comprise the flood hazard exposure database for the floodplain. This completes the feature extraction phase of the project.



Figure 31 shows the Digital Surface Model (DSM) of Himogaan floodplain overlaid with its ground features.

Figure 31. Extracted features for Himogaan floodplain.

CHAPTER 4: DATA VALIDATION SURVEY AND MEASUREMENTS IN THE HIMOGAAN RIVER BASIN

Engr. Louie P. Balicanta, Engr. Joemarie S. Caballero, Ms. Patrizcia Mae. P. dela Cruz, Engr. Dexter T. Lozano For. Dona Rina Patricia C. Tajora, Elaine Bennet Salvador, and For. Rodel C. Alberto

4.1 Summary of Activities

The Data Validation and Bathymetry Component (DVBC) conducted a field survey in Himogaan River from December 6 to 18, 2014 with the following scope of work: reconnaissance survey to determine the viability of traversing the planned routes for bathymetric survey; courtesy call to the barangays near the survey area for information dissemination of the team's activities and to ask for a boat and a local aide's assistance; control survey for the establishment of a control point; cross-section survey, bridge as-built and water level marking in MSL of Himogaan Bridge piers; ground validation data acquisition survey of about 106.70 km; and bathymetric survey from Brgy. Paraiso, Sagay City down to the mouth of the river in Brgy. Himogaan Baybay, Sagay City, with an estimated length of 18 km using an Ohmex[™] Single Beam Echo Sounder integrated with a roving GNSS receiver, Trimble[®] SPS 882 utilizing GNSS PPK survey technique. The survey extent of the Himogaan river basin is shown in Figure 32.



Figure 32. Himogaan survey extent

4.2 Control Survey

The GNSS network used for Himogaan River survey is composed of a single loop established on September 9, 2014 occupying the following reference points: NGW-50, a second order GCP in Brgy. Paraiso, Sagay City; and NW-100, a first order BM in Brgy. Jonobjonob, Escalante City, Negros Occidental.

The point NW-130, a NAMRIA established control point, along the approach of Trozo Bridge in Brgy. Daga, Cadiz City, was also occupied to use by the DVBC survey team as marker during the survey.

An offset of 0.0188 m between geoid (EGM2008) and MSL values of the benchmark NW-100 from September 10 to 24, 2014 was applied for referring the elevation of the control points to MSL because the direct processing to BMOrtho will give a low accuracy level.

The summary of reference and control points is shown in Table 24, while the GNSS network established is illustrated in Figure 33.

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)



Figure 33. GNSS Network of Himogaan River Field Survey

Table 24. List of references and control points occupied in Himogaan River survey (Source: NAMRIA; UP-TCAGP)

		Geographic Coordinates (WGS 84)						
Control Point	Order of Accuracy	Latitude	Longitude	Ellipsoidal Height (m)	MSL Elevation (m)	Date Estab- lished		
NGW-50	2 nd order, GCP	10°53'22.52478"	123°21′11.86863″	74.422	13.0512	2013		
NW-100	1 st order, BM	-	-	68.325	7.2272	2007		
NW-130	Used as Marker	-	-	-	-	2017		

The GNSS set-ups on recovered reference points and established control points in Himogaan River are shown in Figure 34 to Figure 36.



Figure 34. GNSS base receiver setup, Trimble[®] SPS 852, at NGW-50 in Himogaan Bridge, Brgy. Paraiso, Sagay City, Negros Occidental



Figure 35. GNSS base receiver setup, Trimble[®] SPS 852, at NW-100 in Danao Bridge, Brgy. Jonobjonob, Escalante City, Negros Occidental



Figure 36. GNSS base receiver setup, Trimble[®] SPS 852, over NW-130 in Troso Bridge, Brgy. Daga, Cadiz City, Negros Occidental

4.3 Baseline Processing

The GNSS baselines were processed simultaneously in TBC by observing that all baselines have fixed solutions with horizontal and vertical precisions within +/- 20 cm and +/- 10 cm requirement, respectively. In case where one or more baselines did not meet all of these criteria, masking is performed. Masking is done by removing/masking portions of these baseline data using the same processing software. It is repeatedly processed until all baseline requirements are met. If the reiteration yields out of the required accuracy, resurvey is initiated. The Baseline processing result of control points in Himogaan River Basin is summarized in Table 25, as generated by TBC software.

Observation	Date of Ob- serva- tion	Solution Type	H. Prec. (Meter)	V. Prec. (Meter)	Geodetic Az.	Ellipsoid Dist. (Meter)	∆Height (Meter)
NGW 50 NW 130 (B4)	09-11- 2014	Fixed	0.005	0.008	302°49'33"	10801.487	-2.613
NW 130 NW 100 (B5)	9-11- 2014	Fixed	0.185	0.037	119°37'31"	27388.571	-3.542
NGW 50 NW 100 (B6)	9-11- 2014	Fixed	0.004	0.006	117°34'16"	16614.558	-6.178

Table 25. Baseline Processing Report for Himogaan River Survey

4.4 Network Adjustment

After the baseline processing procedure, network adjustment is performed using TBC. Looking at the Adjusted Grid Coordinates Table C-of the TBC generated Network Adjustment Report, it is observed that the square root of the sum of the squares of x and y must be less than 20 cm and z less than 10 cm or in equation from:

$$\sqrt{((x_e)^2 + (y_e)^2)}$$
 <20cm and, <10 cm

Where:

 x_e is the Easting Error, y_e is the Northing Error, and z_a is the Elevation Error

for each control point. See the Network Adjustment Report shown in Table 26 to Table 29 for complete details.

The three control points, NGW-50, NW-100, and NW-130 were occupied and observed simultaneously to form a GNSS loop. Coordinates and elevation value of NGW-50 were held fixed during the processing of the control points as presented in Table 26. Computed elevation offset of NW-100 were applied after the processing. Through these reference points, the coordinates and elevation of the unknown control points will be computed.

Table 26. Contro	l Point Constraints
------------------	---------------------

Point ID	Туре	East σ (Meter)	North σ (Meter)	Height σ (Meter)	Elevation σ (Meter)
NGW 50	Global	Fixed	Fixed	Fixed	

Fixed = 0.000001 (Meter)

The list of adjusted grid coordinates, i.e. Northing, Easting, Elevation and computed standard errors of the control points in the network is indicated in Table 27. The fixed control NGW-50 has no values for and elevation error yet.

Table 27. Adjusted C	Grid Coordinates
----------------------	------------------

Point ID	Easting (Meter)	Easting Error (Meter)	Northing (Meter)	Northing Error (Meter)	Elevation (Meter)	Elevation Error (Meter)	Constraint
NGW 50	538610.026	?	1203793.905	?	13.070	?	LLh
NW 100	553341.183	0.013	1196123.819	0.007	7.170	0.020	
NW 130	529529.956	0.017	1209636.397	0.008	10.639	0.024	

With the mentioned equation, for horizontal and for the vertical; the computation for the accuracy are as follows:

NGW-50

horizontal accura vertical accuracy	cy = Fixed = Fixed	
NW-100 horizontal accuracy	$\begin{aligned} xy &= \sqrt{((1.3)^2 + (0.7))} \\ &= \sqrt{(1.69 + 0.49)} \\ &= 1.48 < 20 \text{ cm} \\ &= 2.0 \text{ cm} < 10 \text{ cm} \end{aligned}$	2
NW-130	- 2.0 cm < 10 cm	
horizontal accura	$\begin{aligned} xy &= \sqrt{((1.7)^2 + (0.8))} \\ &= \sqrt{(2.89 + 0.64)} \\ &= 1.88 < 20 \text{ cm} \end{aligned}$	2
vertical accuracy	= 2.4 cm < 10 cm	n

Following the given formula, the horizontal and vertical accuracy result of the three occupied control points are within the required precision.

Point ID	Latitude	Latitude Longitude		Height Error (Meter)	Constraint
NGW 50	N10°53'22.52478"	E123°21'11.86863"	74.422	?	LLh
NW 130	N10°56'33.04992"	E123°16′12.93293"	71.819	0.024	
NW 100	N10°49'12.14033"	E123°29'16.71793"	68.325	0.020	

The corresponding geodetic coordinates of the observed points are within the required accuracy as shown in Table C-5. Based on the result of the computation, the equation is satisfied; hence, the required accuracy for the program was met.

The summary of reference and control points used is indicated in Table 29.

Table 29. Reference and control points used and its location (Source: NAMRIA, UP-TCAGP)

		Geograph	ic Coordinates (WGS	UTM ZONE 51 N			
Control Point	Order of Accuracy	Latitude	Longitude	Ellipsoidal Height (m)	Northing	Easting	MSL El- evation (m)
NGW- 50	2 nd order, GCP	10°53'22.52478"	123°21′11.86863″	74.422	1203793.905	538610.026	13.051
NW-100	1 st order BM	10°49′12.14033″	123°29′16.71793″	68.325	1196123.819	553341.183	7.227
NW-130	Used as Marker	10°56'33.04992″	123°16′12.93293″	71.819	1209636.397	529529.956	10.643

4.5 Cross-section, Bridge As-Built, and Water Level Marking

Cross-section and bridge as-built surveys were conducted on September 12 and 22, 2014 along the downstream part of Himogaan bridge in Brgy. Paraiso, Sagay Cityusing a GNSS receiver Trimble[®] SPS 882 and an Ohmex[™] Single Beam Echo Sounder utilizing GNSS PPK survey technique as shown in Figure 37.



Figure 37. (A) Cross-Section Survey and (B) Bridge As-Built survey at Himogaan Bridge in Sagay City

The cross-sectional line of Himogaan Bridge is about 83.28 m with 86 points acquired using NGW-50 as GNSS base station. Figure 38 to Figure 40 show the location map, cross-section diagram, and bridge as-

built form of Himogaan Bridge.



Figure 38. Location map of Himogaan bridge cross-section



Bridge N	ame: H	limoga-An Bridge				Date: Septen	nber 12 & 22, 201	
River Na	er Name: Himoga-An River				Time: 12:30 PM			
Location	(Brgy, Ci	ity,Region): Brgy. Fabrica	, Sagay City, N	legros O	ccidental			
Survey T	eam: Ne	gros Occidental Survey Te	am					
Flow con	dition:	low <u>normal</u> high			Weather O	Condition: fai	r rainy	
Latitude	: 10d53'	22.52478"N Longitud	e: 123d21'11.	86863" (E			
В	A2	D 🔪	\bigcirc	BA3		sgend:		
BA1		V V			BA4	A = Bridge Approach b = Abutment	P = Pier LC = Low D = Deck HC = High	
	Ab1			Ab2				
		P		HC				
-	0.0000	Deck (Please start your	measurement from	m the left s	ide of the bank fac	ing upstream)		
cievation	: 6.9663 f	Station	m	High	Chord Flevatio	u 109.91 W	w Chord Flevation	
1		-			12.815 m		-	
2					12.013 III			
2								
4								
5								
,		Bridge Approach miss	a start your measurem	ent from the l	aft side of the back lash	an documentre and		
		bridge Approach (Ann	e start your measurem	ent in one s	and side of the bank radi	ng downstream)		
	Statio	n(Distance from BA1)	Elevation		Station(Distance from BA1)		Elevation	
BA1		0	12.6142m	BA3	122	122.78 m		
BA2		15.23 m	13.1552 m	BA4	155.	155.607 m		
Abutmer	nt: Ist	he abutment sloping?	Yes No;	If yes,	fill in the follov	ving informatio	on:	
		Station (Distance fror	n BA1)		Elev	vation	
	Ab1		n/a	n/a			n/a	
	Ab2		n/a			1	n/a	
		Pier (Please start your m	easurement from	the left sid	e of the bank facin	g downstream)		
Shap	e: rectan	gular Number	of Piers: 2		Height of col	umn footing:		
		Station (Distance fro	om BA1)	E	levation		Pier Width	
Pier	Pier 1 23.5648			13	3.2112 m			
Pier	2	73.02		1	13.2852			
Pier	4	121.73			13.1932			
Pier	5							
Pier	6							
		1100EF 11-						

Figure 40. Himogaan Bridge Data Form

The water surface elevation of Himogaan River on the left and right banks was acquired using GNSS receiver Trimble[®] SPS 882 in GNSS PPK survey technique on September 12, 2014 at 12:57 PM. The resulting water surface elevation data is 1.1562 m above MSL, translated and marked at the pier of Himogaan Bridge as shown in Figure 41. The markings on the bridge piers shall serve as a reference for flow data gathering and depth gauge deployment of UP Cebu PHIL-LIDAR 1.



Figure 41. Water Level Mark at the pier of Himogaan Bridge

4.6 Validation Points Acquisition Survey

Validation points acquisition survey was conducted on September 12 and 13, 2014 using a survey GNSS rover receiver Trimble[®] SPS 882 mounted on a pole, which was attached in front of the vehicle as shown in Figure 42. It was secured with a steel rod and tied with cable ties to ensure that it was horizontally and vertically balanced. The antenna height was measured from the ground up to the bottom of the notch of the GNSS rover receiver with a value of 2.10 m.

The ground validation line is approximately 106.70 km in length and with a total of 8,887 gathered points acquired using NGW-50 and NW-130 as GNSS base station. The survey covered four Cities, namely: Escalante, Sagay, Cadiz and Victorias. Figure 43 shows the ground validation survey result.





Figure 42. (A) Occupied base station, NGW-50 in Himogaan Bridge, Sagay City and (B) Installation of GNSS Receiver Trimble[®] SPS 882 in front of a van



4.7 Bathymetric Survey

Bathymetric survey was conducted on December 9, 2014 and December 14, 2014 using an Ohmex™ Single Beam Echo Sounder integrated with a roving GNSS receiver, Trimble*SPS 882, installed on a boat was utilizing PPK survey technique as shown in Figure 44. The survey began in the upstream part of the river in Brgy. Parais, Sagay City with coordinates 10°52'41.10112"123°21'07.23521", down to the mouth of the river in Brgy. Himogaan Baybay, Sagay City with coordinates 10°56'54.14218"123°24'03.54658". The reference point NGW-50, located at Himogaan Bridge in Brgy. Fabrica, Sagay City, served as the base station in conducting the bathymetric survey.



OHMEX Top Unit

Figure 44. Set up on a paddle boat for the Bathymetric Survey at the Himogaan River upstream

Bathymetric line measured is approximately 18 km in length with a total of 34,313 points acquired using NGW-50 covering Brgy. Himogaan Baybay and Paraiso as shown in Figure 45. A CAD drawing was also produced to illustrate the Himogaan riverbed profile. As shown in Figure 46 and Figure 47, the lowest elevation was recorded at -11.997 m in MSL, approximately 2,000 m from Himogan Bridge and about 1,000 m from Himogaan to Bridge, while the highest elevation observed was 0.519 m in MSL located in Brgy. Paraiso, Sagay City.



Figure 45. Bathymetric points gathered from Himogaan River



Himoga-An Riverbed Profile







Figure 47. Riverbed profile of Himogaan River

CHAPTER 5: FLOOD MODELING AND MAPPING

Dr. Alfredo Mahar Lagmay, Christopher Uichanco, Sylvia Sueno, Marc Moises, Hale Ines, Miguel del Rosario, Kenneth Punay, Neil Tingin, Narvin Clyd Tan, and Marvin Arias

5.1 Data Used for Hydrologic Modeling

5.1.1 Hydrometry and Rating Curves

All data that affect the hydrologic cycle of the river basin was monitored, collected, and analyzed. Rainfall, water level, and flow in a certain period of time, which may affect the hydrologic cycle of the Himogaan River Basin were monitored, collected, and analyzed.

5.1.2 Precipitation

Precipitation data was taken from an automatic rain gauge (ARG) deployed by the UP Cebu Flood Modeling Component (FMC) team. The ARG was installed at Brgy. Puey, Sagay City, Negros Occidental (Figure 50). The precipitation data collection started from July 29, 2016 at 2:20 PM to July 30, 2016 at 12:10 with 10 minutes recording interval.

The total precipitation for this event in Brgy Puey ARG was 43.8 mm. It has a peak rainfall of 2.88 mm. on January 9, 2017 at 9:25 in the evening. The lag time between the peak rainfall and discharge is 7 hours and 35 minutes.



Figure 48. Location map of Himogaan HEC-HMS model used for calibration

5.1.3 Rating Curves and River Outflow

A rating curve was developed at Himogaan Bridge, Sagay City, Negros Occidental (10°53'25.0"N 123°21'12.9"E). It gives the relationship between the observed water levels at Himogaan Bridge and outflow of the watershed at this location.

For Himogaan Bridge, the rating curve is expressed as Q = 162.07x - 129.63 as shown in Figure 50.



Himoga-an Bridge Cross-Section

Figure 49. Cross-Section Plot of Himogaan Bridge



Figure 50. Rating Curve at Himogaan Bridge, Paraiso, Sagay City

This rating curve equation was used to compute the river outflow at Himogaan Bridge for the calibration of the HEC-HMS model shown in Figure 51. Peak discharge is 461.1 cubic meters per second at 5:00 PM, January 9, 2017.



5.2 RIDF Station

The Philippines Atmospheric Geophysical and Astronomical Services Administration (PAGASA) computed Rainfall Intensity Duration Frequency (RIDF) values for the Iloilo Rain Gauge. The RIDF rainfall amount for 24 hours was converted to a synthetic storm by interpolating and re-arranging the value in such a way certain peak value will be attained at a certain time. This station chosen based on its proximity to the Himogaan watershed. The extreme values for this watershed were computed based on a 59-year record.

COMPUTED EXTREME VALUES (in mm) OF PRECIPITATION									
T (yrs)	10 mins	20 mins	30 mins	1 hr	2 hrs	3 hrs	6 hrs	12 hrs	24 hrs
5	28.7	39.4	48	59.4	74.9	90	114.7	131.7	165.2
10	33.9	45.6	55.6	68.1	85	103.6	133.6	155.4	198.9
25	40.5	53.5	65.3	79.2	97.6	120.8	157.6	185.3	241.5
50	45.4	59.4	72.4	87.3	107	133.5	175.3	207.4	273.1
100	50.3	65.2	79.5	95.4	116.4	146.2	193	229.4	304.5

Table 30. RIDF values for Iloilo Rain Gauge computed by PAGASA



Figure 52. Location of Iloilo RIDF station relative to Himogaan River Basin



Figure 53. Synthetic storm generated for a 24-hr period rainfall for various return periods

5.3 HMS Model

The soil dataset was generated in 2004 by the Bureau of Soils; this is under the Department of Agriculture. The land cover dataset is from the National Mapping and Resource information Authority (NAMRIA). The soil and land cover of the Himogaan River Basin are shown in Figures 54 and 55, respectively.


Figure 54. Soil map of Himogaan River Basin

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)



Figure 55. Land cover map of Himogaan River Basin



Figure 56. Slope Map of Himogaan River Basin

Using the SAR-based DEM, the Himogaan basin was delineated and further subdivided into subbasins. The model consists of 47 sub basins, 23 reaches, and 23 junctions as shown in Figure 57. The main outlet is at Himogaan Bridge.



Figure 57. The Himogaan River Basin model generated using HEC-HMS

5.4 Cross-section Data

Riverbed cross-sections of the watershed are crucial in the HEC-RAS model setup. The cross-section data for the HEC-RAS model was derived using the LiDAR DEM data. It was defined using the Arc GeoRAS tool and was post-processed in ArcGIS.



Figure 58. River cross-section of Himogaan River generated through Arcmap HEC GeoRAS tool

5.5 Flo 2D Model

The automated modelling process allows for the creation of a model with boundaries that are almost exactly coincidental with that of the catchment area. As such, they have approximately the same land area and location. The entire area is divided into square grid elements, 10 meter by 10 meter in size. Each element is assigned a unique grid element number which serves as its identifier, then attributed with the parameters required for modelling such as x-and y-coordinate of centroid, names of adjacent grid elements, Manning coefficient of roughness, infiltration, and elevation value. The elements are arranged spatially to form the model, allowing the software to simulate the flow of water across the grid elements and in eight directions (north, south, east, west, northeast, northwest, southeast, southwest).

Based on the elevation and flow direction, it is seen that the water will generally flow from the south of the model to the northeast, following the main channel. As such, boundary elements in those particular regions of the model are assigned as inflow and outflow elements respectively.



Figure 59. Screenshot of subcatchment with the computational area to be modeled in FLO-2D GDS Pro

The simulation is then run through FLO-2D GDS Pro. This particular model had a computer run time of 22.20007 hours. After the simulation, FLO-2D Mapper Pro is used to transform the simulation results into spatial data that shows flood hazard levels, as well as the extent and inundation of the flood. Assigning the appropriate flood depth and velocity values for Low, Medium, and High creates the following food hazard map. Most of the default values given by FLO-2D Mapper Pro are used, except for those in the Low hazard level. For this particular level, the minimum h (Maximum depth) is set at 0.2 m while the minimum vh (Product of maximum velocity (v) times maximum depth (h)) is set at 0 m2/s. The generated hazard maps for Himogaan are in Figure 70, 72, and 74, respectively.



Figure 60. Generated 100-year rain return hazard map from FLO-2D Mapper

The creation of a flood hazard map from the model also automatically creates a flow depth map depicting the maximum amount of inundation for every grid element. The legend used by default in Flo-2D Mapper is not a good representation of the range of flood inundation values, so a different legend is used for the layout. In this particular model, the inundated parts cover a maximum land area of 22958400.00 m2. The generated flood depth maps for Himogaan are in Figure 71, 73, and 75, respectively.



Figure 61. Generated 100-year rain return flow depth map from FLO-2D Mapper

There is a total of 61783670.89 m3 of water entering the model. Of this amount, 6072171.66 m3 is due to rainfall while 55711499.22 m3 is inflow from other areas outside the model 4363573.50 m3 of this water is lost to infiltration and interception, while 33831397.31 m3 is stored by the flood plain. The rest, amounting up to 23588699.98 m3, is outflow.

5.6 Results of HMS Calibration



After calibrating the Silaga HEC-HMS river basin model, its accuracy was measured against the observed values. Figure 62 shows the comparison between the two discharge data.

Figure 62. Outflow Hydrograph of Himogaan produced by the HEC-HMS model compared with observed outflow

Enumerated in Table 31 are the adjusted ranges of values of the parameters used in calibrating the model.

Hydrologic Element	Calculation Type	Method	Parameter	Range of Calibrated Values
	Loss	SCS Curve number	Initial Abstraction (mm)	0.015-0.13
		SCS Curve number	Curve Number	39.3-99
Basin	Transform	Clark Unit Hydro- graph	Time of Concentration (hr)	0.25-9
			Storage Coefficient (hr)	0.11-5.52
	Baseflow	Decession	Recession Constant	0.9
		Recession	Ratio to Peak	0.65
Reach	Routing	Muskingum-Cunge	Manning's Coefficient	0.0001

Table 31. Range of Calibrated Values for Himogaan River Basin

Initial abstraction defines the amount of precipitation that must fall before surface runoff. The magnitude of the outflow hydrograph increases as initial abstraction decreases. The range of values from 0.015 mm to 0.13 mm means that there is minimal to average amount of infiltration or rainfall interception by vegetation.

Curve number is the estimate of the precipitation excess of soil cover, land use, and antecedent moisture. The magnitude of the outflow hydrograph increases as curve number increases. The range of 65 to 90 for curve number is advisable for Philippine watersheds depending on the soil and land cover of the area. For Himogaan, the basin mostly consists of brushlands and urban area, and the soil consists of clay, clay loam, and mountain soil.

Time of concentration and storage coefficient are the travel time and index of temporary storage of runoff in a watershed. The range of calibrated values from 0.25 hours to 9 hours determines the reaction time of the model with respect to the rainfall. The peak magnitude of the hydrograph also decreases when these parameters are increased.

Recession constant is the rate at which baseflow recedes between storm events and ratio to peak is the ratio of the baseflow discharge to the peak discharge. Recession constant of 0.9 indicates that the basin is unlikely to quickly go back to its original discharge and instead, will be higher. Ratio to peak of 0.65 indicates a steeper receding limb of the outflow hydrograph.

Manning's roughness coefficient of 0.0001 corresponds to the common roughness of Philippine watersheds. Himogaan river basin is determined to be cultivated with mature field crops.

Accuracy Measure	Value
RMS Error	16.7
r ²	0.9917
NSE	0.98
RSR	0.15
PBIAS	1.35

Table 32. Summary of the Efficiency Test of Himogaan HMS Model

The Root Mean Square Error (RMSE) method aggregates the individual differences of these two measurements. It was computed as 16.7 (m3/s).

The Pearson correlation coefficient (r^2) assesses the strength of the linear relationship between the observations and the model. This value being close to 1 corresponds to an almost perfect match of the observed discharge and the resulting discharge from the HEC HMS model. Here, it measured 0.9917.

The Nash-Sutcliffe (E) method was also used to assess the predictive power of the model. Here the optimal value is 1. The model attained an efficiency coefficient of 0.98.

A positive Percent Bias (PBIAS) indicates a model's propensity towards under-prediction. Negative values indicate bias towards over-prediction. Again, the optimal value is 0. In the model, the PBIAS is 0.15.

The Observation Standard Deviation Ratio, RSR, is an error index. A perfect model attains a value of 0 when the error in the units of the valuable a quantified. The model has an RSR value of 1.35.

5.7 Calculated outflow hydrographys and discharge values for different Rainfall Return Periods

5.7.1 Hydrograph using the Rainfall Runoff Model

The summary graph (Figure 63) shows the Himogaan outflow using the Iloilo Rainfall Intensity-Duration-Frequency curves (RIDF) in 5 different return periods (5-year, 10-year, 25-year, 50-year, and 100-year rainfall time series) based on the Philippine Atmospheric Geophysical and Astronomical Services Administration (PAG-ASA) data. The simulation results reveal significant increase in outflow magnitude as the rainfall intensity increases for a range of durations and return periods.



Figure 63. Outflow hydrograph at Himogaan Station generated using Iloilo RIDF simulated in HEC-HMS

A summary of the total precipitation, peak rainfall, peak outflow and time to peak of the Himogaan discharge using the Iloilo Rainfall Intensity-Duration-Frequency curves (RIDF) in five different return periods is shown in Table 33.

		-		
RIDF Period	Total Precipitation (mm)	Peak rainfall (mm)	Peak outflow (m ³/s)	Time to Peak
5-Year	165.2	28.7	1931.5	4 hours, 30 minutes
10-Year	198.9	33.9	2255.2	4 hours, 30 minutes
25-Year	241.5	40.5	2663.7	4 hours, 20 minutes
50-Year	273.1	45.4	2964.2	4 hours, 20 minutes
100-Year	304.5	50.3	3264.3	4 hours, 10 minutes

Table 33. Peak values of the Himogaan HEC-HMS Model outflow using the Iloilo RIDF

5.7.2 Discharge data using Dr. Horritts's recommended hydrologic method

The river discharges entering the floodplain are shown in Figure 64 to Figure 68 and the peak values are summarized in Table 34 to Table 37.



Figure 64. Himogaan and Tanao river (1) generated discharge using 5-, 25-, and 100-year Iloilo and Mactan stations' rainfall intensity-duration-frequency (RIDF) in HEC-HMS



Figure 65. Himogaan and Tanao river (2) generated discharge using 5-, 25-, and 100-year Iloilo and Mactan stations' rainfall intensity-duration-frequency (RIDF) in HEC-HMS







Figure 67. Himogaan and Tanao river (4) generated discharge using 5-, 25-, and 100-year Iloilo and Mactan stations' rainfall intensity-duration-frequency (RIDF) in HEC-HMS



Figure 68. Himogaan and Tanao river (5) generated discharge using 5-, 25-, and 100-year lloilo and Mactan stations' rainfall intensity-duration-frequency (RIDF) in HEC-HMS

Table 34. Summary of Himogaan a	nd Tanao river (1) discharge	generated in HEC-HMS
---------------------------------	------------------------------	----------------------

RIDF Period	Peak discharge (cms)	Time-to-peak	
100-Year	82.8	13 hours, 20 minutes	
25-Year	63.4	13 hours, 30 minutes	
5-Year	39.5	13 hours, 30 minutes	

Table 35. Summary of Himogaan and Tanao river (2) discharge generated in HEC-HMS

RIDF Period	Peak discharge (cms)	Time-to-peak
100-Year	60.0	16 hours, 10 minutes
25-Year	44.6	16 hours, 10 minutes
5-Year	26.2	16 hours, 10 minutes

Table 36. Summary of Himogaan and Tanao river (3) discharge generated in HEC-HMS

RIDF Period	Peak discharge (cms)	Time-to-peak	
100-Year	4646.0	13 hours	
25-Year	3430.0	13 hours	
5-Year	2176.8	13 hours	

RIDF Period	Peak discharge (cms)	Time-to-peak	
100-Year	100.7	14 hours	
25-Year	74.3	14 hours	
5-Year	42.3	14 hours	

Table 38. Summary of Himogaan and Tanao river (5) discharge generated in HEC-HMS

RIDF Period	Peak discharge (cms)	Time-to-peak
100-Year	100.5	16 hours, 20 minutes
25-Year	71.6	16 hours, 30 minutes
5-Year	43.1	16 hours, 30 minutes

The comparison of the discharge results using Dr. Horritt's recommended hydrological method against the bankful and specific discharge estimates is shown in Table 39.

				VALIDATION	
Discharge Point	Q _{MED(SCS)} , cms	Q _{BANKFUL} , cms	Q _{MED(SPEC)} , cms	Bankful Discharge	Specific Discharge
Himogaan-Tanao (1)	34.760	51.930	34.649	Pass	Pass
Himogaan-Tanao (2)	23.056	29.710	75.694	Pass	Fail
Himogaan-Tanao (3)	1915.584	3471.490	529.417	Pass	Fail
Himogaan-Tanao (4)	37.224	58.830	45.224	Pass	Pass
Himogaan-Tanao (5)	37.928	66.320	118.887	Pass	Fail

Table 39. Validation of river discharge estimates

All five values from the HEC-HMS river discharge estimates were able to satisfy at least one of the conditions for validation using the bankful and specific discharge methods. The calculated values are based on theory but are supported using other discharge computation methods so they were good to use flood modeling. However, these values will need further investigation for the purpose of validation. It is therefore recommended to obtain actual values of the river discharges for higher-accuracy modeling.

5.8 River Analysis (RAS) Model Simulation

The HEC-RAS Flood Model produced a simulated water level at every cross-section for every time step for every flood simulation created. The resulting model will be used in determining the flooded areas within the model. The simulated model will be an integral part in determining real-time flood inundation extent of the river after it has been automated and uploaded on the DREAM website. The sample generated map of Himogaan River using the calibrated HMS event flow is shown in Figure 69.



Figure 69. Sample output of Himogaan RAS Model

5.9 Flow Depth and Flood Hazard

The resulting hazard and flow depth maps have a 10m resolution. Figure 70 to Figure 75 shows the 5-, 25-, and 100-year rain return scenarios of the Himogaan floodplain.





79









82



Figure 75. 100-year Flow Depth Map for Himogaan Floodplain

5.10 Inventory of Areas Exposed to Flooding of Affected Areas

Affected barangays in Himogaan river basin, grouped by municipality, are listed below. For the said basin, two municipalities consisting of 12 barangays are expected to experience flooding when subjected to 5-yr rainfall return period.

For the 5-year return period, 1.88% of the city of Cadiz with an area of 516.18 sq. km. will experience flood levels of less 0.20 meters. 0.07% of the area will experience flood levels of 0.21 to 0.50 meters while 0.06%, 0.06%, 0.12%, and 0.04% of the area will experience flood depths of 0.51 to 1 meter, 1.01 to 2 meters, 2.01 to 5 meters, and more than 5 meters, respectively. Listed in Table 40 are the affected areas in square kilometres by flood depth per barangay.

Affected area (sq. km.)	Area of affected barangays in Cadiz City (in sq. km.)				
by flood depth (in m.)	Banquerohan	Cabahug	Magsaysay	Tiglawigan	
0.03-0.20	0.55	2.42	2.91	3.8	
00.21-0.50	0.02	0.07	0.09	0.20	
0.51-1.00	0	0.08	0.1	0.14	
1.01-2.00	0	0.15	0.06	0.12	
2.01-5.00	0	0.59	0.03	0.01	
> 5.00	0	0.09	0.11	0	

Table 40. Affected Areas in Cadiz City, Negros Occidental during 5-Year Rainfall Return Period



Figure 76. Affected Areas in Cadiz City, Negros Occidental during 5-Year Rainfall Return Period

For the city of Sagay, with an area of 304.62 sq. km., 16.36% will experience flood levels of less 0.20 meters. 1% of the area will experience flood levels of 0.21 to 0.50 meters while 1.57%, 1.72%, 1.49%, and 0.82% of the area will experience flood depths of 0.51 to 1 meter, 1.01 to 2 meters, 2.01 to 5 meters, and more than 5 meters, respectively. Listed in Table 41 are the affected areas in square kilometres by flood depth per barangay.

Affected area		Area of affected barangays in Sagay City (in sq. km.)						
(sq. km.) by flood depth (in m.)	Fabrica	Himogaan Baybay	Malubon	Old Sagay	Paraiso	Poblacion I	Poblacion II	Taba-Ao
0.03-0.20	1.28	17.44	4.002	4.24	10.4	0.75	10.34	1.38
0.21-0.50	0.041	1.25	0.17	0.49	0.48	0.081	0.47	0.062
0.51-1.00	0.035	1.77	0.14	1.98	0.4	0.011	0.41	0.042
1.01-2.00	0.052	2.95	0.14	1.26	0.37	0.0011	0.46	0.016
2.01-5.00	0.11	3.49	0.22	0	0.37	0	0.35	0
> 5.00	0.27	1.3	0.25	0	0.56	0	0.13	0

Table 41. Affected Areas in Sagay City, Negros Occidental during 5-Year Rainfall Return Period



Figure 77. Affected Areas in Sagay City, Negros Occidental during 5-Year Rainfall Return Period

For the 25-year return period, 1.81% of the city of Cadiz with an area of 516.18 sq. km. will experience flood levels of less 0.20 meters. 0.08% of the area will experience flood levels of 0.21 to 0.50 meters while 0.07%, 0.07%, 0.13%, and 0.07% of the area will experience flood depths of 0.51 to 1 meter, 1.01 to 2 meters, 2.01 to 5 meters, and more than 5 meters, respectively. Listed in Table 42 are the affected areas in square kilometres by flood depth per barangay.

Affected area (sq. km.)	Area of affected barangays in Cadiz City (in sq. km.)					
by flood depth (in m.)	Banquerohan	Cabahug	Magsaysay	Tiglawigan		
0.03-0.20	0.54	2.32	2.84	3.69		
0.21-0.50	0.04	0.08	0.1	0.22		
0.51-1.00	0.01	0.07	0.1	0.16		
1.01-2.00	0.01	0.12	0.07	0.15		
2.01-5.00	0	0.58	0.05	0.05		
> 5.00	0	0.23	0.13	0		

Table 42. Affected Areas in Cadiz City, Negros Occidental during 25-Year Rainfall Return Period



Figure 78. Affected Areas in Cadiz City, Negros Occidental during 25-Year Rainfall Return Period

For the city of Sagay, with an area of 304.62 sq. km., 15.41% will experience flood levels of less 0.20 meters. 1.1% of the area will experience flood levels of 0.21 to 0.50 meters while 1%, 1.7%, 2.7%, and 1.01% of the area will experience flood depths of 0.51 to 1 meter, 1.01 to 2 meters, 2.01 to 5 meters, and more than 5 meters, respectively. Listed in Table 43 are the affected areas in square kilometres by flood depth per barangay.

Table 43. Affected Ar	eas in Sagay City, N	Negros Occidental o	during 25-Year Rair	nfall Return Period

Affected area		Area of affected barangays in Cadiz City (in sq. km.)						
(sq. km.) by flood depth (in m.)	Fabrica	Himogaan Baybay	Malubon	Old Sagay	Paraiso	Poblacion I	Poblacion II	Taba-Ao
0.03-0.20	1.22	16.18	4.04	3.41	10.26	0.66	9.84	1.32
0.21-0.50	0.043	1.24	0.23	0.58	0.53	0.16	0.50	0.082
0.51-1.00	0.03	1.42	0.17	0.55	0.4	0.018	0.41	0.054
1.01-2.00	0.049	2.21	0.11	1.86	0.35	0.0019	0.56	0.036
2.01-5.00	0.11	5.30	0.11	1.58	0.54	0	0.58	0
> 5.00	0.34	1.87	0.26	0	0.49	0	0.26	0



Figure 79. Affected Areas in Sagay City, Negros Occidental during 25-Year Rainfall Return Period

For the 100-year return period, 1.77% of the city of Cadiz with an area of 516.18 sq. km. will experience flood levels of less 0.20 meters. 0.09% of the area will experience flood levels of 0.21 to 0.50 meters while 0.07%, 0.07%, 0.1%, and 0.14% of the area will experience flood depths of 0.51 to 1 meter, 1.01 to 2 meters, 2.01 to 5 meters, and more than 5 meters, respectively. Listed in Table 44 are the affected areas in square kilometres by flood depth per barangay.

Affected area (sq. km.)	Area of affected barangays in Cadiz City (in sq. km.)					
by flood depth (in m.)	Banquerohan	Cabahug	Magsaysay	Tiglawigan		
0.03-0.20	0.52	2.22	2.78	3.6		
0.21-0.50	0.05	0.08	0.1	0.25		
0.51-1.00	0.01	0.06	0.1	0.18		
1.01-2.00	0.01	0.1	0.09	0.16		
2.01-5.00	0	0.39	0.05	0.09		
> 5.00	0	0.55	0.18	0		

Table 44. Affected Areas in Cadiz City, Negros Occidental during 100-Year Rainfall Return Period



Figure 80. Affected Areas in Cadiz City, Negros Occidental during 100-Year Rainfall Return Period

For the city of Sagay, with an area of 304.62 sq. km., 14.65% will experience flood levels of less 0.20 meters. 1.15% of the area will experience flood levels of 0.21 to 0.50 meters while 1%, 1.35%, 3.24%, and 1.6% of the area will experience flood depths of 0.51 to 1 meter, 1.01 to 2 meters, 2.01 to 5 meters, and more than 5 meters, respectively. Listed in Table 45 are the affected areas in square kilometres by flood depth per barangay.

Affected area	ea Area of affected barangays in Cadiz City (in sq. km.)					km.)		
(sq. km.) by flood depth (in m.)	Fabrica	Himogaan Baybay	Malubon	Old Sagay	Paraiso	Poblacion I	Poblacion II	Taba-Ao
0.03-0.20	1.18	15.11	3.91	2.88	10.06	0.62	9.58	1.28
0.21-0.50	0.043	1.24	0.24	0.64	0.55	0.2	0.49	0.1
0.51-1.00	0.024	1.22	0.18	0.64	0.44	0.024	0.4	0.061
1.01-2.00	0.04	2.03	0.15	0.92	0.36	0.0027	0.55	0.046
2.01-5.00	0.076	5.53	0.14	2.91	0.45	0	0.78	0.0034
> 5.00	0.43	3.09	0.31	0	0.72	0	0.35	0

Table 45. Affected Areas in Sagay City, Negros Occidental during 100-Year Rainfall Return Period



Figure 81. Affected Areas in Sagay City, Negros Occidental during 100-Year Rainfall Return Period

Among the barangays in the city of Cadiz, Tiglawigan is projected to have the highest percentage of area that will experience flood levels at 4.27%. Meanwhile, Cabahug posted the second highest percentage of area that may be affected by flood depths at 3.4%.

Among the barangays in the city of Sagay, Himogaan Baybay is projected to have the highest percentage of area that will experience flood levels at 28.21%. Meanwhile, Paraiso posted the second highest percentage of area that may be affected by flood depths at 12.57%.

Moreover, the generated flood hazard maps for the Himogaan-Tanao Floodplain were used to assess the vulnerability of the educational and medical institutions in the floodplain. Using the flood depth units of PAG-ASA for hazard maps - "Low", "Medium", and "High" - the affected institutions were given their individual assessment for each Flood Hazard Scenario (5 yr, 25 yr, and 100 yr).

Warning Loval	Area Covered in sq. km.				
warning Lever	5 year	25 year	100 year		
Low	3.56	3.92	4.12		
Medium	8.83	16.22	5.91		
High	10.65	16.22	18.89		
Total	23.04	36.36	28.92		

Table 46. Area covered by each warning level with respect to the rainfall scenario

Of the twenty (20) identified Education Institute in Himogaan-Tanao Flood plain, 1 school was assessed to be exposed to the medium level flooding during a 25 year scenario while 2 schools were assessed to be exposed to high level flooding in the same scenario. In the 100 year scenario, 3 schools were assessed to be exposed to the high level flooding scenario.

Two (2) Medical Institutions were identified in Himogaan-Tanao Floodplain, only 1 was assessed to be exposed to high level flooding in two different scenarios, medium and high, in Barangay Himogaan Baybay.

5.11 Flood Validation

In order to check and validate the extent of flooding in different river systems, there is a need to perform validation survey work. Field personnel gathered secondary data regarding flood occurrence in the area within the major river system in the Philippines.

From the Flood Depth Maps produced by Phil-LiDAR 1 Program, multiple points representing the different flood depths for different scenarios were identified for validation.

The validation personnel went to the specified points identified in a river basin and gathered data regarding the actual flood level in each location. Data gathering was done through a local DRRM office to obtain maps and situation reports about the past flooding events and through interview of some residents with knowledge of or have had experienced flooding in a particular area.

After which, the actual data from the field was compared to the simulated data to assess the accuracy of the Flood Depth Maps produced and to improve on what is needed.

The flood validation consisted of 245 points randomly selected all over Himogaan floodplain. It has an RMSE value of 2.959962.



123°20'0"E

Figure 82. Validation points for 5-year Flood Depth Map of Himogaan Floodplain



Figure 83. Flood map depth vs. actual flood depth

Actual Flood	Modeled Flood Depth (m)								
Depth (m)	0-0.20	0.21-0.50	0.51-1.00	1.01-2.00	2.01-5.00	> 5.00	Total		
0-0.20	75	5	10	10	15	5	120		
0.21-0.50	12	3	4	3	2		24		
0.51-1.00	15	1	12	6	1		35		
1.01-2.00	7	1	7	7	3		25		
2.01-5.00	5	2	5	0	4	4	20		
> 5.00	1	0	0	3	10	7	21		
Total	115	12	38	29	35	16	245		

Table 47. Actual	Flood Depth vs Sir	nulated Flood	Depth in	Himogaan
	•		•	0

The overall accuracy generated by the flood model is estimated at 44.08%, with 108 points correctly matching the actual flood depths. In addition, there were 52 points estimated one level above and below the correct flood depths while there were 38 points and 21 points estimated two levels above and below, and three or more levels above and below the correct flood. A total of 68 points were overestimated while a total of 69 points were underestimated in the modelled flood depths of Himogaan-Tanao.

	No. of Points	%
Correct	108	44.08
Overestimated	68	27.76
Underestimated	69	28.16
Total	245	100

Table 48. Summary of Accuracy Assessment in the Himogaan River Basin Survey

REFERENCES

Ang M.O., Paringit E.C., et al. 2014. DREAM Data Processing Component Manual. Quezon City, Philippines: UP Training Center for Applied Geodesy and Photogrammetry.

Balicanta L.P., Paringit E.C., et al. 2014. DREAM Data Validation Component Manual. Quezon City, Philippines: UP Training Center for Applied Geodesy and Photogrammetry.

Brunner, G. H. 2010a. HEC-RAS River Analysis System Hydraulic Reference Manual. Davis, CA: U.S. Army Corps of Engineers, Institute for Water Resources, Hydrologic Engineering Center.

Lagmay A.F., Paringit E.C., et al. 2014. DREAM Flood Modeling Component Manual. Quezon City, Philippines: UP Training Center for Applied Geodesy and Photogrammetry.

Paringit E.C, Balicanta L.P., Ang, M.O., Sarmiento, C. 2017. Flood Mapping of Rivers in the Philippines Using Airborne Lidar: Methods. Quezon City, Philippines: UP Training Center for Applied Geodesy and Photogrammetry.

Sarmiento C., Paringit E.C., et al. 2014. DREAM Data Acquisition Component Manual. Quezon City, Philippines: UP Training Center for Applied Geodesy and Photogrammetry.

UP TCAGP 2016, Acceptance and Evaluation of Synthetic Aperture Radar Digital Surface Model (SAR DSM) and Ground Control Points (GCP). Quezon City, Philippines: UP Training Center for Applied Geodesy and Photogrammetry.

ANNEXES

Annex 1. Optech Technical Specifications

1. Pegasus Sensor



Laptop

Control Rack

Parameter	Specification
Operational envelope (1,2,3,4)	150-5000 m AGL, nominal
Laser wavelength	1064 nm
Horizontal accuracy (2)	1/5,500 x altitude, 1σ
Elevation accuracy (2)	< 5-20 cm, 1σ
Effective laser repetition rate	Programmable, 100-500 kHz
Position and orientation system	POS AV ™AP50 (OEM)
Scan width (FOV)	Programmable, 0-75 °
Scan frequency (5)	Programmable, 0-140 Hz (effective)
Sensor scan product	800 maximum
Beam divergence	0.25 mrad (1/e)
Roll compensation	Programmable, ±37° (FOV dependent)
Vertical target separation distance	<0.7 m
Range capture	Up to 4 range measurements, including 1st, 2nd, 3rd, and last returns
Intensity capture	Up to 4 intensity returns for each pulse, including last (12 bit)
Image capture	5 MP interline camera (standard); 60 MP full frame (optional)
Full waveform capture	12-bit Optech IWD-2 Intelligent Waveform Digitizer
Data storage	Removable solid state disk SSD (SATA II)
Power requirements	28 V, 800 W, 30 A
Dimensions and weight	Sensor: 630 x 540 x 450 mm; 65 kg;
	Control rack: 650 x 590 x 490 mm; 46 kg
Operating Temperature	-10°C to +35°C
Relative humidity	0-95% non-condensing

2. Aquarius Sensor



Control Rack

Camera

Digitizer

Camera Controller Tablet

Parameter	Specification
Operational altitude	300-600 m AGL
Laser pulse repetition rate	33, 50. 70 kHz
Scan rate	0-70 Hz
Scan half-angle	0 to ± 25 °
Laser footprint on water surface	30-60 cm
Depth range	0 to > 10 m (for k < 0.1/m)
Topographic mode	
Operational altitiude	300-2500
Range Capture	Up to 4 range measurements, including 1st, 2nd, 3rd, and last returns
Intensity capture	12-bit dynamic measurement range
Position and orientation system	POS AVTM 510 (OEM) includes embedded 72-channel GNSS receiver (GPS and GLONASS)
Data Storage	Ruggedized removable SSD hard disk (SATA III)
Power	28 V, 900 W, 35 A
Image capture	5 MP interline camera (standard); 60 MP full frame (optional)
Full waveform capture	12-bit Optech IWD-2 Intelligent Waveform Digitizer (optional)
Dimensions and weight	Sensor:250 x 430 x 320 mm; 30 kg; Control rack: 591 x 485 x 578 mm; 53 kg
Operating temperature	0-35°C
Relative humidity	0-95% no-condensing

3. ITRES TECHNICAL SPECIFICATIONS OF CASI

Sense	or Type					
VNIR Push-broom Sensor						
(Compact Airborne Spectrographic Imager)						
Performance						
Spectral Range (Continuous Coverage)	380-1050 nm					
# Spectral Channels	Up to 288					
#Across-Track Pixels	1500					
Total Field of View	40 deg					
IFOV	0.49 mRad					
t/#	t/3.5					
Spectral Width Sampling Row	2.4 nm					
Spectral Resolution (FWHM)	<3.5 nm					
Pixel Size	20x20 microns					
Dynamic Range	14-bits (16384:1)					
Sustained Date Rate (Mpix/Second)	9.6 Mpix/Sec					
Spectral Smile/Keystone Distortion	±0.35 pixels					
Peak Signal Noise Ration	SNR models for various radiance conditions are available					
Relative humidity	0-95% no-condensing					

Annex 2. NAMRIA Certificates of Reference Points Used

NGW-50

					May 09, 2014
		CEF	RTIFICATION		
whom it i	may concern:				
I NIS IS t	o certify that according	to the records on	file in this office, the requ	uested survey inform	nation is as follows
		Province: NEG	ROS OCCIDENTAL		
		Station N Orde	lame: NGW-50		
Island: VISAYAS		orde	2110	Barangay: FAE	BRICA
wancipa	IN SAGAT	PRS	92 Coordinates		
Latitude:	10° 53' 26.84456"	Longitude:	123° 21' 6.66799"	Ellipsoidal Hgt:	15.38600 m.
		WGS	84 Coordinates		
Latitude:	10° 53' 22.52478"	Longitude:	123° 21' 11.86863"	Ellipsoidal Hgt:	74.42200 m.
		PTI	M Coordinates		
Northing:	1204272.594 m.	Easting:	538465.927 m.	Zone: 4	
lothing	4 000 054 00	UTI	M Coordinates		
Northing:	1,203,851.08	Easting:	538,452.46	Zone: 51	
	the state of the state of the state				
e station is rk is the h of the col questing F bose: Number: I.:	s on the NW sidewalk ead of a 4" copper na ncrete sidewalk with ir Party: UP DREAM Reference 8796117 A 2014-1064	of Himoga-an brid il drilled and groute scriptions "NGW-	ge at km. 73+545 along i d at the center of a 30 x 50; 2007; NAMRIA".	the Sagay-Bacolod 30 cm. cement putt UEL DM. BELEN, N , Mapping And Geod	national highway. ty embedded on / / / / / / / / / / / / / / / / / / /
NGW-58



AB CIP/4701/12/09/814

www.namria.gov.ph

ISO 9001: 2008 CERTIFIED FOR MAPPING AND GEOSPATIAL INFORMATION MANAGEMENT

NGW-63

					May 09,
		CER	TIFICATION		
To whom it may co	oncern:	the records on	file in this office, the requ	lested survey inform	ation is as fall
	ly that according to	Desciones NEO			
		Station N	ame: NGW-63		
		Order	: 2nd		
Island: VISAYA	AS Alatrava			Barangay: LEM	ERY
inano.punty. Or		PRS	92 Coordinates		
Latitude: 10° 3	8' 30.18023"	Longitude:	123° 29' 18.57332"	Ellipsoidal Hgt:	10.15500 r
		WGS	84 Coordinates		
Latitude: 10° 3	8' 25.93535"	Longitude:	123° 29' 23.79491"	Ellipsoidal Hgt:	70.11800 m
		PTI	M Coordinates		
Northing: 1176	744.618 m.	Easting:	553448.18 m.	Zone: 4	
		UTI	W Coordinates	7	
Northing: 1,17	6,332.74	Easting:	553,429.47	Zone: 51	
NGW-63 The station is on th	he NF end of the s	idewalk. It is loca	ated at Daan-Lunsod brid	doe at km.124+077 a	along San
NGW-63 The station is on th Carlos-Bacolod na 4" copper nail drille sidewalk with insci Requesting Party: Pupose: OR Number: T.N.:	he NE end of the s titional highway. Th ed and grouted at riptions "NGW-63; UP DREAM Reference 8796117 A 2014-1067	idewalk. It is loc: le station is abou the center of a 3 2007; NAMRIA"	ated at Daan-Lunsod brid it 10.1 km. from Calatrav 0 x 30 cm. cement putty	dge at km.124+077 a a town proper. Mark embedded on top of UEL DM. BELEN, N , Mapping And Geod	along San is the head o the concrete INSA lesy Branch





NAMRIA OFFICES: Main : Lawton Avenue, Fort Bonifacio, 1634 Taguig City, Philippines Tel. No. (632) 810-4831 to 41 Branch : 421 Barraca SI. San Nicolas, 1010 Manila, Philippines, Tel. No. (632) 241-3494 to 96 www.namria.gov.ph

ISO 9001: 2008 CERTIFIED FOR MAPPING AND GEOSPATIAL INFORMATION MANAGEMENT

Annex 3. Baseline Processing Reports

NW-123

Vector Components (Mark to Mark)

From:	NGW-50						
	Grid		Local		G	lobal	
Easting	538452.463 m	Latitude	N10°53'26.84456"	Latitude		N10°53'22.52478"	
Northing	1203851.077 m	Longitude	E123°21'06.66798"	Longitude		E123°21'11.86863"	
Elevation	13.070 m	Height	15.386 m	Height		74.422 m	
To:	NW-123					-	
	Grid		Local		G	lobal	
Easting	535814.193 m	Latitude	N10°54'55.44186"	Latitude		N10°54'51.11379"	
Northing	1206569.165 m	Longitude	E123°19'39.85826"	Longitude		E123°19'45.05691"	
Elevation	26.999 m	Height	29.378 m	Height		88.296 m	
Vector							
∆Easting	-2638.27	0 m NSFwd Azir	nuth	315°55'13"	ΔX	2477.863 m	
ΔNorthing	2718.08	37 m Ellipsoid Dist	t.	3789.388 m	ΔΥ	1030.277 m	
∆Elevation	13.92	9 m ∆Height		13.992 m	ΔZ	2675.529 m	

Standard Errors

Vector errors:					
σ ΔEasting	0.009 m	σ NS fwd Azimuth	0°00'00"	σΔΧ	0.017 m
σ ΔNorthing	0.003 m	σ Ellipsoid Dist.	0.006 m	σΔΥ	0.024 m
σ ΔElevation	0.029 m	σ∆Height	0.029 m	σΔΖ	0.007 m

Aposteriori Covariance Matrix (Meter²)

	X	Y	Z
x	0.0002973675		
Y	-0.0003341330	0.0005735969	
Z	-0.0000950547	0.0001441364	0.0000468436

2

Vector Components (Mark to Mark)

From:	CBU-327					
	Grid		Local	Global		
Easting	602254.054 m	Latitude	N11°04'30.20546"	Latitude	Global N11*04*25.8 E 123*56*15.5 63.4 Global N11*01*07.1 E 123*55*25.4 75.3 766* ΔX 600.4 0 m ΔY 1828.8	N11°04"25.88935"
Northing	1224362.494 m	Longitude	E123°56'10.33433"	Longitude		E123°56'15.51412"
Elevation	2.863 m	Height	3.541 m	Height		63.573 m
To:	CU-621A					
	Grid		Local		G	lobal
Easting	600754.296 m	Latitude	N11°01'11.40740"	Latitude		N11°01'07.10407*
Northing	1218251.484 m	Longitude	E123°55'20.28492"	Longitude		E123°55'25.46968"
Elevation	15.098 m	Height	15.654 m	Height		75.785 m
Vector						
∆Easting	-1499.75	7 m NS Fwd Azin	nuth	193°58'06"	ΔX	600.402 m
∆Northing	-6111.01	1 m Ellipsoid Dist		6294.070 m	ΔΥ	1828.859 m
∆Elevation	12.23	5 m ∆Height		12.113 m	ΔZ	-5992.519 m

Standard Errors

/ector errors:								
σ ΔEasting	0.002 m	σ NS fwd Azimuth	0°00'00"	σΔΧ	0.004 m			
σ ΔNorthing	0.001 m	σ Ellipsoid Dist.	0.001 m	σΔΥ	0.006 m			
σ ΔElevation	0.007 m	σΔHeight	0.007 m	σΔΖ	0.002 m			

Aposteriori Covariance Matrix (Meter²)

	x	Y	Z
x	0.0000156253		
Y	-0.0000207517	0.0000355938	
Z	-0.0000049255	0.0000086616	0.0000031280

2

Annex 4. The Survey Team

Data Acquisition Component Sub-Team	Designation	Name	Agency/ Affiliation		
PHIL-LIDAR 1	Program Leader	ENRICO C. PARINGIT, D.ENG	UP-TCAGP		
Data Acquisition	Data Component Project	ENGR. CZAR JAKIRI SARMIENTO	UP-TCAGP		
Component Leader	Leader – I	ENGR. LOUIE P. BALICANTA			
	Chief Science Research Specialist (CSRS)	ENGR. CHRISTOPHER CRUZ	UP-TCAGP		
Survey Supervisor	Supervising Science	LOVELY GRACIA ACUÑA	UP-TCAGP		
	Research Specialist (Supervising SRS)	LOVELYN ASUNCION	UP-TCAGP		
	FIE	LD TEAM			
	Senior Science Research	JASMINE ALVIAR			
	Specialist (SSRS)	Specialist (SSRS) CHRISTOPHER JOAQUIN			
LiDAR Operation	Posoarch Associato (PA)	DC ALDOVINO			
	Research Associate (RA)	RENAN PUNTO	UP-ICAGP		
	D۸	MA. VERLINA TONGA,			
	NA	JONALYN GONZALES	UF-TCAGP		
Ground Survey, Data	RΛ	LANCE CINCO			
Download and Transfer		KENNETH QUISADO	UFTCAGE		
	Airborno Socurity	SSG. DAVE GUMBAN	PILIPPINE AIR FORCE		
LiDAR Operation	All bottle Security	SSG. LEE JAY PUNZALAN	(PAF)		
		CAPT. JEFFREY JEREMY ALAJAR;	ASIAN AEROSPACE		
	Dilat	CAPT. RANDY LAGCO	CORPORATION (AAC)		
	Pliot	CAPT. BRYAN DONGUINES	AAC		
		CAPT. JERICHO JECIEL	AAC		



Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1))
--	---

	erner	LOCATION	Z:\DAC\RAW DATA										
	PLAN	KML	14	30	22	38	20	20	22	22			
	FLIGHT	Actual	9	20	40	18	8	80	10	16			
	OPERATOR	(OPLOG) LOPLOG	1KB	NA									
	TION(S)	3ase Info (.txt)	1KB			16							
	BASE STA	BASE STATION(S)	99.1	91	94	100	107	158	90.5	64.6			5 20
		DIGITIZER	101	85.3	6.99	66.5	67.4	23.9	139	55.3	ed by	Bongal served	Con a
		RANGE	13.9	10.2	8.64	10.3	8.59	4	8.33	4.59	Receiv	Vame AC	Signature
IEET 16	MISSION LOG	FILE/CASI LOGS	NA	43	221	248	187	3.23	263	3.7		-1-1	
TRANSFER SH OLOD 5/18/20	DAW	IMAGES/CASI	NA	38.5	39.6	43.4	37.4	9.78	45.3	5.45			
DATA 1 BAC		POS	246	233	222	262	229	143	241	206			
		LOGS	769	663	544	603	502	209	541	320		e	a
	LAS	KML (swath)	343	247	197	240	194	81	191	88	d from	R. PW	all of
	RAW	Output LAS	NA	Receive	Name Position	Signature							
		SENSOR	AQUAICASI	AQUA/CASI	AQUA/CASI	AQUA/CASI	AQUA/CASI	AQUA/CASI	AQUAICASI	AQUA/CASI			
		MISSION NAME	3BLK44AS113A	3BLK44AS114A	3BLK44EDS115A	3BLK44US116A	3BLK46AS117B	3BLK46AS118B	3BLK44FGHS122A	3BLK46AS123A			
		FLIGHT NO.	8453AC	8455AC	8457AC	8459AC	8462AC	8464AC	8471AC	8473AC			
		DATE	April 22,2016	April 23,2016	April 24,2016	April 25,2016	April 26,2016	April 27,2016	May 1,2016	May 2,2016			

Indext Index Index Index <th></th> <th>SERVER</th> <th>CCATION</th> <th>:'Vairborne_</th> <th>:'Vairbome_</th> <th>Z:\Airbome_</th> <th>Z:VAirborne</th> <th>Z:\Airborne_ Raw</th> <th></th> <th></th> <th></th>		SERVER	CCATION	:'Vairborne_	:'Vairbome_	Z:\Airbome_	Z:VAirborne	Z:\Airborne_ Raw			
Index Index <th< td=""><td></td><td>AN</td><td>KML</td><td>NA</td><td>NA R</td><td>NA R</td><td>NA</td><td>NA</td><th></th><td></td><td></td></th<>		AN	KML	NA	NA R	NA R	NA	NA			
Image: Line contract Image: Li		FLIGHT PL	ctual	51	55/53	55	38/30	37			
Name Environ Marconologie		ERATOR	(SOLIG								
Lucr. Inc. MISSION NAME ENNOTINATE MONUTAS Lucr. Inc. MISSION NAME ENNOTINATE MISSION NAME		do (s)	se Info (0	1KB	1KB	1KB	1KB	1KE			
Luerr. No. MISSION NAME ENS/OR RAMIC RA		BASE STATIO	ASE Ba	5.03 1KB	10.4 1KB	10.4 1KB	9.78 1KB	3.45 1KB	+1021		
Literino. Mission name mission name relation Fand for and for sension Constraine and for sension Constraine and for sension Possion and for and for sension Possion and for and			IIZER B STA	17 5	9.3	24	NA	NA	+/8		
Udert vo. Mission NaMel SENSOR RAW LAS Loos(MB) POS RAW Resonance 1725P ILL(477E150A Mission NaMel SENSOR Curput LAS KML Loos(MB) POS Mission Loo 1741P ILL(477E150A Begauus 2.62 1.67 1.33 2.32 46.1 315 23 1747P ILL(451F10A) Begauus 2.62 1.15 7.36 236 23 23 1747P ILL(451F10A) ILL(451F10A) 1.15 7.34 132 236 23 23 1747P ILL(451F10A) Begauus NA 1.18 7.24 132 236 23 ILL(451F10A) ILL(451F10A) Mission 100 7.34 132 114 10 ILL(451F10A) Mission 100 7.36 7.34 132 114 10 ILL(451F10A) Mission 100 7.36 7.34 132 114 10 ILL(451F10A) Mission 100 7.34 132 114 10 Mission 100 Mission 100 Mission 100 132 134 10 ILL(451F10A) Mission 100 7.34 132 114 10 Reserened from				-	3	5	5	- -	PRIET		
Licht Mol Mission Masion Masion Raw LAS Raw LAS Licht Mol Mission NAME Sensor Licht Mol Mission Madescus, Luck 1743P IBLK4/7B190A Pegasus 2.82 1.67 13.3 2.32 44.1 315 1743P IBLK36H203B IBLK36H203B Pegasus 2.82 1.15 7.35 1.70 2.36 2.33 1743P IBLK36H203B Pegasus 1.33 2.27 48.4 365 1743P IBLK36H203B Pegasus 1.33 1.27 2.35 2.31 315 1743P IBLK36H203B Pegasus 1.33 1.32 2.34 1.4 365 1743P IBLK36A203B Pegasus 1.35 1.15 2.35 43.4 365 Pegasus NA 7.06 7.24 192 13.4 144 Name NAMA 7.06 7.24 192 13.8 Pediatus NA 7.06 7.24 192 13.8 Name T.M MANDAM Name Name Name Providion P.A P.A 1.12 1.28 1.33 1.44 Perestored from Name MANDAM		Dog	RANG	26	23.	18	27.	10	The second second		
LIGHT NO. MISSION NAME SENSON NAME Pegasus 2.62 1.67 1.3.8 2.32 4.61 1741P 19LK47B199A Pegasus 2.62 1.67 1.3.8 2.32 4.61 1747P 19LK36H203B Pegasus 1.33 1.15 7.35 170 2.36 1747P 19LK36A204B Pegasus 1.33 1.15 7.35 170 2.36 1747P 2.24 1.5 7.35 1.70 2.36 18LK36A204B Pegasus NA 1.82 7.24 132 1.38 1746P 19LK36A202CAB Pegasus NA 1.82 7.24 132 1.38 NA 708 7.24 132 1.38 Signature TIN ANDAM Feature TIN ANDAM Feature Pesition Signature Position Signature TIN ANDAM Feature TIN ANDAM Feat	16	I NOISSIM	VSI FILE/CA	315	288	243	385	114	In the second se		
LIGHT NO. MISSION NAME LIGHT NO. MISSION NAME 1725P 1741P 1243P 1244P 1244P 1244P 1244P 1244P 1244P 1244P 1244P 1244P 1245P 1244P 1245P 1244P 1245P 1245 1245 124 1245 1245 124 1245 124 1245 124 124 124 124 124 124 124 124		MVG	IMAGES/CP	45.1	40.4	29.6	48.4	13.8	Received Name Position Signature		
LIGHT NO. MISSION NAME SENSOR ANN LAS LOGS(MB) 1725P 1BLK47B199A Pegasus 2.82 1.67 13.8 1741P 1BLK36H203A Pegasus 2.84 1.5 7.35 1743P 1BLK36H203A Pegasus 1.33 1.15 7.35 1743P 1BLK36A204B Pegasus 1.33 1.15 7.35 Pegasus 1.30 7.08 7.24 Received from Name TIN ANDAMA 708 7.24 Name TIN ANDAMA Fegasus 1.28 Pegasus 1.30 7.24 Name TIN ANDAMA			POS	232	036	170	700	192			
LIGHT NO. MISSION NAME SENSOR RAW LAS 1725P 18LK476199A Pegasus 2.82 1.67 1747P 1BLK476199A Pegasus 2.82 1.15 1747P 1BLK36H203B Pegasus 1.93 1.15 1749P 1BLK36A204B Pegasus 1.93 1.15 Pegasus NA 1.82 NA 1.8			LOGS(MB)	13.8		7 95	10.8	7.24			
LIGHT NO. MISSION NAME SENSOR Output LAS 1725P 1BLK47B199A Pegasus 2.62 1741P 1BLK36H203B Pegasus 1.93 1747P 1BLK36A204B Pegasus 1.93 1749P 1BLK36A204B Pegasus 1.93 1749P 1BLK36A204B Pegasus 1.93 Name TI N ANDASA NA Pegasus NA Pegasus NA Pegasus NA Pegasus NA		AS	KML	(swath)	101	2 Y Y		708		5	
LIGHT NO. MISSION NAME SENSOR 1741P 1BLK47B199A Pegasus 1747P 1BLK36H203A Pegasus 1747P 1BLK36A204B Pegasus 1749P 1BLK36A204B Pegasus 1749P 1BLK36A5205A Pegasus Received from Name Pesition TIN ANDAS Signature TIN ANDAS		RAW L	Turtout 1 AS		7.02	2.24	201 V	NA	\$		
Light no. Mission NAME 1741P 1BLK478199A 1 1747P 1BLK36H203B 1 1747P 1BLK36A204B 1 1749P 1BLK36A5204B 1 1749P 1BLK36A5204B 1 Patien 7 Pestion Signature 1			SENSOR		egasus	egasus	egasus	Pegasus	ANDER PAR		
1725P 1741P 1743P 1743P 1749P			MISSION NAME		1BLK47B199A	1BLK36H203A	1BLK36H203B	1BLK36Å204B	Received from Name Position Signature		
			FLIGHT NO.		1725P	1741P	1743P	1747P			

Annex 6. Flight Logs

Flight Log for 1411P Mission

Hight Log No.: /4//	fication: RP-09022	Ime:		U		Mame	W
	6 Aircraft Identi	18 Total Flight 1		BLK44		idar Operator	REA
	5 Aircraft Type: Cesnna T206H	irport, GtV/Province): 10 J 17 Landing:		up and parts of		nd Mined Name	
	214 4 Type: VFR	12 Airport of Arrival (A Baco 16 Take off:		red terk 44		Pilot-in-Comma	Ż
	M Model: Pegasus 3 Mission Name: 18ck 4401	B. PONGUIALS 9 Route: Ba volod port of Departure (Airport, Gty/Province): Bavolo 6 15 15 15 15 15 15 15 15 15 15 15 15 15 1	2H 3+47	ccessful at 1200 m; survey		Acquisition Flight Certified by D-ve D Cert Lan Lan Signature over Printed Name (PAF Representative)	
	1 LiDAR Operator: D. A lo vino 2 ALTA	7 Pilot: J. A Jajar 8 Co-Pilot: 1 10 Date: May 1, 2014 12 Min 13 Engine On: 14 Engine Off	1505 # 185 19 Weather Part /	20 Remarks: Mission Sul	21 Problems and Solutions:	Acquisition Flight Approved by	

Flight Log for 1431P Mission

Flight Log No.: 143	enuncation: Per - C-2014		ght Time:			Printed Name
C Almonth J	o AIICIAILIU		18 Total Fli	_		Lidar Operator
C Aircrafe Turner, Countration	אוורופור ואאבי הבאווופו לחסו	(Airport, City/Province):	17 Landing:			mand A Art of Printed Name
Tuno. VED	DCC.	12 Airport of Arrival	16 Take off:			Pilot-in-Com
under instruction	scondate :	, City/Province):	al Engine Time: 석 + 석 l			ight Certified by Burnbaun Printed Name ntative)
PCACIAC 2 Mice	INET 9 Rout	parture (Airport	15 Tot			Acquisition Fil
Log	8 Co-Pilot: & Donyer	12 Airport of Der	14 Engine Off: 12 + S 1	very cloudy		proved by v. → r ed Name tative)
EAM Data Acquisition Flight	ilot: J. MALAR	Date: MAN C, 2014	Engine On:	Weather	1 Problems and Solutions	Acquisition Flight As Jesening Ol Signature over Print (End User Represent

Flight Log for 1433P Mission



Flight log for 1435P Mission

it Log No.: 1435	20- 0022					
Fligh	6 Aircraft Identification: /		18 Total Flight Time:			Lidar Operator
	5 Aircraft Type: Cesnna T206H	Airport, City/Province):	17 Landing:			mand And And Bernted Name
	4 PS 124 4 Type: VFR	12 Airport of Arrival (16 Take off:	-		Pilot-in-com
	3 Mission Name: 18024	9 Route: N.E. (Airport, City/Province):	15 Total Engine Time:			uisition Flight Certified by
	0 2 ALTM Model: PERPENS	Pilot: B. De Januer 12 Airport of Departure	ngine Off: 18 + D	partly cloudy		Aca Bage
Data Acquisition Flight Log	R Operator: D. Andevin	1. J. ALASTATL 8 CO.	ine On: 14 Er	ather	oblems and Solutions:	Acquisition Flight Approve <u>Jermine</u> <u>Alvien</u> Signature over Printed Mar

			yor			height;		boje					
	Eyesafe:	r name	Ground Surve			Hying	•	in of					
Airport of Departure:	ath: Camera Mission Folds				- · · ·	at 1200m	in Siland	to electron					ED BY: DN: URE: GANSFERRED:
	* Approx. Sw	und Baca Ctation	Units asse Station		in the second of the	hal casson	Dartaye	Veter					RECEIV NAME: POSITI
Ceby	1/2 Scan Angle:	Gro	5		Milei m	no no no no	passion	Please					
5	r Name:		Comment				2						
Scan Fren .	Mission Folde		SPS Status PDOP										
KHZ KHZ	A 8		a SVS										
L PRF:	-		Rng/Ht AGL										
102.6	d Drive		Speed Kts									Suc	D FROM: V: RE: (NSFERRED:
Date: Th/v 23	Set of Har	Weather:	LINE #: Primary POS		2							Problems and Solutio	RECEIVEL NAME:POSITIOA POSITIOA SIGNATUI DATE TRA
1 1 11 31 1 11 31	Date: Thy 23.20 14 PRF: kHz Scan Front us 11. 1.	Date: Th (Y 23, 20) PRF: KHz Scan Freq : Hz 1/2 Scan Angle: Approx. Swath: Set of Hard Drive A B Mission Folder Name: CLBU Camera Mission Folder Name:	Date: U.D.U PRF: Water Mission Folder Name: Date: U.D.U PRF: Write Set of Hard Drive A B Mission Folder Name: Weather: Camera Mission Folder Name: Counce Barrow	Date: Thrify 23 PRF: KHz Scan Freq: Hz J/2 Scan Angle: Approx. Swath: Set of Hard Drive A B Mission Folder Name: Approx. Swath: Camera Mission Folder I Weather: A B Mission Folder Name: Comments Camera Mission Folder I LINE #: Speed Kts Rng/Ht m GPS Status Comments Ground Base Station Primary POS Speed Kts AGL SVS PDOP Comments	Date: Thrify 23 20 Thri KHz Scan Freq : Hz 1/2 Scan Angle: Approx. Swath: Set of Hard Drive A B Mission Folder Name: I/2 Scan Angle: Approx. Swath: Weather:	Date: Thi V 23 20 PRF: kHz Scan Freq : Hz 1/2 Scan Angle: Approx. Swath: Set of Hard Drive A B Mission Folder Name: COBM COBM Comment Weather: A B Mission Folder Name: COBM Comment Camera Mission Folder Name: UNE #: Speed Kis Rng/Ht m GPS Status Comments Comments INNE #: Speed Kis Adit Svs PDOP Comments	Date: Th [y 23 20] th PRF: Htz Scan Freq : Hz J/2 Scan Angle: Approx. Swath: Set of Hard Drive A B Mission Folder Name: Approx. Swath: Cloud Weather: A B Mission Folder Name: Cloud Cloud Cloud UNE #: Speed Kts Rng/Ht m GPS Status Comments Ground Base Station G INE #: Speed Kts Ang Nus Y Y M Status Comments	Date: Th [V 23 20 PRF: Hz Scan Freq : Hz J/2 Scan Angle: Approx. Swath: Set of Hard Drive A B Mission Folder Name: 1/2 Scan Angle: Approx. Swath: Weather: Mission Folder Name: Approx. Swath: Approx. Swath: Approx. Swath: Weather: Speed Kts Rng/Ht m GPS Status Ground Base Station G INE #: Speed Kts Angl Nus Speed Kts Angl Mission Folder Primary POS Speed Kts Angl Nus Status Comments Primary POS Speed Kts PDOP Comments Apple: Primary POS Speed Kts Angl Status Comments Primary POS Speed Kts PDOP Comments Apple: Primary POS Speed Kts PDOP Comments Apple:	Date: Th (v<23,20) PR:: kHz Scan Freq : Hz J2 Scan Angle: Approx. Swath: set of Hard Drive A B Mission Folder Name:	Date: Thily 23 20 PR: ktz Scan freq: Hz 1/2 Scan Angle: Incom Default Set of Hard Drive A B Mission folder Name: 1/2 Scan Angle: Approx. Swath: Weather: Viet B Mission folder Name: Comments Camera Mission folder UNE #: Speed Kts Rng/Ht GPS Status Ground Base Station G UNE #: Speed Kts Rng/Ht GPS Status Comments UNE #: Speed Kts Rng/Ht Superior G UNE #: Speed Kts Rng/Ht Superior G UNA Mission folder Mission folder G Primary POS Speed Kts Rng/Ht Superior Primary POS Speed Kts Comments G Primary POS Speed Kts PDOP Mission folder Primary POS PDOP PDOP PDOP Primary POS PDOP PDOP PDOP Primary POS PDOP PDOP PD	Date: Tult And Description Set of Hard Drive A B Mission Folder Name: A Weather: COLON Mission Folder Name: COLON Weather: A B Mission Folder Name: A INE #: Speed Kis Ring/Ht Ground Base Station Ground Base Station INE #: Speed Kis Ring/Ht Ground Base Station Ground Base Station Primary POS Speed Kis PDP Mission Folder Name: Ground Base Station Primary POS Speed Kis PDP Mission Folder Name: Ground Base Station Primary POS Speed Kis PDP Mission Folder Name: Ground Base Station Ground Base Station	Date: Hulf 23_D0 H PR: Hiz Scan Freq : Hz CLDU Set of Hard Drive A B Mission folder Name: CLDU Approx. swath: Weather: IUNE #: France Approx. Swath: Camera Mission Folder Name: UNE #: Speed Kis Ring/Ht Gers Status Comments UNE #: Speed Kis Ring/Ht Gers Status Comments UNE #: Speed Kis Ring/Ht Gers Status Ground Base Station Of Drivey POS Speed Kis Ring/Ht Status Comments Of Drivey POS Speed Kis Poop Comments Comments Of Drivey POS Speed Kis Poop Comments Comments	Date: Titly 23_200 fr PRI: Kan on the same frequency of the same frequency o

Flight Log for 1745P Mission

Flight Log for 8453AC Mission

1 UDAR Operator: MN	10NG 2 ALTM Modal-A 1 Cr	The second s			Flight Low No Critie -	
7 Pilot: Julyoo 10 Date:	28 Co-Pilot: JRUEL TIA	9 Route:	4 Type: VFR	5 Aircraft Type: Cesnna T206H	6 Aircraft Identification: 923	22
13 FOOD 22, 2016	14 Airport of Departure	Alrport, Oty/Province): 2	? Airport of Arrivel (Ai	(port, Gtv/Provinca)-		
26:2	14 Engine Off: /3. J.)	15 Total Engine Time: 3	Take off: 1	Bruckel		
9 Weather	partys lloudy	44	9:45	13.46	18 Total Flight Time: 7+ 2/	
0 Flight Classification						
O.a Billable Acquisition Flight C Farry Flight O System Bast Flight O Calibration Flight	20.b Non Billable O Aircraft Test Flight O AAC Admin Flight O Others:	20.c Others O LIDAR System Maintenan O Alicraft Maintenance O Phil-LiDAR Admin Activitie	21 Remarks 60Wh6J	sthhing da wind		
Problems and Solutions		t constant				
 Meather Problem System Problem Alrcartt Problem Plot Problem Others: 						
cquisition Flight Aspecored by	Acquisition FlightCertigod	by post the post of the post o	nd MKH0 inted Name	Lidar Openstar Bio 1971 in Day	Aircait Michank/ Technician Signiture over Princed Name	

Flight Log for 8455AC Mission

3 Mission Name 改んしく名化合 4 Type: VFR 5 Alicraft Type: CesnnaT2064 6 Aircraft Identification: 952 2 9 Route:	Lipport, Gity/Prowince): 12 Airport of Arrival (Airport, Gity/Province): 23 Airport, Gity/Province): 23 Airport of Arrival (Airport, Gity/Province): 115 Total Flight Time: 115 Take off: 117 Landing: 1	5153 10.45 HOR 31.43	21 Remarks	20.0 others Completed Buck 44 A and some wids	O LIDAR System Maintenance O Aincraft Maintenance O Phil-LIDAR Admin Activities				ed by Placin Command ' Lidar Operator Aircraft Mechanic/ Technician	Signature over Printed Name Signature over Printed Name Signature over Printed Nama
2 ALTM Model Typus 1003 Mission Name	12 Airport of Departure (Airport, Gty/Provi Beut/od - Cityon (15 Total Engline T	Mr 153		0.b Non Billable 20.c Others	0 Aircrait Text Flight 0 LIDAR Sys 0 AAC Admin Flight 0 Aircrait M 0 Others: 0 Phil-LIDA				Acquisition Fluth, Confried by	Signature cose Printed Name (PAF Representative)
1 LiDAR Operator:]. (Somuch	10 Date: 15, 20 M	19 Weather	20 flight Classification	20.e Billable 21	Acquisition Flight System Yest Flight Calibration Flight Calibration Flight	22 Problems and Solutions	 Weather Problem System Problem 	 Aircraft Problem Pilot Problem Others: 	Acquisition Fight Approved by	Signature cost Plinted Name

Flight Log for 8457AC Mission



Annex 7. Flight Status

		Арш	10 1010 2014 011	4 2010	
FLIGHT NO	AREA	MISSION	OPERATOR	DATE FLOWN	REMARKS
1411P	BLK 44DE	1BLK44D121A	D. Aldovino	May 1, 2014	Mission successful at 1200m; surveyed BLK 44D and parts of BLK 44E
1431P	BLK 44G, BLK 44H, BLK 44F	1BLK44GHS126A	D. Aldovino	May 6, 2014	Mission successful at 800m; filled gaps in BLK 44H and BLK 44G and some parts of BLK 44F
1433P	BLK 44G, BLK 44F	1BLK44FGS126B	R. Punto	May 6, 2014	Mission successful at 800m; filled gaps in BLK 44H; gaps due to diminished overlap (high terrain, low cloud ceiling)
1435P	BLK 44D, 44E, 44F, 44G	1BLk44DS127A	D. Aldovino	May 7, 2014	Mission successful in BLK 44D at 1200m and filled up gaps in BLK 44 at 800m.
1745P	Bantayan Island	1BTYN204A	G. Sinadjan	July 23, 2016	Surveyed Bantayan at 1200m
8453AC	BLK44As Himogaan, Himogaan FP	3BLK44AS113A	V. TONGA	APR 22, 2016	SURVEYED PARTS OF BLK44AS
8455AC	BLK44As Himogaan, Himogaan FP	3BLK44As114A	J. GONZALES	APR 23, 2016	SURVEYED REST OF BLK44AS
8457AC	BLK44IS, BLK44JS	3BLK44IJS116A	J. GONZALES	APR 25	SURVEYED BLK44IS AND BLK- 44JS

FLIGHT STATUS REPORT HIMOGAAN April to May 2014 and 2016

LAS/SWATH BOUNDARIES PER MISSION FLIGHT

1411P
BLK 44DE
1BLK44D121A
356.01 sq.km.



Flight No. :	1415P
Area:	BLK 44H
Mission Name:	1BLK44H122A
Area Surveyed:	371.6 sq.km



Flight No. : Area: Mission Name: Area Surveyed: 1431P BLK 44G, 44H, 44F 1BLK44GHS126A 230.5 sq.km



Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)

Flight No. :
Area:
Mission Name:
Area Surveyed:

1433P BLK 44G, 44F 1BLKFGS126B 204.44 sq.km.



 Flight No.:
 1435P

 Area:
 BLK 44D, 44E, 44F, 44G

 Mission Name:
 1BLK44DS127A

 Area Surveyed:
 139.55 sq.km new area; 131.307 gap filling



Flight No. :8453ACArea:BLK44ASMission Name:3BLK44As113AParameters:Altitude: 500m; Scan Frequency: 45; Scan Angle: 18; Overlap: 30 %; PRF: 50kHzTotal Area Surveyed:98.3 sq km



Flight No. :8455ACArea:BLK44ASMission Name:3BLK44AS114AParameters:Altitude: 500m; Scan Frequency: 45; Scan Angle: 18; Overlap: 30%; PRF: 50kHzTotal Area Surveyed:35 sq km



Flight No. :8459ACArea:BLK44IS, BLK44JSMission Name:3BLK44IJS116AParameters:Altitude: 500m; Scan Frequency: 45; Scan Angle: 18; Overlap: 50 %; PRF: 50kHzTotal Area Surveyed:70 sq km



Flight Area	Negros				
Mission Name	Blk44D				
Inclusive Flights	1411P, 1435P				
Range data size	75.2 GB				
POS	728 MB				
Base data size	13.88 MB				
Image	31.5 GB				
Transfer date	May 26, 2014				
Solution Status					
Number of Satellites (>6)	Yes				
PDOP (<3)	Yes				
Baseline Length (<30km)	Yes				
Processing Mode (<=1)	No				
Smoothed Performance Metrics (in cm)					
RMSE for North Position (<4.0 cm)	1.04				
RMSE for East Position (<4.0 cm)	1.26				
RMSE for Down Position (<8.0 cm)	2.51				
Boresight correction stdev (<0.001deg)	0.000446				
IMU attitude correction stdev (<0.001deg)	0.005774				
GPS position stdev (<0.01m)	0.0134				
Minimum % overlap (>25)	27.44%				
Ave point cloud density per sq.m. (>2.0)	3.51				
Elevation difference between strips (<0.20 m)	Yes				
Number of 1km x 1km blocks	552				
Maximum Height	395.70 m				
Minimum Height	50.84 m				
Classification (# of points)					
Ground	387,844,370				
Low vegetation	324,638,606				
Medium vegetation	458,253,579				
High vegetation	120,361,293				
Building	9,453,151				
Orthophoto	Yes				
Processed by	Engr. Jommer Medina, Engr. Carlyn Ann Ibañez, Engr. Melanie Hingpit, Engr. Gladys Mae Apat				

Annex 8. Mission Summary Report



Figure 1.1.1 Solution Status



Figure 1.1.2 Smoothed Performance Metric Parameters



Figure 1.1.3 Best Estimated Trajectory



Figure 1.1.4 Coverage of LiDAR data



Figure 1.1.5 Image of data overlap



Figure 1.1.6 Density map of merged LiDAR data



Figure 1.1.7 Elevation difference between flight lines

Flight Area	Negros				
Mission Name	Blk44FG				
Inclusive Flights	1431P, 1433P, 1435P				
Range data size	105.7 GB				
POS	810 MB				
Base data size	35.94 MB				
Image	110.3 GB				
Transfer date	May 26, 2014				
Solution Status					
Number of Satellites (>6)	Yes				
PDOP (<3)	Yes				
Baseline Length (<30km)	Yes				
Processing Mode (<=1)	Yes				
Smoothed Performance Metrics (in cm)					
RMSE for North Position (<4.0 cm)	1.24				
RMSE for East Position (<4.0 cm)	1.41				
RMSE for Down Position (<8.0 cm)	2.62				
Boresight correction stdev (<0.001deg)	0.000248				
IMU attitude correction stdev (<0.001deg)	0.001112				
GPS position stdev (<0.01m)	0.0062				
Minimum % overlap (>25)	43.01%				
Ave point cloud density per sq.m. (>2.0)	9.26				
Elevation difference between strips (<0.20 m)	Yes				
Number of 1km x 1km blocks	347				
Maximum Height	584.11 m				
Minimum Height	72.76 m				
Classification (# of points)					
Ground	445,025,694				
Low vegetation	463,475,098				
Medium vegetation	838,129,177				
High vegetation	234,468,284				
Building	6,471,602				
Orthophoto	Yes				
Processed by	Engr. Carlyn Ann Ibañez, Engr. Christy Lubiano, Engr. Gladys Mae Apat				



Figure 1.2.1 Solution Status



Figure 1.2.2 Smoothed Performance Metric Parameters



Figure 1.2.3 Best Estimated Trajectory



Figure 1.2.4 Coverage of LiDAR data



Figure 1.2.5 Image of data overlap



Figure 1.2.6 Density map of merged LiDAR data

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)



Figure 1.2.7 Elevation difference between flight lines
Flight Area	Bacolod
Mission Name	Block 44E
Inclusive Flights	8453AC
Range data size	13.9 GB
POS data size	246 MB
Base data size	99.1 MB
Image	n/a
Transfer date	May 20, 2016
Solution Status	
Number of Satellites (>6)	No
PDOP (<3)	No
Baseline Length (<30km)	Yes
Processing Mode (<=1)	No
Smoothed Performance Metrics (in cm)	
RMSE for North Position (<4.0 cm)	2.002
RMSE for East Position (<4.0 cm)	1.603
RMSE for Down Position (<8.0 cm)	5.037
Boresight correction stdev (<0.001deg)	0.000258
IMU attitude correction stdev (<0.001deg)	0.000791
GPS position stdev (<0.01m)	0.0016
Minimum % overlap (>25)	30.04
Ave point cloud density per sq.m. (>2.0)	3.95
Elevation difference between strips (<0.20 m)	Yes
Number of 1km x 1km blocks	139
Maximum Height	578.38
Minimum Height	60.03
Classification (# of points)	
Ground	93,527,454
Low vegetation	98,324,857
Medium vegetation	111,788,117
High vegetation	66,668,017
Building	3,363,991
Orthophoto	
Processed by	Engr. Sheila-Maye Santillan, Engr. Merven Natino, Engr. Elainne Lopez



Figure 1.3.1 Solution Status



Figure 1.3.2 Smoothed Performance Metric Parameters



Figure 1.3.3 Best Estimated Trajectory



Figure 1.3.4 Coverage of LiDAR Data



Figure 1.3.5 Image of data overlap



Figure 1.3.6. Density map of merged LiDAR data



Figure 1.3.7. Elevation difference between flight lines

Flight Area	Bacolod
Mission Name	Block 44E additional
Inclusive Flights	8455AC
Range data size	10.2 GB
POS data size	233 MB
Base data size	91 MB
Image	38.5 GB
Transfer date	May 20, 2016
Solution Status	
Number of Satellites (>6)	Yes
PDOP (<3)	No
Baseline Length (<30km)	Yes
Processing Mode (<=1)	Yes
Smoothed Performance Metrics (in cm)	
RMSE for North Position (<4.0 cm)	1.245
RMSE for East Position (<4.0 cm)	1.87
RMSE for Down Position (<8.0 cm)	4.065
Boresight correction stdev (<0.001deg)	0.000218
IMU attitude correction stdev (<0.001deg)	0.004166
GPS position stdev (<0.01m)	0.0027
Minimum % overlap (>25)	41.20
Ave point cloud density per sq.m. (>2.0)	4.92
Elevation difference between strips (<0.20 m)	Yes
Number of 1km x 1km blocks	120
Maximum Height	387.49
Minimum Height	59.77
Classification (# of points)	
Ground	53,625,771
Low vegetation	63,815,686
Medium vegetation	72,382,824
High vegetation	55,860,054
Building	2,859,236
Orthophoto	None
Processed by	Engr. Sheila-Maye Santillan, Engr. Edgardo Gubatanga, Jr., Engr. Melissa Fernandez



Figure 1.4.1 Solution Status



Figure 1.4.2 Smoothed Performance Metric Parameters



Figure 1.4.3 Best Estimated Trajectory



Figure 1.4.4 Coverage of LiDAR Data



Figure 1.4.5 Image of data overlap



Figure 1.4.6 Density map of merged LiDAR data



Figure 1.4.7 Elevation difference between flight lines

Flight Area	Bacolod
Mission Name	Block 44D
Inclusive Flights	8457AC
Range data size	8.64 GB
POS data size	222 MB
Base data size	94 MB
Image	39.6
Transfer date	May 20, 2016
Solution Status	
Number of Satellites (>6)	Yes
PDOP (<3)	No
Baseline Length (<30km)	No
Processing Mode (<=1)	No
Smoothed Performance Metrics (in cm)	
RMSE for North Position (<4.0 cm)	1.2
RMSE for East Position (<4.0 cm)	1.204
RMSE for Down Position (<8.0 cm)	5.78
Boresight correction stdev (<0.001deg)	0.000478
IMU attitude correction stdev (<0.001deg)	0.000940
GPS position stdev (<0.01m)	0.0025
Minimum % overlap (>25)	30.10
Ave point cloud density per sq.m. (>2.0)	3.33
Elevation difference between strips (<0.20 m)	Yes
Number of 1km x 1km blocks	48
Maximum Height	106.51
Minimum Height	57.85
Classification (# of points)	
Ground	11,374,042
Low vegetation	10,746,942
Medium vegetation	12,511,682
High vegetation	8,971,525
Building	2,031,597
Orthophoto	None
Processed by	Engr. Irish Cortez, Engr. Melanie Hingpit, Engr. Monalyne Rabino



Figure 1.5.1 Solution Status



Figure 1.5.2 Smoothed Performance Metric Parameters



Figure 1.5.3 Best Estimated Trajectory



Figure 1.5.4 Coverage of LiDAR Data



Figure 1.5.5 Image of data overlap



Figure 1.5.6 Density map of merged LiDAR data



Figure 1.5.7 Elevation difference between flight lines

Ś
Ð
et.
ž
ar
Ľ
Å
2
SI.
a
<u> </u>
Ð
Z
ž
an
a
Q
ğ
I.
6
×
Ø

	Ratio to Peak	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65
	Thres- hold Type	Ratio to Peak																								
າ Baseflow	Recession Constant	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9
Recession	Initial Discharge (M3/S)	2.3002	0.0775488	3.8044	12.709	1.4654	2.73	0.3769	4.4211	3.9555	3.0008	1.0173	5.3266	1.8902	5.1452	0.23029	2.7996	1.6831	2.3262	2.6923	1.9621	0.93965	0.23682	0.81368	2.029	1.0656
	Initial Type	Discharge																								
ydrograph orm	Storage Coefficient (HR)	0.57503	0.13161	0.70325	3.1251	0.59151	1.691	0.25233	0.84027	4.3865	2.7261	0.18564	2.6333	0.6831	2.1354	0.13112	4.7521	0.45582	5.007	2.2699	3.4549	2.5326	0.16841	0.40598	1.1763	3.4313
Clark Unit H Transi	Time of Concen- tration (HR)	2.5545	0.28756	0.97479	2.7907	1.1124	0.32619	1.7611	6.0123	8.9884	1.6718	1.9047	3.4106	0.92465	3.5644	0.42111	2.9141	4.8695	6.9047	0.95434	1.4469	2.3461	0.79966	4.3371	0.75308	2.757
OSS	Imper- vious (%)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
ve Number L	Curve Number	87.646	66	97.02	95.818	97.223	66	66	96.706	98.832	98.93	66	97.333	96.524	66	66	98.772	95.559	66	98.627	66	66	66	66	39.382	66
SCS Curv	Initial Abstraction (mm)	0.0154555	0.0155	0.0287197	0.0352893	0.0155	0.0163968	0.0155	0.0155	0.0155	0.0713777	0.0155	0.0703753	0.0155	0.024235	0.0155	0.0164458	0.0162888	0.047173	0.0291891	0.10276	0.0959578	0.0155	0.0155	0.1069	0.12166
	Basin Number	W480	W490	W500	W510	W520	W530	W540	W550	W560	W570	W580	W590	W600	W610	W620	W630	W640	W650	W660	W670	W680	W690	W700	W710	W720

0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65
Ratio to Peak																					
6.0	6.0	6'0	6'0	6'0	6.0	6.0	6'0	6'0	6'0	6.0	6.0	6.0	6.0	0.9	0.9	0.9	6.0	0.9	0.9	0.9	6.0
7.4228	0.0195923	4.1024	3.0597	6.3949	2.0837	1.3435	0.88101	2.904	2.9869	4.1331	2.1194	1.4292	4.5768	0.0353209	0.6844	3.8858	6.5112	3.1206	3.296	2.7609	2.0504261
Discharge																					
4.4558	0.13864	2.7393	5.5169	3.7924	3.2164	0.43765	2.6305	3.0198	3.0171	3.5726	3.381	2.5931	5.0626	0.11769	0.74072	3.8026	2.8863	2.9682	2.4949	1.7502	1.8853
7.3207	0.30291	3.0488	2.6593	5.1042	3.9132	3.1321	1.622	4.1672	2.2041	5.3931	1.4123	1.5914	5.1739	0.25325	1.1217	1.5162	4.3775	0.53179	3.0783	1.1596	1.1331
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
95.136	66	98.803	97.875	97.629	89.132	92.778	98.366	86.601	90.014	85.877	86.797	98.206	97.968	98.06	66	90.296	88.133	66	95.954	88.647	66
0.0879324	0.0155	0.10871	0.0702108	0.020799	0.1086274	0.0155	0.0442372	0.11456	0.1123537	0.12007	0.11091	0.0233456	0.0318954	0.0814581	0.0416304	0.12579	0.11233	0.0369628	0.0355	0.10578	0.1073651
W730	W740	W750	W760	W770	W780	067W	W800	W810	W820	W830	W840	W850	W860	W870	W880	W890	006M	W910	W920	W930	W940

Reach Number		Mus	skingum Cunge	Channel Routing			
Number	Time Step Method	Length (m)	Slope	Manning's n	Shape	Width	Side Slope
R10	Automatic Fixed Interval	5818.97	0.001019	0.0409744	Trapezoid	75.48	1
R20	Automatic Fixed Interval	333.848	0.004958	0.0407784	Trapezoid	75.48	1
R30	Automatic Fixed Interval	2326.81	0.007981	0.0403754	Trapezoid	75.48	1
R50	Automatic Fixed Interval	1731.25	0.006182	0.0608454	Trapezoid	75.48	1
R90	Automatic Fixed Interval	9737.03	0.020112	0.0908368	Trapezoid	75.48	1
R100	Automatic Fixed Interval	7596.37	0.005574	0.0883801	Trapezoid	75.48	1
R120	Automatic Fixed Interval	2097.94	0.006663	0.0891	Trapezoid	75.48	1
R150	Automatic Fixed Interval	962.548	0.008648	0.0906639	Trapezoid	75.48	1
R170	Automatic Fixed Interval	3644.34	0.015614	0.14234	Trapezoid	75.48	1
R190	Automatic Fixed Interval	5164.87	0.020032	0.0874535	Trapezoid	75.48	1
R200	Automatic Fixed Interval	5198.72	0.011111	0.0588148	Trapezoid	75.48	1
R210	Automatic Fixed Interval	1087.4	0.003816	0.0602832	Trapezoid	75.48	1
R230	Automatic Fixed Interval	1713.68	0.041131	0.0884677	Trapezoid	75.48	1
R240	Automatic Fixed Interval	2103.09	0.031525	0.0600594	Trapezoid	75.48	1
R250	Automatic Fixed Interval	442.426	0.015362	0.0592017	Trapezoid	75.48	1
R260	Automatic Fixed Interval	2612.79	0.008366	0.0395608	Trapezoid	75.48	1
R300	Automatic Fixed Interval	3028.36	0.021735	0.0403847	Trapezoid	75.48	1
R310	Automatic Fixed Interval	4148.65	0.020545	0.0401911	Trapezoid	75.48	1
R340	Automatic Fixed Interval	3660.9	0.01293	0.0591948	Trapezoid	75.48	1
R380	Automatic Fixed Interval	5135	0.019052	0.0350633	Trapezoid	75.48	1
R390	Automatic Fixed Interval	279.706	0.038434	0.0393473	Trapezoid	75.48	1
R410	Automatic Fixed Interval	2198.82	0.015092	0.0599762	Trapezoid	75.48	1
R420	Automatic Fixed Interval	6037.01	0.035476	0.0402832	Trapezoid	75.48	1

Annex 10. Himogaan Model Reach Parameters

Annex 11. Himogaan-Tanao Field Validation

Point	Validatior	n Coordinates	Model	Vali- dation			Rain
Num- ber	Lat	Long	var (m)	Points (m)	Error	Event/Date	Return / Scenario
1	10.89304	123.4049171	3.49	5	2.2801	Undang/November 5-7, 1985	100-Year
2	10.88665	123.3956462	1.08	5	15.3664	Undang/November 5-7, 1986	100-Year
3	10.88706	123.3956749	0.95	5	16.4025	Undang/November 5-7, 1987	100-Year
4	10.88671	123.3956508	3.17	5	3.3489	Undang/November 5-7, 1988	100-Year
5	10.88675	123.3961603	0.00	3	9	Ruping/November 13-18, 1990	100-Year
6	10.89284	123.4048072	4.03	5	0.9409	Undang/November 5-7, 1989	100-Year
7	10.8866	123.3956406	1.97	5	9.1809	Undang/November 5-7, 1990	100-Year
8	10.88644	123.3964139	0.30	5	22.09	Undang/November 5-7, 1991	100-Year
9	10.88685	123.3961504	1.78	3	1.4884	Ruping/November 13-18, 1991	100-Year
10	10.89264	123.4047981	0.05	5	24.5025	Undang/November 5-7, 1992	100-Year
11	10.88679	123.395619	0.24	5	22.6576	Undang/November 5-7, 1993	100-Year
12	10.88678	123.395511	1.84	5	9.9856	Undang/November 5-7, 1994	100-Year
13	10.88679	123.3957428	1.98	3	1.0404	Ruping/November 13-18, 1992	100-Year
14	10.89333	123.4049507	1.62	3	1.9044	Ruping/November 13-18, 1993	100-Year
15	10.89323	123.4049247	0.03	3	8.8209	Ruping/November 13-18, 1994	100-Year
16	10.89268	123.4047117	0.39	3	6.8121	Ruping/November 13-18, 1995	100-Year
17	10.89289	123.4048491	0.59	5	19.4481	Undang/November 5-7, 1995	100-Year
18	10.88686	123.3957575	0.26	5	22.4676	Undang/November 5-7, 1996	100-Year
19	10.88656	123.3963104	0.74	5	18.1476	Undang/November 5-7, 1997	100-Year
20	10.88494	123.4104032	0.59	0.75	0.0256	Yolanda/ November 2-11, 2013	5-Year
21	10.89096	123.357543	0.6	3	5.76	Yolanda/ November 2-11, 2013	5-Year
22	10.88607	123.4179368	1.39	0	1.9321		5-Year
23	10.89276	123.4133247	2.46	0	6.0516		5-Year
24	10.8828	123.3463334	0.00	0	0		5-Year
25	10.89703	123.4134465	2.17	0	4.7089		5-Year
26	10.89627	123.3590016	0.03	0	0.0009		5-Year
27	10.8868	123.3485264	0.00	0	0		5-Year
28	10.88362	123.3492893	0.00	0	0		5-Year
29	10.89705	123.4145236	0.00	0.2	0.04	Yolanda/ November 2-11, 2013	5-Year
30	10.88689	123.4107982	0.23	0	0.0529	Yolanda/ November 2-11, 2013	5-Year
31	10.88372	123.4107134	10.23	0	104.6529		5-Year
32	10.88471	123.4146668	5.62	0	31.5844		5-Year
33	10.88612	123.4161576	5.67	0	32.1489		5-Year
34	10.89088	123.4108827	0.14	0	0.0196		5-Year
35	10.88573	123.3495022	5.37	0	28.8369		5-Year
36	10.89633	123.3609441	0.04	0	0.0016		5-Year
37	10.89118	123.3577763	1.08	3	3.6864	Yolanda/ November 2-11, 2013	5-Year
38	10.89884	123.3622023	0.03	0	0.0009		5-Year
39	10.89628	123.3627223	0.06	0	0.0036		5-Year
40	10.89005	123.4133036	5.23	0.3	24.3049	Yolanda/ November 2-11, 2013	5-Year
41	10.94794	123.4139833	0.05	0	0.0025	. ,	5-Year
42	10.88898	123.4135544	0.00	0	0		5-Year
43	10.93673	123.4201519	0.76	0.6	0.0256	Marce/November 24 -28. 2016	5-Year
44	10.89043	123.4125809	6.5	0.2	39.69	Yolanda/ November 2-11. 2013	5-Year
45	10.89063	123.4128556	5.71	0.2	30.3601	Yolanda/ November 2-11, 2013	5-Year

46	10.88668	123.4128659	2.58	0	6.6564		5-Year
47	10.89215	123.4154028	4.75	0	22.5625		5-Year
48	10.93655	123.4206146	0.03	0.6	0.3249	Marce/November 24 -28, 2016	5-Year
49	10.88829	123.4136962	5.62	0	31.5844		5-Year
50	10.89798	123.4144229	5.71	0.2	30.3601	Yolanda/ November 2-11, 2013	5-Year
51	10.89053	123.4130661	6.06	0.2	34.3396	Yolanda/ November 2-11, 2013	5-Year
52	10.93826	123.4266992	0.14	0	0.0196		5-Year
53	10.88767	123.3510572	0.03	0.5	0.2209	Yolanda/ November 2-11, 2013	5-Year
54	10.94281	123.4271363	0.03	1	0.9409	Marce/November 24 -28, 2016	5-Year
55	10.94779	123.4144961	0.54	0	0.2916		5-Year
56	10.89166	123.4150796	1.37	0	1.8769		5-Year
57	10.88746	123.4138217	4.44	0	19.7136		5-Year
58	10.88362	123.3495837	0.00	0	0		5-Year
59	10.88819	123.4135659	4.95	0	24.5025		5-Year
60	10.94931	123.4117194	0.1	1	0.81	Yolanda/ November 2-11, 2013	5-Year
61	10.94866	123.415151	0.72	0	0.5184		5-Year
62	10.94504	123.419977	0.03	0.3	0.0729	Yolanda/ November 2-11, 2013	5-Year
63	10.89353	123.4142786	0.03	0	0.0009		5-Year
64	10.88829	123.4137663	2.73	0	7.4529		5-Year
65	10.94956	123.4118795	0.05	1.5	2.1025	Yolanda/ November 2-11, 2013	5-Year
66	10.94901	123.4124439	0.03	1	0.9409	Yolanda/ November 2-11, 2013	5-Year
67	10.88985	123.4138047	0.00	0.5	0.25	Yolanda/ November 2-11, 2013	5-Year
68	10.89388	123.4141792	5.12	0	26.2144		5-Year
69	10.94486	123.4127808	0.1	2	3.61	Yolanda/ November 2-11, 2013	5-Year
70	10.9471	123.4128954	0.21	1	0.6241	Yolanda/ November 2-11, 2013	5-Year
71	10.94125	123.4250748	0.03	0	0.0009		5-Year
72	10.93804	123.4228981	0.03	0.8	0.5929	Marce/November 24 -28, 2016	5-Year
73	10.89136	123.3540596	0.03	2.5	6.1009	Senyang/December 28-30, 2014	5-Year
74	10.94379	123.4243637	0.03	1	0.9409	Marce/November 24 -28, 2016	5-Year
75	10.94798	123.4126136	0.00	1.5	2.25	Yolanda/ November 2-11, 2013	5-Year
76	10.94448	123.4226574	0.12	1	0.7744	Yolanda/ November 2-11, 2013	5-Year
77	10.94873	123.411936	0.56	0	0.3136		5-Year
78	10.94538	123.4124247	0.37	0.35	0.0004	Yolanda/ November 2-11, 2013	5-Year
79	10.89627	123.4128828	0.03	0	0.0009		5-Year
80	10.94769	123.4121133	0.16	1.5	1.7956	Yolanda/ November 2-11, 2013	5-Year
81	10.88862	123.4145798	3.45	0.15	10.89	Yolanda/ November 2-11, 2013	5-Year
82	10.93814	123.4265406	0.09	0	0.0081		5-Year
83	10.88516	123.3463296	0.00	0	0		5-Year
84	10.93711	123.4205947	0.55	0.6	0.0025	Marce/November 24 -28, 2016	5-Year
85	10.93403	123.4220335	0.04	0.65	0.3721	Yolanda/ November 2-11, 2013	5-Year
86	10.93393	123.4223241	1.18	0.65	0.2809	Yolanda/ November 2-11, 2013	5-Year
87	10.94984	123.411379	0.05	1	0.9025	Yolanda/ November 2-11, 2013	5-Year
88	10.88415	123.3511928	0.00	0	0		5-Year
89	10.9476	123.413034	0.03	1.5	2.1609	Yolanda/ November 2-11, 2013	5-Year
90	10.88392	123.353926	0.67	1.5	0.6889	Ruby/December 6-7, 2014	5-Year
91	10.93823	123.4230217	0.03	0.8	0.5929	Marce/November 24 -28, 2016	5-Year
92	10.94181	123.4262827	0.09	1	0.8281	Yolanda/ November 2-11, 2013	5-Year
93	10.94222	123.4269669	0.03	1	0.9409	Marce/November 24 -28, 2016	5-Year
94	10.94785	123.4121691	0.25	1.5	1.5625	Yolanda/ November 2-11, 2013	5-Year
95	10.94717	123.4133356	0.04	0	0.0016		5-Year

96	10.94743	123.4133695	0.31	0	0.0961		5-Year
97	10.94449	123.4205476	0.00	0.3	0.09	Yolanda/ November 2-11, 2013	5-Year
98	10.8908	123.3542476	4.66	2	7.075599	Ruping/November 13-18, 1996	100-Year
99	10.94782	123.4125584	0.24	0	0.0576		5-Year
100	10.94669	123.4109516	0.30	2	2.89	Sig #3/November 5-7, 1984	5-Year
101	10.94582	123.4137397	0.03	0	0.0009		5-Year
102	10.94898	123.4101126	0.03	0	0.0009		5-Year
103	10.94556	123.414017	0.06	0	0.0036		5-Year
104	10.94657	123.4102076	0.67	0	0.4489		5-Year
105	10.94168	123.4191304	0.26	2	3.0276	Yolanda/ November 2-11, 2013	5-Year
106	10.94083	123.4202902	0.47	2	2.3409	Yolanda/ November 2-11, 2013	5-Year
107	10.89189	123.3577537	1.21	3	3.2041	Yolanda/ November 2-11, 2013	5-Year
108	10.9455	123.4114517	0.64	0	0.4096		5-Year
109	10.94693	123.4125658	1.12	0	1.2544		5-Year
110	10.94939	123.4121342	0.68	1	0.1024	Yolanda/ November 2-11, 2013	5-Year
111	10.94532	123.4145939	0.03	0	0.0009		5-Year
112	10.94217	123.4266381	0.03	1	0.9409	Yolanda/ November 2-11, 2013	5-Year
113	10.94568	123.4247056	0.03	1	0.9409	Marce/November 24 -28, 2016	5-Year
114	10.88547	123.3529407	0.00	0	0		5-Year
115	10.94778	123.4110035	0.03	0.6	0.3249	Yolanda/ November 2-11, 2013	5-Year
116	10.94503	123.4194403	0.47	0.3	0.0289	Yolanda/ November 2-11, 2013	5-Year
117	10.94869	123.4091837	1.09	0	1.1881		5-Year
118	10.9408	123.4198035	0.03	2	3.8809	Yolanda/ November 2-11, 2013	5-Year
119	10.94689	123.4135927	0.03	1	0.9409	Yolanda/ November 2-11, 2013	5-Year
120	10.9431	123.4242639	0.76	1	0.0576	Marce/November 24 -28, 2016	5-Year
121	10.94663	123.4141144	1.23	1	0.0529	Yolanda/ November 2-11, 2013	5-Year
122	10.88535	123.3536215	0.00	0	0		5-Year
123	10.94103	123.4205604	0.85	2	1.3225	Yolanda/ November 2-11, 2013	5-Year
124	10.94587	123.4126984	0.03	0.35	0.1024	Yolanda/ November 2-11, 2013	5-Year
125	10.88297	123.3536586	3.19	1.5	2.8561	Ruby/December 6-7, 2014	5-Year
126	10.9455	123.4112715	0.51	0	0.2601		5-Year
127	10.947	123.4134435	0.73	1	0.0729	Yolanda/ November 2-11, 2013	5-Year
128	10.94695	123.4143944	0.8	1	0.04	Yolanda/ November 2-11, 2013	5-Year
129	10.94077	123.4209853	0.97	2	1.0609	Yolanda/ November 2-11, 2013	5-Year
130	10.89127	123.3507638	0.06	0	0.0036	Frank/June 18-23, 2008	100-Year
131	10.94646	123.409658	1.09	0	1.1881		5-Year
132	10.94662	123.4123274	0.84	0	0.7056		5-Year
133	10.94694	123.4114504	1.08	1.5	0.1764	Yolanda/ November 2-11, 2013	5-Year
134	10.94881	123.4094301	0.67	0	0.4489		5-Year
135	10.94613	123.4142009	0.97	1	0.0009	Yolanda/ November 2-11, 2013	5-Year
136	10.94109	123.4190218	0.89	2	1.2321	Yolanda/ November 2-11, 2013	5-Year
137	10.89125	123.3570098	3.07	3	0.0049	Yolanda/ November 2-11, 2013	5-Year
138	10.8848	123.3539152	0.51	1.5	0.9801	Ruby/December 6-7, 2014	5-Year
139	10.88527	123.3551674	0.47	0	0.2209		5-Year
140	10.8866	123.354211	1.36	0	1.8496		5-Year
141	10.89279	123.3549387	0.03	0.2	0.0289	Yolanda/ November 2-11, 2013	5-Year
142	10.88906	123.3534196	1.37	0	1.8769		5-Year
143	10.88613	123.3536963	0.11	0	0.0121		5-Year
144	10.88834	123.3536729	3.16	0	9.985601		5-Year
145	10.89299	123.3564838	0.05	0.2	0.0225	Yolanda/ November 2-11, 2013	5-Year

146	10.88535	123.3545947	0.00	0.3	0.09	Ondoy/September 24-30, 2009	5-Year
147	10.89117	123.3509395	0.04	0	0.0016	Frank/June 18-23, 2008	100-Year
148	10.88769	123.3547796	1.69	2	0.0961		5-Year
149	10.89275	123.3545688	0.04	0.2	0.0256	Yolanda/ November 2-11, 2013	5-Year
150	10.8828	123.3540693	0.92	1.5	0.3364	Ruby/December 6-7, 2014	5-Year
151	10.87203	123.3459072	0.21	5	22.9441	Yolanda/ November 2-11, 2013	5-Year
152	10.88474	123.3552168	2.02	0	4.0804		5-Year
153	10.88795	123.3549578	1.48	0	2.1904		5-Year
154	10.88947	123.3511989	0.13	8	61.9369	Ruping/November 13-18, 1997	100-Year
155	10.88835	123.3529977	1.87	0	3.4969		5-Year
156	10.8897	123.3518951	0.65	6.00	28.6225	Yolanda/ November 2-11, 2013	5-Year
157	10.88832	123.3548094	1.78	0	3.1684		5-Year
158	10.88597	123.3557111	1.73	5	10.6929	Luding/August 8 – August 18,	5-Year
159	10.87262	123.345349	0.21	0.6	0.1521	Ruby/December 6-7, 2014	5-Year
160	10.88441	123.3536771	1.05	1.5	0.2025	Ruby/December 6-7, 2014	5-Year
161	10.87179	123.3459513	0.03	5	24.7009	Yolanda/ November 2-11, 2013	5-Year
162	10.88495	123.3553053	0.88	0	0.7744		5-Year
163	10.89071	123.3538806	0.59	2.50	3.6481	Yolanda/ November 2-11, 2013	5-Year
164	10.88782	123.3552082	4.02	0	16.1604		5-Year
165	10.88772	123.3541393	0.00	2	4	Yolanda/ November 2-11, 2013	5-Year
166	10.88548	123.3540685	0.08	0.3	0.0484	Ondoy/September 24-30, 2009	5-Year
167	10.88856	123.3552818	3.04	0	9.2416		5-Year
168	10.89271	123.3566393	0.06	0.2	0.0196	Yolanda/ November 2-11, 2013	5-Year
169	10.88339	123.3543612	0.03	1.5	2.1609	Ruby/December 6-7, 2014	5-Year
170	10.89154	123.3530177	0.05	4	15.6025	Yolanda/ November 2-11, 2013	5-Year
171	10.89266	123.3543278	0.04	0.2	0.0256	Yolanda/ November 2-11, 2013	5-Year
172	10.88496	123.3553005	0.00	0	0		5-Year
173	10.86769	123.3447925	3.34	1.50	3.3856	Marce/November 24 -28, 2016	5-Year
174	10.90128	123.3612056	0.32	5	21.9024	Sendong/December 28, 2011	5-Year
175	10.90067	123.3612542	0.03	5	24.7009	Sendong/December 28, 2011	5-Year
176	10.9024	123.3624837	0.21	8	60.6841	Zoraida/November 11-15, 1013	5-Year
177	10.88853	123.3555433	1.78	0	3.1684		5-Year
178	10.90054	123.3615289	0.05	5	24.5025	Sendong/40905	5-Year
179	10.90149	123.3621954	0.03	8	63.5209	Zoraida/November 11-15, 1013	5-Year
180	10.8727	123.3463318	0.05	5	24.5025	Yolanda/ November 2-11, 2013	5-Year
181	10.90195	123.3626131	0.25	8	60.0625	Zoraida/November 11-15, 1013	5-Year
182	10.89962	123.3607491	0.06	2	3.7636	Ruby/December 6-7, 2014	5-Year
183	10.89979	123.3608398	0.16	2	3.3856	Ruby/December 6-7, 2014	5-Year
184	10.90154	123.3618846	0.04	8	63.3616	Zoraida/November 11-15, 1013	5-Year
185	10.87314	123.3461015	0.23	5	22.7529	Yolanda/ November 2-11, 2013	5-Year
186	10.90215	123.3620047	0.15	8	61.6225	Zoraida/November 11-15, 1013	5-Year
187	10.90189	123.3622862	0.13	8	61.9369	Zoraida/November 11-15, 1013	5-Year
188	10.86925	123.3449526	7.28	1.50	33.4084	Marce/November 24 -28, 2016	5-Year
189	10.89191	123.3516445	0.46	2	2.3716	Ruping/November 13-18, 1998	100-Year
190	10.90145	123.361588	0.00	8	64	Zoraida/November 11-15, 1013	5-Year
191	10.87239	123.3461403	0.09	5	24.1081	Yolanda/ November 2-11, 2013	5-Year
192	10.87319	123.3456494	0.03	0.6	0.3249	Ruby/December 6-7, 2014	5-Year
193	10.90047	123.3616751	0.08	5	24.2064	Sendong/December 8, 2011	5-Year
194	10.90143	123.3671474	0.13	7	47.1969	Yolanda/ November 2-11, 2013	5-Year
195	10.86851	123.3455463	5.33	1.50	14.6689	Marce/November 24 -28. 2016	5-Year

196	10.90385	123.3658228	0.03	7	48.5809	Yolanda/ November 2-11, 2013	5-Year
197	10.89079	123.3518837	0.08	0	0.0064		5-Year
198	10.88872	123.3531789	2.28	0	5.1984		5-Year
199	10.92649	123.3678583	0.61	1	0.1521		5-Year
200	10.89668	123.358702	0.19	0	0.0361		5-Year
201	10.86897	123.344254	0.00	0	0		5-Year
202	10.94411	123.4215309	0.39	0	0.1521		5-Year
203	10.89078	123.3545456	6.15	1.68	19.9809		5-Year
204	10.87069	123.3446994	0.22	0	0.0484		5-Year
205	10.89266	123.3566754	0.09	6	34.9281		5-Year
206	10.9199	123.3710044	0.03	1	0.9409		5-Year
207	10.94221	123.4260776	0.07	0.94	0.7569	Yolanda/ November 2-11, 2013	5-Year
208	10.94244	123.4253684	0.05	0	0.0025		5-Year
209	10.94783	123.4105409	0.74	0	0.5476		5-Year
210	10.94529	123.4248301	0.03	0	0.0009		5-Year
211	10.95827	123.377296	0.17	0	0.0289		5-Year
212	10.94357	123.4245559	0.03	0	0.0009		5-Year
213	10.94642	123.4110986	0.00	0	0		5-Year
214	10.94901	123.4099329	1.08	0	1.1664		5-Year
215	10.95403	123.3618145	4.70	0	22.09		5-Year
216	10.88718	123.4132905	6.36	0	40.4496		5-Year
217	10.94763	123.4148646	0.03	1	0.9409	Yolanda/ November 2-11, 2013	5-Year
218	10.93618	123.4218418	2.02	0.18	3.3856	Yolanda/ November 2-11, 2013	5-Year
219	10.95537	123.3622837	0.00	1	1	Ruby/December 6-7, 2014	5-Year
220	10.90032	123.3698211	0.13	1.5	1.8769		5-Year
221	10.87358	123.3409052	1.26	0	1.5876		5-Year
222	10.88663	123.4126754	3.85	0	14.8225		5-Year
223	10.88559	123.4155922	9.91	0	98.2081		5-Year
224	10.89121	123.4149052	7.35	0	54.0225		5-Year
225	10.94175	123.4263453	0.09	0	0.0081	Yolanda/ November 2-11, 2013	5-Year
226	10.94381	123.4232168	0.04	0	0.0016		5-Year
227	10.93502	123.4224829	0.75	1.22	0.2209	Yolanda/ November 2-11, 2013	5-Year
228	10.94338	123.4248985	0.03	0	0.0009		5-Year
229	10.95766	123.3838976	0.04	0.43	0.1521	Yolanda/ November 2-11, 2013	5-Year
230	10.9434	123.4187944	1.05	0.43	0.3844	Yolanda/ November 2-11, 2013	5-Year
231	10.89648	123.4148746	2.44	0	5.9536		5-Year
232	10.95714	123.3704565	0.00	0	0		5-Year
233	10.95632	123.3611062	2.73	0	7.4529		5-Year
234	10.89286	123.4126843	1.00	0	1		5-Year
235	10.9419	123.4239126	0.06	0.94	0.7744		5-Year
236	10.95734	123.37657	0.00	0	0		5-Year
237	10.88541	123.416213	4.13	0	17.0569		5-Year
238	10.94599	123.4206997	1.10	0	1.21		5-Year
239	10.88727	123.3527191	0.03	0	0.0009		5-Year
240	10.89034	123.3559081	0.08	0	0.0064		5-Year
241	10.88543	123.4139001	0.06	0	0.0036		5-Year
242	10.94451	123.4253982	0.03	0	0.0009		5-Year
243	10.92607	123.370525	0.03	1	0.9409		5-Year
244	10.92209	123.3734647	0.08	1	0.8464		5-Year
245	10.91786	123.375687	0.73	1	0.0729		5-Year

Negros Occidental							
Sagay City							
Barangay	Building Name	Rainfall Scenario					
		5-year	25-year	100-year			
Fabrica	Faraon Institute						
Fabrica	Gil Lopez Elementary School						
Fabrica	TLRC Building						
Himogaan Baybay	Fabrica Elementary School						
Himogaan Baybay	Himogaan Integrated School						
Himogaan Baybay	Holy Family School						
Himogaan Baybay	Josebio Gonzaga Elementary School		High	High			
Himogaan Baybay	Paraiso Day Care		High	High			
Malubon	Filomeno Pascual Elementary School		Medium	High			
Malubon	Uychiat Elementary School						
Paraiso	Eusebio Lopez Integrated School						
Paraiso	Josebio Lopez Gonzaga Memorial Extension						
Paraiso	Ricardo Gamboa Elementary School						

Annex 12. Educational Institutions Affected in Himogaan-Tanao Floodplain

Annex 13. Medical Institutions Affected in Himogaan-Tanao Floodplain

Negros Occidental							
Sagay City							
Deveneration	Building Name	Rainfall Scenario					
вагапдау		5-year	25-year	100-year			
Himogaan Baybay	Paraiso Health Center		High	High			

Annex 14. UPC Phil-LiDAR 1 Team Composition

Project Leader

Jonnifer R. Sinogaya, PhD.

Chief Science Research Specialist Chito Patiño

Senior Science Research Specialists Christine Coca Jared Kislev Vicentillo

Research Associates

Isabella Pauline Quijano Jarlou Valenzuela Rey Sidney Carredo Mary Blaise Obaob Rani Dawn Olavides Sabrina Maluya Naressa Belle Saripada Jao Hallen Bañados Michael Angelo Palomar Glory Ann Jotea