HAZARD MAPPING OF THE PHILIPPINES USING LIDAR (PHIL-LIDAR I)

LiDAR Surveys and Flood Mapping of Mercedes River





University of the Philippines Training Center for Applied Geodesy and Photogrammetry Ateneo de Zamboanga University

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Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)



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TABLE OF CONTENTS

| LIST OF TABLES | V |
|--|---|
| LIST OF FIGURES | vii |
| LIST OF ACRONYMS AND ABBREVIATIONS | Х |
| CHAPTER 1: OVERVIEW OF THE PROGRAM AND MERCEDES RIVER | 1 |
| 1.1 Background of the Phil-LiDAR 1 Program | 1 |
| 1.2 Overview of the Mercedes River Basin | 1 |
| CHAPTER 2: LIDAR DATA ACQUISITION OF THE MERCEDES FLOODPLAIN | 4 |
| 2.1 Flight Plans | 4 |
| 2.2 Ground Base Stations | 6 |
| 2.3 Flight Missions | 12 |
| CHAPTER 3: LIDAR DATA PROCESSING OF THE MERCEDES FLOODPLAIN | 15 |
| 3.1 Overview of the LiDAR Data Pre-Processing | 15 |
| 3 2 Transmittal of Acquired LiDAR Data | 16 |
| 3 3 Trajectory Computation | 16 |
| 3.4 LiDAP Point Cloud Computation | 10 10 |
| 2.5 LiDAR Point Cloud Computation | 10 |
| 2.6 LiDAR Data Quality Clickling | פע בר |
| 3.0 LIDAR POINT CIOUD CIASSINCATION and Rasterization. | 23 |
| 3.7 LIDAR Image Processing and Orthophotograph Rectification | 25 |
| 3.8 DEM Editing and Hydro-Correction | 27 |
| 3.9 Mosaicking of Blocks | 29 |
| 3.10 Calibration and Validation of Mosaicked LiDAR DEM | 31 |
| 3.11 Integration of Bathymetric Data into the LiDAR Digital Terrain Model | 34 |
| 3.12 Feature Extraction | 36 |
| 3.12.1 Quality Checking of Digitized Features' Boundary | 36 |
| 3.12.2 Height Extraction | 37 |
| 3.12.3 Feature Attribution | 37 |
| 3.12.4 Final Quality Checking of Extracted Features | 39 |
| CHAPTER 4: LIDAR VALIDATION SURVEY AND MEASUREMENTS OF THE MERCEDES RIVER BAS | N.40 |
| 4.1. Summary of Activities | 40 |
| 4.2 Control Survey | 11 |
| | |
| 4.3 Baseline Processing | 41 45 |
| 4.3 Baseline Processing | 41 45 |
| 4.3 Baseline Processing 4.4 Network Adjustment 4.5 Cross-section and Bridge As Built survey and Water Level Marking | 41 45 46 |
| 4.3 Baseline Processing 4.4 Network Adjustment 4.5 Cross-section and Bridge As-Built survey and Water Level Marking 4.6 Validation Baints Acquisition Survey. | 41 45 46 49 |
| 4.3 Baseline Processing 4.4 Network Adjustment 4.5 Cross-section and Bridge As-Built survey and Water Level Marking 4.6 Validation Points Acquisition Survey | 41 45 46 49 54 |
| 4.3 Baseline Processing 4.4 Network Adjustment 4.5 Cross-section and Bridge As-Built survey and Water Level Marking 4.6 Validation Points Acquisition Survey | 41 45 46 49 54 56 |
| 4.3 Baseline Processing | 41 45 46 49 54 54 56 |
| 4.3 Baseline Processing | 41 45 46 49 54 56 59 59 |
| 4.3 Baseline Processing | 41 45 46 54 54 56 59 59 |
| 4.3 Baseline Processing | 41 45 46 54 54 56 59 59 59 |
| 4.3 Baseline Processing. 4.4 Network Adjustment. 4.5 Cross-section and Bridge As-Built survey and Water Level Marking. 4.6 Validation Points Acquisition Survey. 4.7 River Bathymetric Survey. CHAPTER 5: FLOOD MODELING AND MAPPING. 5.1 Data Used for Hydrologic Modeling. 5.1.1 Hydrometry and Rating Curves. 5.1.2 Precipitation. 5.1.3 Rating Curves and River Outflow. | 41 45 46 54 56 59 59 59 59 59 |
| 4.3 Baseline Processing. 4.4 Network Adjustment. 4.5 Cross-section and Bridge As-Built survey and Water Level Marking. 4.6 Validation Points Acquisition Survey. 4.7 River Bathymetric Survey. CHAPTER 5: FLOOD MODELING AND MAPPING. 5.1 Data Used for Hydrologic Modeling. 5.1.1 Hydrometry and Rating Curves. 5.1.2 Precipitation. 5.1.3 Rating Curves and River Outflow. 5.2 RIDF Station. | 41 45 49 54 59 59 59 59 59 60 61 |
| 4.3 Baseline Processing. 4.4 Network Adjustment. 4.5 Cross-section and Bridge As-Built survey and Water Level Marking. 4.6 Validation Points Acquisition Survey. 4.7 River Bathymetric Survey. CHAPTER 5: FLOOD MODELING AND MAPPING. 5.1 Data Used for Hydrologic Modeling. 5.1.1 Hydrometry and Rating Curves. 5.1.2 Precipitation. 5.1.3 Rating Curves and River Outflow. 5.2 RIDF Station. 5.3 HMS Model. | 41 45 46 54 56 59 59 59 60 61 63 |
| 4.3 Baseline Processing. 4.4 Network Adjustment. 4.5 Cross-section and Bridge As-Built survey and Water Level Marking. 4.6 Validation Points Acquisition Survey. 4.7 River Bathymetric Survey. CHAPTER 5: FLOOD MODELING AND MAPPING. 5.1 Data Used for Hydrologic Modeling. 5.1.1 Hydrometry and Rating Curves. 5.1.2 Precipitation. 5.1.3 Rating Curves and River Outflow. 5.2 RIDF Station. 5.3 HMS Model. 5.4 Cross-section Data. | 41 45 46 54 54 59 59 59 60 61 63 67 |
| 4.3 Baseline Processing. 4.4 Network Adjustment. 4.5 Cross-section and Bridge As-Built survey and Water Level Marking. 4.6 Validation Points Acquisition Survey. 4.7 River Bathymetric Survey. CHAPTER 5: FLOOD MODELING AND MAPPING. 5.1 Data Used for Hydrologic Modeling. 5.1.1 Hydrometry and Rating Curves. 5.1.2 Precipitation. 5.1.3 Rating Curves and River Outflow. 5.2 RIDF Station. 5.3 HMS Model. 5.4 Cross-section Data. 5.5 Flo 2D Model. | 41 45 46 54 56 59 59 59 60 61 63 67 68 |
| 4.3 Baseline Processing | 41 45 46 54 56 59 59 59 60 61 63 67 68 70 |
| 4.3 Baseline Processing | 41 45 46 54 59 59 59 60 61 63 67 68 70 72 |
| 4.3 Baseline Processing 4.4 Network Adjustment | 41 45 46 54 59 59 59 60 61 63 67 63 67 68 70 72 72 |
| 4.3 Baseline Processing | 41 45 46 54 59 59 59 60 61 63 67 63 67 68 70 72 72 72 |
| 4.3 Baseline Processing. 4.4 Network Adjustment. 4.5 Cross-section and Bridge As-Built survey and Water Level Marking. 4.6 Validation Points Acquisition Survey. 4.7 River Bathymetric Survey. CHAPTER 5: FLOOD MODELING AND MAPPING. 5.1 Data Used for Hydrologic Modeling. 5.1.1 Hydrometry and Rating Curves. 5.1.2 Precipitation. 5.1.3 Rating Curves and River Outflow. 5.2 RIDF Station. 5.3 HMS Model. 5.4 Cross-section Data. 5.5 Flo 2D Model. 5.6 Results of HMS Calibration. 5.7 Calculated outflow hydrographs and discharge values for different rainfall return periods 5.8 River Analysis (RAS) Model Simulation. 5.9 Flow Depth and Flood Hazard. | 41 45 46 54 59 59 59 59 60 61 63 67 63 70 72 72 73 74 |
| 4.3 Baseline Processing 4.4 Network Adjustment 4.5 Cross-section and Bridge As-Built survey and Water Level Marking | 41 45 46 54 59 59 59 60 61 63 67 63 70 72 72 72 74 74 74 |
| 4.3 Baseline Processing | 41 45 46 54 59 59 59 60 61 63 67 63 67 70 72 72 72 73 74 81 |
| 4.3 Baseline Processing 4.4 Network Adjustment | 41 45 46 54 59 59 59 60 61 63 67 63 67 70 72 72 73 74 81 88 |
| 4.3 Baseline Processing | 41 45 46 54 59 59 59 60 61 63 67 63 67 68 70 72 72 73 74 81 88 91 |
| 4.3 Baseline Processing | 41 45 46 54 59 59 59 60 61 63 67 63 67 68 70 72 72 72 73 74 81 88 91 |
| 4.3 Baseline Processing | 41 45 46 54 59 59 59 60 61 63 67 63 67 68 70 72 72 72 72 72 73 74 81 88 91 |
| 4.3 Baseline Processing | 41 45 46 54 59 59 59 59 60 61 63 67 63 67 63 70 72 72 72 72 73 74 81 88 91 92 94 |
| 4.3 Baseline Processing | 41 45 46 54 59 59 59 59 60 61 63 67 63 67 63 70 72 72 72 72 73 74 81 88 91 92 94 96 |
| 4.3 Baseline Processing | 41 45 46 49 54 59 59 59 60 61 63 67 63 67 63 70 72 72 72 73 74 81 92 92 94 96 91 |

| Annex 6. Flight Logs for the Flight Missions | 104 |
|--|-----|
| Annex 7. Flight Status Reports | 108 |
| Annex 8. Mission Summary Reports | 113 |
| Annex 9. Mercedes Model Basin Parameters | 129 |
| Annex 10. Mercedes Model Reach Parameters | 132 |
| Annex 11. Mercedes Field Validation Points | 133 |
| Annex 12. Educational Institutions Affected in Mercedes Floodplain | 138 |
| Annex 13. Medical Institutions Affected in Mercedes Floodplain | 138 |

LIST OF TABLES

| Table 1. Flight planning parameters for Pegasus LiDAR system | 4 |
|--|--------|
| Table 2. Details of the recovered NAMRIA horizontal control point ZGS-100 used as base station for the LiDAR acquisition | e 7 |
| Table 3. Details of the recovered NAMRIA horizontal control point ZGS-99 used as base station for the LiDAR acquisition | 8 |
| Table 4. Details of the recovered NAMRIA horizontal control point ZS-131 used as base station for the LiDAR acquisition | 9 |
| Table 5. Details of the established control point BVA-1 used as base station for the LiDAR acquisition | 10 |
| Table 6. Details of the established point BLLM-166 used as base station for the LiDAR acquisition | 11 |
| Table 7. Details of the established control point ZGS-99A used as base station for the LiDAR acquisition | า.11 |
| Table 8. Ground control points used during LiDAR data acquisition | 12 |
| Table 9. Flight missions for LiDAR data acquisition in Mercedes Floodplain | 12 |
| Table 10. Actual parameters used during LiDAR data acquisition | 13 |
| Table 11. List of Municipalities/Cities Surveyed in Mercedes Floodplain LiDAR survey | 13 |
| Table 12. Self-Calibration Results values for Mercedes flights | 18 |
| Table 13. List of LiDAR blocks for Mercedes Floodplain | 19 |
| Table 14. Mercedes classification results in TerraScan | 23 |
| Table 15. LiDAR blocks with its corresponding area | 27 |
| Table 16. Shift Values of each LiDAR Block of Mercedes Floodplain | 29 |
| Table 17. Calibration Statistical Measures | 33 |
| Table 18. Validation Statistical Measures | 34 |
| Table 19. Quality Checking Ratings for Mercedes Building Features | 36 |
| Table 20. Building Features Extracted for Mercedes Floodplain | 38 |
| Table 21. Total Length of Extracted Roads for Mercedes Floodplain | 38 |
| Table 22. Number of Extracted Water Bodies for Mercedes Floodplain | 38 |
| Table 23. List of references and control points used in Mercedes (Culianan) River Basin | 41 |
| Table 24. Baseline Processing Report for Mercedes (Culianan) River static survey | 45 |
| Table 25. Control Point Constraints | 46 |
| Table 26. Adjusted Grid Coordinates | 46 |
| Table 27. Adjusted Geodetic Coordinates | 48 |
| Table 28. Reference and control points used and its location | 48 |
| Table 29. RIDF values for Zamboanga City Rain Gauge computed by PAGASA | 61 |
| Table 30. Range of Calibrated Values for Mercedes | 70 |
| Table 31. Summary of the Efficiency Test of Mercedes HMS Model | 71 |
| Table 32. Peak values of the Mercedes HECHMS Model outflow using the Zamboanga City RIDF | 72 |
| Table 33. Municipalities affected in Mercedes Floodplain | 74 |
| Table 34. Affected Areas in Zamboanga City during 5-Year Rainfall Return Period | 82 |
| Table 35. Affected Areas in Zamboanga City during 25-Year Rainfall Return Period | 84 |
| Table 36. Affected Areas in Zamboanga City during 100-Year Rainfall Return Period | 86 |
| Table 37. Summary of the Accuracy Assessment in the Mercedes River Basin Survey | 88 |
| Table 38. Actual Flood Depth vs Simulated Flood Depth in Mercedes | 90 |
| Table 39. Summary of Accuracy Assessment in Mercedes | 90 |
| | |

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)

LIST OF FIGURES

| Figure 1. N | ิศลุ of the Mercedes River Basin (in brown) | .2 |
|-------------|--|----------|
| Figure 2. A | ARG and WLMS at Culianan Bridge | . 3 |
| Figure 3. T | he gate of the diversion dam in Culianan | .3 |
| Figure 4. F | light plan and base stations used for Mercedes Floodplain survey | .5 |
| Figure 5. G | GPS set-up over ZGS-100 in Brgy. Manicahan, Zamboanga del Sur (a) and NAMRIA | |
| r | eference point ZGS-100 (b) as recovered by the field team | .7 |
| Figure 6. G | GPS set-up over ZGS-99 beside the seawall in Calarian, Zamboanga City (a) and NAMRIA | |
| r | eference point ZGS-99 (b) as recovered by the field team | .8 |
| Figure 7. G | GPS set-up over ZS-131 in Curuan, Zamboanga City (a) and NAMRIA reference point | |
| Z | ZS-131 (b) as recovered by the field team | .9 |
| Figure 8. G | GPS set-up over BVA-1 established in Brgy. Buenavista, Zamboanga City (a) | |
| and Refere | ence point BVA-1 (b) as established by the field team | 10 |
| Figure 9. A | Actual LiDAR survey coverage for Mercedes Floodplain | 14 |
| Figure 10. | Schematic Diagram for Data Pre-Processing Component | 15 |
| Figure 11. | Smoothed Performance Metric Parameters of a Mercedes Flight 2535P | 16 |
| Figure 12. | Solution Status Parameters of Mercedes Flight 2535P | 17 |
| Figure 13. | Best Estimated Trajectory of the LiDAR Missions for Mercedes floodplain | 18 |
| Figure 14. | Boundary of the processed LiDAR data over Mercedes Floodplain | 19 |
| Figure 15. | Image of data overlap for Mercedes floodplain | 20 |
| Figure 16. | Density map of merged LiDAR data for Mercedes floodplain | 21 |
| Figure 17. | Elevation difference map between flight lines for Mercedes floodplain | 22 |
| Figure 18. | Quality checking for a Mercedes flight 2535P using the Profile Tool of QT Modeler | 23 |
| Figure 19. | Tiles for Mercedes floodplain (a) and classification results (b) in TerraScan | 24 |
| Figure 20. | Point cloud before (a) and after (b) classification | 24 |
| Figure 21. | The production of last return DSM (a) and DTM (b), first return DSM (c) and secondary | |
| 0 | DTM (d) in some portion of Mercedes floodplain | 25 |
| Figure 22. | Mercedes floodplain with available orthophotographs | 26 |
| Figure 23. | Sample orthophotograph tiles for Mercedes floodplain | 26 |
| Figure 24. | Portions in the DTM of Mercedes floodplain – a paddy field before (a) and after (b) data | |
| 0 | retrieval: a bridge before (c) and after (d) manual editing. | 28 |
| Figure 25. | Map of Processed LiDAR Data for Mercedes Floodplain | 30 |
| Figure 26. | Map of Mercedes Floodplain with validation survey points in green | 32 |
| Figure 27 | Correlation plot between calibration survey points and LiDAR data | 33 |
| Figure 28. | Correlation plot between validation survey points and LiDAR data | 34 |
| Figure 29 | Map of Mercedes Flood Plain with bathymetric survey points shown in blue | 35 |
| Figure 30 | Blocks (in blue) of Mercedes building features that were subjected to OC blocks | 36 |
| Figure 31 | Extracted features for Mercedes floodplain | 20 |
| Figure 32 | Extent of the Bathymetric survey (in blue line) in Mercedes River | 40 |
| Figure 32 | GNSS Network covering Mercedes (Culianan) River | 41 |
| Figure 34 | GNSS hase receiver setup. Trimble® SPS 852 at 7GS-99 | 42 |
| Figure 35 | GNSS receiver setup. Trimble® SPS 882 at 7S-177 located in Rizal Park | 42 |
| Figure 35. | GNSS receiver occupation. Trimble® SPS 852 at ARO-1 located along approach | . 2 |
| | of Abong Bridge | 43 |
| Figure 27 | GNSS hase receiver setup. Trimble® SPS 882 at CLIL-1 along approach of Culianan Bridge | 42 42 |
| Figure 32 | GNSS base receiver setup. Trimble® SPS 852 at 7GS-3508 along Tumaga Rridge | |
| inguic 50. | in Broy Tumaga Zamboanga City Zamboanga Del Sur | 44 |
| | | · T |

| Figure 39 (a) Culianan Bridge and (b) Cross-section and bridge as-bui | It survey for Culianan Bridge49 |
|---|---------------------------------|
| Figure 40. Culianan bridge cross-section location map | 50 |
| Figure 41 Culianan Bridge cross-section diagram | 51 |
| Figure 42. The Culianan Bridge as-built survey data | 52 |
| Figure 43. (a) Existing water level post near Culianan Bridge and (b) V | Vater level marking53 |
| Figure 44. (a) Ground validation set-up by: Trimble® SPS 882 mounte | ed on a pole |
| attached on the side of the vehicle | 54 |
| Figure 45. Validation acquisition points survey covering Mercedes (C | ulianan) River55 |
| Figure 46. Bathymetric survey in Culianan River: (a) upstream and (b) |) downstream56 |
| Figure 47. Bathymetric survey of Culianan River | 57 |
| Figure 48. Riverbed profile of Culianan River | 58 |
| Figure 49. Location map of Mercedes HEC-HMS model used for calib | ration59 |
| Figure 50. Cross-Section Plot of Culianan Bridge | 60 |
| Figure 51. Hydrometry rating curve of Culianan Bridge | 60 |
| Figure 52. Rainfall and outflow data at Mercedes used for modeling. | 61 |
| Figure 53. Zamboanga City RIDF location relative to Mercedes River B | Basin62 |
| Figure 54. Synthetic storm generated for a 24-hr period rainfall for va | arious return periods62 |
| Figure 55. Soil Map of Mercedes River Basin | 63 |
| Figure 56. Land Cover Map of Mercedes River Basin (Source: NAMRIA | ۹) 64 |
| Figure 57. Stream Delineation Map of Mercedes River Basin | 65 |
| Figure 58. The Mercedes river basin model generated using HEC-HM | S66 |
| Figure 59. River cross-section of Mercedes River generated through A | Arcmap HEC GeoRAS tool67 |
| Figure 60. Screenshot of subcatchment with computational area to b | e modeled in FLO-2D GDS Pro.68 |
| Figure 61. Generated 100-year rain return hazard map from FLO-2D I | Mapper68 |
| Figure 62. Generated 100-year rain return flow depth map from FLO- | 2D Mapper69 |
| Figure 63. Outflow Hydrograph of Mercedes produced by the HEC-HI | VIS model |
| compared with observed outflow | 70 |
| Figure 64. Outflow hydrograph at Mercedes Station | 72 |
| Figure 65. Sample output of Mercedes RAS Model | 73 |
| Figure 66. 100-year Flood Hazard Map for Mercedes Floodplain | 75 |
| Figure 67. 100-year Flow Depth Map for Mercedes Floodplain | 76 |
| Figure 68. 25-year Flood Hazard Map for Mercedes Floodplain | 77 |
| Figure 69. 25-year Flow Depth Map for Mercedes Floodplain | 78 |
| Figure 70. 5-year Flood Hazard Map for Mercedes Floodplain | 79 |
| Figure 71. 5-year Flow Depth Map for Mercedes Floodplain | 80 |
| Figure 72. Affected Areas in Zamboanga City during 5-Year Rainfall Re | eturn Period83 |
| Figure 73. Affected Areas in Zamboanga City during 25-Year Rainfall F | Return Period85 |
| Figure 74. Affected Areas in Zamboanga City during 100-Year Rainfall | Return Period87 |
| Figure 75. Validation points for 5-year Flood Depth Map of Mercedes | Floodplain89 |
| Figure 76. Flood map depth vs actual flood depth | 90 |

LiDAR Surveys and Flood Mapping of Mercedes River

LIST OF ACRONYMS AND ABBREVIATIONS

| AAC | Asian Aerospace Corporation |
|---------|---|
| Ab | abutment |
| ADZU | Ateneo de Zamboanga University |
| ALTM | Airborne LiDAR Terrain Mapper |
| ARG | automatic rain gauge |
| AWLS | Automated Water Level Sensor |
| BA | Bridge Approach |
| BM | benchmark |
| CAD | Computer-Aided Design |
| CN | Curve Number |
| CSRS | Chief Science Research Specialist |
| DAC | Data Acquisition Component |
| DEM | Digital Elevation Model |
| DENR | Department of Environment and Natural Resources |
| DOST | Department of Science and Technology |
| DPPC | Data Pre-Processing Component |
| DREAM | Disaster Risk and Exposure Assessment for Mitigation [Program] |
| DRRM | Disaster Risk Reduction and Management |
| DSM | Digital Surface Model |
| DTM | Digital Terrain Model |
| DVBC | Data Validation and Bathymetry Component |
| FMC | Flood Modeling Component |
| FOV | Field of View |
| GiA | Grants-in-Aid |
| GCP | Ground Control Point |
| GNSS | Global Navigation Satellite System |
| GPS | Global Positioning System |
| HEC-HMS | Hydrologic Engineering Center - Hydrologic Modeling System |
| HEC-RAS | Hydrologic Engineering Center - River Analysis System |
| НС | High Chord |
| | Tigh cherd |

| IMU | Inertial Measurement Unit |
|----------|--|
| kts | knots |
| LAS | LiDAR Data Exchange File format |
| LC | Low Chord |
| LGU | local government unit |
| Lidar | Light Detection and Ranging |
| LMS | LiDAR Mapping Suite |
| m AGL | meters Above Ground Level |
| MMS | Mobile Mapping Suite |
| MSL | mean sea level |
| NSTC | Northern Subtropical Convergence |
| PAF | Philippine Air Force |
| PAGASA | Philippine Atmospheric Geophysical and Astronomical Services Administration |
| PDOP | Positional Dilution of Precision |
| РРК | Post-Processed Kinematic [technique] |
| PRF | Pulse Repetition Frequency |
| PTM | Philippine Transverse Mercator |
| QC | Quality Check |
| QT | Quick Terrain [Modeler] |
| RA | Research Associate |
| RIDF | Rainfall-Intensity-Duration-Frequency |
| RMSE | Root Mean Square Error |
| SAR | Synthetic Aperture Radar |
| SCS | Soil Conservation Service |
| SRTM | Shuttle Radar Topography Mission |
| SRS | Science Research Specialist |
| SSG | Special Service Group |
| ТВС | Thermal Barrier Coatings |
| UP-TCAGP | University of the Philippines – Training Center for Applied Geodesy and Photogrammetry |
| UTM | Universal Transverse Mercator |
| WGS | World Geodetic System |
| | |

CHAPTER 1: OVERVIEW OF THE PROGRAM AND MERCEDES RIVER

Enrico C. Paringit, Dr. Eng., Mario Rodriguez, and Emir Epino

1.1 Background of the Phil-LiDAR 1 Program

The University of the Philippines Training Center for Applied Geodesy and Photogrammetry (UP-TCAGP) launched a research program entitled "Nationwide Hazard Mapping using LiDAR" or Phil-LiDAR 1, supported by the Department of Science and Technology (DOST) Grants-in-Aid (GiA) Program. The program was primarily aimed at acquiring a national elevation and resource dataset at sufficient resolution to produce information necessary to support the different phases of disaster management. Particularly, it targeted to operationalize the development of flood hazard models that would produce updated and detailed flood hazard maps for the major river systems in the country.

Also, the program was aimed at producing an up-to-date and detailed national elevation dataset suitable for 1:5,000 scale mapping, with 50 cm and 20 cm horizontal and vertical accuracies, respectively. These accuracies were achieved through the use of the state-of-the-art Light Detection and Ranging (LiDAR) airborne technology procured by the project through DOST.

The methods applied in this report are thoroughly described in a separate publication entitled "Flood Mapping of Rivers in the Philippines Using Airborne LiDAR: Methods" (Paringit, et. al. 2017).

The implementing partner university for the Phil-LiDAR 1 Program is the Ateneo de Zamboanga University (ADZU). ADZU is in charge of processing LiDAR data and conducting data validation reconnaissance, cross section, bathymetric survey, validation, river flow measurements, flood height and extent data gathering, flood modeling, and flood map generation for the 18 river basins in the Western Visayas Region. The university is located in Zamboanga City in the province of Zamboanga Sibugay.

1.2 Overview of the Mercedes River Basin

The Mercedes (also known as Culianan) River Basin covers six (6) barangays of Zamboanga City, namely: Brgy. Tolosa, Salaan, Pasobolong, Culianan, Mercedes and Zambowood with a total population estimate of 37,925, according to the May 2010 census. It has a catchment approximate area of 50.36 km2 according to DENR-RCBO.

Its main stem, Culianan River is part of the 18 river systems in the Zamboanga Peninsula. It is also among the rivers which contributed to the flooding on a large part of Zamboanga City during Typhoon Quedan on October 4, 2013, which left a trail of destruction in many areas that affected thousands of people. Nevertheless, the river is significant in the area as source of water for agricultural lands in the barangays of Tolosa, Salaan, Pasobolong, Culianan and Mercedes. Brgy. Zambowood is the home of Zamboanga wood products and use portions of Culianan River as log ponds since their saw mill is found in the area.

Named after one of the barangays in Zamboanga City, Mercedes lies connected to Tumaga River. It has a catchment area of 49.02 sq.km, almost three times smaller than Tumaga. The main river acts as the boundary between the barangays of Zambowood, Pasobolong, Salaan in the west and the barangays of Tolosa, Lanzones, Culianan, and Mercedes in the east.

The name Mercedes, originally Las Mercedes, was used to honor the Patron Saint of Mercedarian who was responsible for the rescue of Christian captives from the Moors in Spain during the reign of Don Jaime de Aragon. It was given by a Jesuit missionary in the 1870s to a place that was formerly known as Paso Caña because of the abundance of bamboo trees along its river banks. Technically, Culianan and Mercedes are the same rivers, but the city local government stated to use the name Mercedes for consistency purposes.



Figure 1. Map of the Mercedes River Basin (in brown)

Flood Incidence

Areas along Mercedes River are identified by the Mines and Geosciences Bureau of Region 9 to be under low to moderate susceptibility against floods. In the increasing intensity of rain events in Zamboanga City brought about by climate change, the bureau recommends the improvement of storm water drainage networks and the strengthening of the built-up areas along the river banks to mitigate flood damages.



Figure 2. ARG and WLMS at Culianan Bridge

In October of 2006, Zamboanga City experienced torrential rains which flooded many villages and destroyed rice paddies and several aquatic resources particularly seaweed farms and fishponds. Tumaga and Culianan were among the most affected areas (The Mindanao Examiner, 2006).



Figure 3. The gate of the diversion dam in Culianan

In the hopes of mitigating these adverse effects of floods, Mercedes River was included in the nationwide Deployment of Early Warning Systems (DEWS) program of the Department of Science and Technology (DOST). A tandem sensor which consists of an Automated Rain Gauge (ARG) and a Water Level Monitoring System (WLMS) was installed in Culianan Bridge in 2013.

Agriculture and Fishery

Mercedes normally produces 17, 158.40 cubic meters of water per day. This volume was measured at the Culianan Bridge (6.971554°E, 122.138069°N) on April 2015. This provides supply for the irrigation of rice fields in the nearby barangays. A controlled mini dam is installed at Barangay Culianan intended to divert the water from the river to irrigation channels during rainy seasons.

It also partially supports majority of the fishponds in the coastlines of Mercedes and Zambowood.

CHAPTER 2: LIDAR DATA ACQUISITION OF THE MERCEDES FLOODPLAIN

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The methods applied in this Chapter were based on the DREAM methods manual (Sarmiento, et al., 2014) and further enhanced and updated in Paringit, et al. (2017).

2.1 Flight Plans

Plans were made to acquire LiDAR data within the delineated priority area for Mercedes floodplain in Zamboanga. Each flight mission has an average of 12 lines and run for at most four and a half (4.5) hours including take-off, landing and turning time. The parameter used in the LiDAR system for acquisition is found in Table 1. Figure 1 shows the flight plans for Mercedes floodplain.shows the flight plan for the Silaga Floodplain survey.

| Block Name | Flying Height (m AGL) | Overlap (%) | Field of view (ø) | Pulse Repetition Frequency (PRF) (kHz) | Scan Frequency (Hz) | Average Speed (kts) | Average Turn Time (Minutes) |
|-----------------|-----------------------------|----------------|----------------------|--|---------------------------|---------------------------|--------------------------------------|
| BLK75E | 1100 | 30 | 50 | 200 | 30 | 130 | 5 |
| Sacol Island | 800/1200 | 30 | 50 | 200 | 30 | 130 | 5 |
| BLK75AS | 1000 | 30 | 50 | 200 | 30 | 130 | 5 |

Table 1. Flight planning parameters for Pegasus LiDAR system



Figure 4. Flight plan and base stations used for Mercedes Floodplain survey

2.2 Ground Base Stations

The project team was able to recover two (2) NAMRIA ground control points: ZGS-100 and ZGS-99 which are of second (2nd) order accuracy, one (1) Bench Mark point: ZS-131, and three (2) established control point: ZG-99A, BLLM-166 and BVA-1. The certifications for the NAMRIA reference points and processing report for the established points are found in Annex 2. These were used as base stations during flight operations for the entire duration of the survey (January 29-Febuary 12, 2015; May 19-31, 2016). Base stations were observed using dual frequency GPS receivers, TRIMBLE SPS 882, SPS 852 and SPS 985. Flight plans and location of base stations used during the aerial LiDAR acquisition in Mercedes floodplain are also shown in Figure 4.

Figures 5-8 show the recovered NAMRIA control stations within the area, in addition Table 2 to Table 7 show the details about the following NAMRIA control stations and established points, Table 8 shows the list of all ground control points occupied during the acquisition together with the dates they are utilized during the survey.



Figure 5. GPS set-up over ZGS-100 in Brgy. Manicahan, Zamboanga del Sur (a) and NAMRIA reference point ZGS-100 (b) as recovered by the field team.

| Table 2. Details of the recovered NAMRIA horizontal control point ZGS-100 used as base station for the LiDAR |
|--|
| acquisition |

| Station Name | ZGS-100 | | |
|---|---|---|--|
| Order of Accuracy | 2rd | | |
| Relative Error (horizontal positioning) | 1 in 50,000 | | |
| Geographic Coordinates, Philippine Reference of 1992 Datum (PRS 92) | Latitude Longitude Ellipsoidal Height | 7° 1' 26.72368" North 122° 11' 12.74401" East 11.27 meters | |
| Grid Coordinates, Philippine Transverse Mercator Zone 5 (PTM Zone 5 PRS 92) | Easting Northing | 410158.521 meters 776712.542 meters | |
| Geographic Coordinates, World Geodetic System 1984 Datum (WGS 84) | Latitude Longitude Ellipsoidal Height | 7° 1' 23.30149" North 122° 11' 18.30044" East 75.603 meters | |
| Grid Coordinates, Universal Transverse Mercator Zone 51 North (UTM 51N PRS 1992) | Easting Northing | 410189.97 meters 776440.68 meters | |



Figure 6. GPS set-up over ZGS-99 beside the seawall in Calarian, Zamboanga City (a) and NAMRIA reference point ZGS-99 (b) as recovered by the field team

Table 3. Details of the recovered NAMRIA horizontal control point ZGS-99 used as base station for the LiDAR acquisition

| Station Name | ZGS-99 | | |
|---|---|---|--|
| Order of Accuracy | 2rd | | |
| Relative Error (horizontal positioning) | 1 in 50,000 | | |
| Geographic Coordinates, Philippine Reference of 1992 Datum (PRS 92) | Latitude Longitude Ellipsoidal Height | 5° 55' 37.48971" North 122° 0' 52.66431" East 8.14900 meters | |
| Grid Coordinates, Philippine Transverse Mercator Zone 4 (PTM Zone 5 PRS 92) | Easting Northing | 766020.391 meters 391103.346 meters | |
| Geographic Coordinates, World Geodetic System 1984 Datum (WGS 84) | Latitude Longitude Ellipsoidal Height | 6° 55' 34.07737" North 122° 0' 58.23072" East 72.23000 meters | |
| Grid Coordinates, Universal Transverse Mercator Zone 51 North (UTM 51N PRS 1992) | Easting Northing | 765752.27 meters 391141.46 meters | |



Figure 7. GPS set-up over ZS-131 in Curuan, Zamboanga City (a) and NAMRIA reference point ZS-131 (b) as recovered by the field team

| Table 4. Details of the recovered NAMRIA horizontal control point ZS-131 used as base station for the LiDAR |
|---|
| acquisition |

| Station Name | ZS-131 | | |
|---|---|--|--|
| Order of Accuracy | 2nd | | |
| Relative Error (horizontal positioning) | 1 in 5 | 0,000 | |
| Geographic Coordinates, Philippine Reference of 1992 Datum (PRS 92) | Latitude Longitude Ellipsoidal Height | 7°12'31.51602" North 122°13'42.69458" East 15.557 meters | |
| Grid Coordinates, Universal Transverse Mercator Zone 51 North (UTM 51N WGS 1984) | Latitude Longitude Ellipsoidal Height | 414824.878 meters 796847.561 meters | |
| Geographic Coordinates, World Geodetic System 1984 Datum (WGS 84) | Latitude Longitude Ellipsoidal Height | 7°12'28.04890" North 122°13'48.23382" East 79.651 meters | |



Figure 8. GPS set-up over BVA-1 established in Brgy. Buenavista, Zamboanga City and (a) and Reference point BVA-1 (b) as established by the field team

| Station Name | BV | A-1 | |
|---|---|---|--|
| Order of Accuracy | 2nd | | |
| Relative Error (horizontal positioning) | 1 in 5 | 0,000 | |
| Geographic Coordinates, Philippine Reference of 1992 Datum (PRS 92) | Latitude Longitude Ellipsoidal Height | 67° 15' 19.31910"North 122° 15' 28.78738"East 82.446 meters | |
| Grid Coordinates, Universal Transverse Mercator Zone 51 North (UTM 51N PRS 1992) | Easting Northing | 417939.856 meters 802333.522 meters | |
| Geographic Coordinates, World Geodetic System 1984 Datum (WGS 84) | Latitude Longitude Ellipsoidal Height | 7° 15' 15.84241" North 122° 15' 34.32212" East 146.526 meters | |

Table 5. Details of the established control point BVA-1 used as base station for the LiDAR acquisition

Table 6. Details of the established point BLLM-166 used as base station for the LiDAR acquisition

| Station Name | BLLM-166 | | | |
|---|---|--|--|--|
| Order of Accuracy | 21 | nd | | |
| Relative Error (horizontal positioning) | 1 in 5 | 0,000 | | |
| Geographic Coordinates, Philippine Reference of 1992 Datum (PRS 92) | Latitude Longitude Ellipsoidal Height | 7°09'33.60926" North 122°13'54.54820" East 124.333 meters | | |
| Grid Coordinates, Universal Transverse Mercator Zone 51 North (UTM 51N WGS 1984) | Easting Northing | 415179.269 meters 791383.716 meters | | |
| Geographic Coordinates, World Geodetic System 1984 Datum (WGS 84) | Latitude Longitude Ellipsoidal Height | 77°09'30.15553" North 122°14'00.09187" East 188.527 meters | | |

Table 7. Details of the established control point ZGS-99A used as base station for the LiDAR acquisition

| Station Name | ZGS-99A | | |
|---|---|--|--|
| Order of Accuracy | 21 | nd | |
| Relative Error (horizontal positioning) | 1 in 50,000 | | |
| Geographic Coordinates, Philippine Reference of 1992 Datum (PRS 92) | Latitude Longitude Ellipsoidal Height | 6° 55′ 37.63895″North 122° 00′ 52.48834″East 7.850 meters | |
| Grid Coordinates, Universal Transverse Mercator Zone 51 North (UTM 51N WGS 1984) | Easting Northing | 391136.071 meters 765756.864 meters | |
| Geographic Coordinates, World Geodetic System 1984 Datum (WGS 84) | Latitude Longitude Ellipsoidal Height | 6° 55' 34.22659" North 122° 00' 58.05475" East 71.931 meters | |

| Date Surveyed | Flight Number | Mission Name | Ground Control Points |
|----------------------|---------------|--------------|-----------------------|
| February 5, 2015 | 2535P | 1BLK75E36A | BLLM-166 and ZGS-100 |
| February 8, 2015 | 2545P | 1BLK75S39A | BVA-1 and ZGS-100 |
| February 11, 2015 | 2557P | 1BLK75S42A | ZGS-99 and ZGS-99A |
| May 26, 2016 | 23394P | 1BLK75AS147B | ZGS-100 and ZS-131 |

Table 8. Ground control points used during LiDAR data acquisition

2.3 Flight Missions

Four (4) missions were conducted to complete LiDAR data acquisition in Mercedes floodplain, for a total of 14 hours and 14 minutes of flying time for RP-C9022. All missions were acquired using the Pegasus system. Table 9 shows the total area of actual coverage and the corresponding flying hours per mission, while Table 10 presents the actual parameters used during the LiDAR data acquisition.

| | | Flight | | Area Surveved | Area Surveyed | No. of | Flying Hours | |
|----------------------|------------------|--------------------|------------------------|-----------------------------------|------------------------------------|--------------------|--------------|-----|
| Date Surveyed | Flight Number | Plan Area (km²) | Surveyed Area (km²) | within the Floodplain (km²) | Outside the Floodplain (km²) | Images (Frames) | H | Min |
| February 5, 2015 | 2535P | 357.52 | 331.7 | 16.54 | 315.16 | 715 | 3 | 53 |
| February 8, 2015 | 2545P | 906.64 | 318.38 | 7.48 | 310.9 | 608 | 4 | 11 |
| February 11, 2015 | 2557P | 234.33 | 228.21 | 2.16 | 226.05 | 474 | 4 | 23 |
| May 26, 2016 | 23394P | 13.39 | 54.57 | 1.99 | 52.58 | NA | 1 | 47 |
| ΤΟΤΑ | L | 1511.88 | 932.86 | 28.17 | 904.69 | 715 | 14 | 14 |

Table 9. Flight missions for LiDAR data acquisition in Mercedes Floodplain

| Block Name | Flying Height (AGL) | Overlap (%) | Field of View (θ) | Pulse Repetition Frequency (PRF) (kHz) | Scan Fre- quency (Hz) | Average Speed (kts) | Average Turn Time (Minutes) |
|---------------|---------------------------|----------------|----------------------------|---|-----------------------------|---------------------------|-----------------------------------|
| 2535P | 1100 | 30 | 50 | 200 | 30 | 130 | 5 |
| 2545P | 1100 | 30 | 50 | 200 | 30 | 130 | 5 |
| 2557P | 800/1200 | 30 | 50 | 200 | 30 | 130 | 5 |
| 23394P | 1000 | 30 | 50 | 200 | 30 | 130 | 5 |

Table 10. Actual parameters used during LiDAR data acquisition

Mercedes floodplain is located in the provinces of Zamboanga del Sur the floodplain situated within the City of Zamboanga. The list of municipalities and cities surveyed with at least one (1) square kilometer coverage is shown in Table 11. The actual coverage of the LiDAR acquisition for Mercedes floodplain is presented in Figure 6.

|--|

| Province | Municipality/City | Area of Munici- pality/City (km²) | Total Area Surveyed (km²) | Percentage of Area Sur- veyed =(Total Area covered/ Area of Municipality)*100 |
|----------------------|-------------------|--------------------------------------|---------------------------------|--|
| Zamboanga del Sur | Zamboanga City | 1461.04 | 691.32 | 47% |
| Zamboanga Sibugay | Tungawan | 441.86 | 26.7 | 6% |
| | Total | 1902.9 | 718.02 | 37.73% |



Figure 9. Actual LiDAR survey coverage for Mercedes Floodplain

CHAPTER 3: LIDAR DATA PROCESSING OF THE MERCEDES FLOODPLAIN

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The methods applied in this Chapter were based on the DREAM methods manual (Ang, et al., 2014) and further enhanced and updated in Paringit, et al. (2017)

3.1 Overview of the LiDAR Data Pre-Processing

The data transmitted by the Data Acquisition Component are checked for completeness based on the list of raw files required to proceed with the pre-processing of the LiDAR data. Upon acceptance of the LiDAR field data, georeferencing of the flight trajectory is done in order to obtain the exact location of the LiDAR sensor when the laser was shot. Point cloud georectification is performed to incorporate correct position and orientation for each point acquired. The georectified LiDAR point clouds are subject for quality checking to ensure that the required accuracies of the program, which are the minimum point density, vertical and horizontal accuracies, are met. The point clouds are then classified into various classes before generating Digital Elevation Models such as Digital Terrain Model and Digital Surface Model.

Using the elevation of points gathered in the field, the LiDAR-derived digital models are calibrated. Portions of the river that are barely penetrated by the LiDAR system are replaced by the actual river geometry measured from the field by the Data Validation and Bathymetry Component. LiDAR acquired temporally are then mosaicked to completely cover the target river systems in the Philippines. Orthorectification of images acquired simultaneously with the LiDAR data is done through the help of the georectified point clouds and the metadata containing the time the image was captured.

These processes are summarized in the flowchart shown in Figure 10.



Figure 10. Schematic Diagram for Data Pre-Processing Component

3.2 Transmittal of Acquired LiDAR Data

Data transfer sheets for all the LiDAR missions for Mercedes floodplain can be found in Annex 5. Missions flown during the first survey conducted on February 2015 used the Airborne LiDAR Terrain Mapper (ALTM[™] Optech Inc.) Pegasus system while missions the second survey on May 2016 were flown using the same system over Zamboanga City.

The Data Acquisition Component (DAC) transferred a total of 82.53 Gigabytes of Range data, 847 Megabytes of POS data, 156.77 Megabytes of GPS base station data, and 120.20 Gigabytes of raw image data to the data server on June 3, 2015 for the first survey and July 14, 2016 for the second survey. The Data Pre-processing Component (DPPC) verified the completeness of the transferred data. The whole dataset for Mercedes was fully transferred on July 14, 2016, as indicated on the Data Transfer Sheets for Mercedes floodplain.

3.3 Trajectory Computation

The Smoothed Performance Metrics of the computed trajectory for flight 2535P, one of the Mercedes flights, which is the North, East, and Down position RMSE values are shown in Figure 11. The x-axis corresponds to the time of flight, which is measured by the number of seconds from the midnight of the start of the GPS week, which on that week fell on February 5, 2015 00:00AM. The y-axis is the RMSE value for that particular position.



Figure 11. Smoothed Performance Metrics of a Mercedes Flight 2535P.

The time of flight was from 367000 seconds to 379500 seconds, which corresponds to morning of February 5, 2015. The initial spike that is seen on the data corresponds to the time that the aircraft was getting into position to start the acquisition, and the POS system starts computing for the position and orientation of the aircraft.

Redundant measurements from the POS system quickly minimized the RMSE value of the positions. The periodic increase in RMSE values from an otherwise smoothly curving RMSE values correspond to the turnaround period of the aircraft, when the aircraft makes a turn to start a new flight line. Figure 11 shows that the North position RMSE peaks at 2.85 centimeters, the East position RMSE peaks at 1.26 centimeters, and the Down position RMSE peaks at 3.80 centimeters, which are within the prescribed accuracies described in the methodology.



Figure 12. Solution Status Parameters of Mercedes Flight 2535P

The Solution Status parameters of flight 2535P, one of the Mercedes flights, which indicate the number of GPS satellites, Positional Dilution of Precision (PDOP), and the GPS processing mode used, are shown in Figure 12. The graphs indicate that the number of satellites during the acquisition did not go down to 6. Most of the time, the number of satellites tracked was between 6 and 10. The PDOP value also did not go above the value of 3, which indicates optimal GPS geometry. The processing mode remained at 0 for majority of the survey with some peaks up to 1 attributed to the turns performed by the aircraft. The value of 0 corresponds to a Fixed, Narrow-Lane mode, which is the optimum carrier-cycle integer ambiguity resolution technique available for POSPAC MMS. All of the parameters adhered to the accuracy requirements for optimal trajectory solutions, as indicated in the methodology. The computed best estimated trajectory for all Mercedes flights is shown in Figure 13.

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)



Figure 13. Best estimated trajectory for Mercedes Floodplain.

3.4 LiDAR Point Cloud Computation

The produced LAS data contains 36 flight lines, with each flight line containing two channels, since the Pegasus system was used. The summary of the self-calibration results obtained from LiDAR processing in LiDAR Mapping Suite (LMS) software for all flights over Mercedes floodplain are given in Table 12.

| Parameter | Acceptable Value | Value |
|---|------------------|----------|
| Boresight Correction stdev) | <0.001degrees | 0.000223 |
| IMU Attitude Correction Roll and Pitch Correction stdev) | <0.001degrees | 0.000328 |
| GPS Position Z-correction stdev) | <0.01meters | 0.0061 |

| Table 12. Self-calibration | results values | for Mercedes | flights. |
|----------------------------|----------------|--------------|----------|
| | | | |

The optimum accuracy is obtained for all Mercedes flights based on the computed standard deviations of the corrections of the orientation parameters. Standard deviation values for individual blocks are available in the Annex 8:Mission Summary Reports.

3.5 LiDAR Data Quality Checking

The boundary of the processed LiDAR data is shown in Figure 14. The map shows no gaps in the LiDAR coverage.



Figure 14. Boundary of the processed LiDAR on top of a SAR Elevation Data over Mercedes Floodplain.

The total area covered by the Mercedes missions is 527.27 sq.km that is comprised of four (4) flight acquisitions grouped and merged into three (3) blocks as shown in Table 13.

| LiDAR Blocks | Flight Numbers | Area (sq. km) | |
|-----------------------------|----------------|---------------|--|
| Zamboongo PIK75E | 2535P | 204 02 | |
| | 2545P | 394.93 | |
| Zamboanga_Sacol | 2557P | 96.90 | |
| Zamboanga_reflights_Blk75AS | 23394P | 35.24 | |
| | TOTAL | 527.27 sq.km | |

| Table 13 | S List c | of LiDAR | blocks | for Me | rcedes f | floodplain |
|----------|----------|----------|--------|----------|----------|------------|
| I able L | . LISU | л LIDAK | DIOCKS | IOI IVIC | ICCUES I | 100upiam. |

The overlap data for the merged LiDAR blocks, showing the number of channels that pass through a particular location is shown in Figure 15. Since the Pegasus system covered all of the area, we would expect an average value of 2 (blue) for areas where there is limited overlap, and a value of 3 (yellow) or more (red) for areas with three or more overlapping flight lines.



Figure 15. Image of data overlap for Mercedes Floodplain

The overlap statistics per block for the Mercedes floodplain can be found in Annex 8. One pixel corresponds to 25.0 square meters on the ground. For this area, the minimum and maximum percent overlaps are 26.46% and 27.08% respectively, which passed the 25% requirement.

The pulse density map for the merged LiDAR data, with the red parts showing the portions of the data that satisfy the 2 points per square meter criterion is shown in Figure 16. It was determined that all LiDAR data for Mercedes floodplain satisfy the point density requirement, and the average density for the entire survey area is 2.56 points per square meter.



Figure 16. Pulse density map of merged LiDAR data for Mercedes Floodplain

The elevation difference between overlaps of adjacent flight lines is shown in Figure 17. The default color range is from blue to red, where bright blue areas correspond to portions where elevations of a previous flight line, identified by its acquisition time, are higher by more than 0.20m relative to elevations of its adjacent flight line. Bright red areas indicate portions where elevations of a previous flight line are lower by more than 0.20m relative to elevations of its adjacent flight line. Areas with bright red or bright blue need to be investigated further using Quick Terrain Modeler software.

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)



Figure 17. Elevation difference map between flight lines for Mercedes Floodplain

A screen capture of the processed LAS data from a Mercedes flight 2535P loaded in QT Modeler is shown in Figure 18. The upper left image shows the elevations of the points from two overlapping flight strips traversed by the profile, illustrated by a dashed yellow line. The x-axis corresponds to the length of the profile. It is evident that there are differences in elevation, but the differences do not exceed the 20-centimeter mark. This profiling was repeated until the quality of the LiDAR data becomes satisfactory. No reprocessing was done for this LiDAR dataset.



Figure 18. Quality checking for a Mercedes flight 2535P using the Profile Tool of QT Modeler

3.6 LiDAR Point Cloud Classification and Rasterization

| Pertinent Class | Total Number of Points | | |
|-------------------|------------------------|--|--|
| Ground | 503,251,800 | | |
| Low Vegetation | 385,239,703 | | |
| Medium Vegetation | 542,828,825 | | |
| High Vegetation | 1,061,362,902 | | |
| Building | 42,820,674 | | |

Table 14. Mercedes classification results in TerraScan

The tile system that TerraScan employed for the LiDAR data and the final classification image for a block in Mercedes floodplain is shown in Figure 19. A total of 765 1km by 1km tiles were produced. The number of points classified to the pertinent categories is illustrated in Table 14. The point cloud has a maximum and minimum height of 588.90 meters and 65.50 meters respectively.



Figure 19. Tiles for Mercedes Floodplain (a) and classification results (b) in TerraScan

An isometric view of an area before and after running the classification routines is shown in Figure 20. The ground points are in orange, the vegetation is in different shades of green, and the buildings are in cyan. It can be seen that residential structures adjacent or even below canopy are classified correctly, due to the density of the LiDAR data.



Figure 20. Point cloud before (a) and after (b) classification

The production of last return (V_ASCII) and the secondary (T_ASCII) DTM, first (S_ASCII) and last (D_ASCII) return DSM of the area in top view display are shown in Figure 21. It shows that DTMs are the representation of the bare earth while on the DSMs, all features are present such as buildings and vegetation.


Figure 21. The production of last return DSM (a) and DTM (b), first return DSM (c) and secondary DTM (d) in some portion of Mercedes Floodplain

3.7 LiDAR Image Processing and Orthophotograph Rectification

The 697 1km by 1km tiles area covered by Mercedes floodplain is shown in Figure 22. After tie point selection to fix photo misalignments, color points were added to smoothen out visual inconsistencies along the seamlines where photos overlap. The Mercedes floodplain has a total of 552.42 km2 in orthophotogaph coverage comprised of 1,319 images. A zoomed in version of sample orthophotographs named in reference to its tile number is shown in Figure 23.

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)



Figure 22. Mercedes Floodplain with available orthophotographs



Figure 23. Sample orthophotograph tiles for Mercedes floodplain

3.8 DEM Editing and Hydro-Correction

Three (3) mission blocks were processed for Mercedes flood plain. These blocks are composed of Zamboanga and Zamboanga_reflight blocks with a total area of 527.27 square kilometers. Table 15 shows the name and corresponding area of each block in square kilometers.

| LiDAR Blocks | Area (sq.km) |
|-----------------------------|--------------|
| Zamboanga_Blk75E | 394.93 |
| Zamboanga_Sacol | 96.90 |
| Zamboanga_reflights_Blk75AS | 35.24 |
| TOTAL | 527.27 sq.km |

Table 15. LiDAR blocks with its corresponding area

Portions of DTM before and after manual editing are shown in Figure 24. The river embankment (Figure 24a) has been misclassified and removed during classification process and has to be retrieved to complete the surface (Figure 24b) to allow the correct flow of water. The bridge (Figure 24c) is also considered to be an impedance to the flow of water along the river and has to be removed (Figure 24d) in order to hydrologically correct the river.



Figure 24. Portions in the DTM of Mercedes Floodplain – a paddy field before (a) and after (b) data retrieval; a bridge before (c) and after (d) manual editing.

3.9 Mosaicking of Blocks

Simultaneous mosaicking was done to all the available LiDAR data (Zamboanga_Blk75G, Zamboanga_ Blk75F, Zamboanga_Blk75E, Zamboanga_Blk75F_additional, Zamboanga_Blk75D, Zamboanga_Blk75C and Zamboanga_Sacol). Zamboanga_Blk75G was used as the reference block at the start of mosaicking because it is the first available LiDAR data. Zamboanga_reflights_Blk75AS was mosaicked to the available LiDAR data by directly incorporating the height difference to its Z value. Table 16 shows the shift values applied to each LiDAR block during mosaicking.

Mosaicked LiDAR DTM for Mercedes floodplain is shown in Figure 25. It can be seen that the entire Mercedes floodplain is 100% covered by LiDAR data.

| Mission Blocks | Shift Values (meters) | | | | |
|-----------------------------|-----------------------|------|------|--|--|
| | х | У | Z | | |
| Zamboanga_Blk75E | 0.00 | 0.00 | 0.47 | | |
| Zamboanga_Sacol | 0.00 | 0.00 | 0.47 | | |
| Zamboanga_reflights_Blk75AS | 0.00 | 0.00 | 0.44 | | |

| Table 16. Shift | Values of ea | ach LiDAR | Block of N | <i>lercedes</i> | floodplain |
|-----------------|--------------|-----------|------------|-----------------|------------|
| | | | | | |

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)



Figure 25. Map of Processed LiDAR Data for Mercedes Floodplain

3.10 Calibration and Validation of Mosaicked LiDAR DEM

The extent of the validation survey done by the Data Validation and Bathymetry Component (DVBC) in Mercedes to collect points with which the LiDAR dataset is validated is shown in Figure 26. Simultaneous mosaicking was done for the Zamboanga LiDAR blocks and the only available data that time was for Tumaga. The Mercedes flood plain is included in the set of blocks previously mosaicked, therefore, the Tumaga calibration data and methodology was used.

A total of 1,739 survey points from Tumaga data were used for calibration and validation of all the blocks of Zamboanga LiDAR data. Random selection of 80% of the survey points, resulting to 1,391 points, were used for calibration. A good correlation between the uncalibrated mosaicked LiDAR elevation values and the ground survey elevation values is shown in Figure 27. Statistical values were computed from extracted LiDAR values using the selected points to assess the quality of data and obtain the value for vertical adjustment. The computed height difference between the LiDAR DTM and calibration elevation values is 8.06 meters with a standard deviation of 0.07 meters. Calibration for Zamboanga LiDAR data was done by adding the height difference value, 8.06 meters, to Zamboanga mosaicked LiDAR data. Table 17 shows the statistical values of the compared elevation values between LiDAR data and calibration data.



Figure 26. Map of Mercedes Floodplain with validation survey points in green



Figure 27. Correlation plot between calibration survey points and LiDAR data

| Calibration Statistical Measures | Value (meters) |
|----------------------------------|----------------|
| Height Difference | 8.06 |
| Standard Deviation | 0.07 |
| Average | 8.06 |
| Minimum | 7.91 |
| Maximum | 8.20 |

Table 17. Calibration Statistical Measures

The Mercedes floodplain has a total of 1029 survey points and only 20% of the total survey points, resulting to 206 points, were randomly selected and used for the validation of calibrated Mercedes DTM. The good correlation between the calibrated mosaicked LiDAR elevation values and the ground survey elevation, which reflects the quality of the LiDAR DTM is shown in 28. The computed RMSE between the calibrated LiDAR DTM and validation elevation values is 0.12 meters with a standard deviation of 0.08 meters, as shown in Table 18.



Figure 28. Correlation plot between validation survey points and LiDAR data

| Validation Statistical Measures | Value (meters) |
|---------------------------------|----------------|
| RMSE | 0.12 |
| Standard Deviation | 0.08 |
| Average | -0.09 |
| Minimum | -0.25 |
| Maximum | 0.07 |

Table 18. Validation Statistical Measures

3.11 Integration of Bathymetric Data into the LiDAR Digital Terrain Model

For bathy integration, only centerline data was available for Mercedes with 362 bathymetric survey points. The resulting raster surface produced was done by Inverse Distance Weighted (IDW) interpolation method. After burning the bathymetric data to the calibrated DTM, assessment of the interpolated surface is represented by the computed RMSE value of 0.04 meters. The extent of the bathymetric survey done by the Data Validation and Bathymetry Component (DVBC) in Mercedes integrated with the processed LiDAR DEM is shown in Figure 29.



Figure 29. Map of Mercedes Floodplain with bathymetric survey points shown in blue

3.12 Feature Extraction

The features salient in flood hazard exposure analysis include buildings, road networks, bridges and water bodies within the floodplain area with 200 m buffer zone. Mosaicked LiDAR DEM with 1 m resolution was used to delineate footprints of building features, which consist of residential buildings, government offices, medical facilities, religious institutions, and commercial establishments, among others. Road networks comprise of main thoroughfares such as highways and municipal and barangay roads essential for routing of disaster response efforts. These features are represented by a network of road centerlines.

3.12.1 Quality Checking of Digitized Features' Boundary

Mercedes floodplain, including its 200 m buffer, has a total area of 29.39 sq km. For this area, a total of 5.0 sq km, corresponding to a total of 2,740 building features, are considered for QC. Figure 30 shows the QC blocks for Mercedes floodplain.



Figure 30. Blocks (in blue) of Mercedes building features that were subjected to QC blocks

Quality checking of Mercedes building features resulted in the ratings shown in Table 19.

| FLOODPLAIN | COMPLETENESS | CORRECTNESS | QUALITY | REMARKS |
|------------|--------------|-------------|---------|---------|
| Mercedes | 99.71 | 100.00 | 96.57 | PASSED |

Table 19. Quality Checking Ratings for Mercedes Building Features

3.12.2 Height Extraction

Height extraction was done for 12,207 building features in Mercedes floodplain. Of these building features, 169 was filtered out after height extraction, resulting to 12,038 buildings with height attributes. The lowest building height is at 2.00 m, while the highest building is at 6.86 m.

3.12.3 Feature Attribution

One of the Research Associate of ADZU Phil LiDAR 1 was able to develop GEONYT, an offline web-based application for feature attribution extracted from a LiDAR-based Digital Surface Model and which attribution is conducted by combining automatic data consolidation, geotagging and offline navigation. The app is conveniently integrated in a smart phone/ tablet. The data collected are automatically stored in database and can be viewed as CSV (or excel) and KML (can viewed via google earth). The Geonyt App was the main tool used in all feature attribution activity of the team.

The team, thru the endorsement of the Local Government Units of the Municipality/ City hired a number of enumerators who conducted the house-to-house survey of the features using the GEONYT application. The team provided the enumerators smart tablets where the GEONYT is integrated. The number of days by which the survey was conducted was dependent on the number of features of the flood plain of the riverbasin; likewise, the number of enumerators are also dependent on the availability of the tablet and the number of features of the flood plain. Table 20 summarizes the number of building features per type. On the other hand, Table 21 shows the total length of each road type, while Table 22 shows the number of water features extracted per type.

| Facility Type | No. of Features | | |
|---|-----------------|--|--|
| Residential | 11,262 | | |
| School | 136 | | |
| Market | 383 | | |
| Agricultural/Agro-Industrial Facilities | 80 | | |
| Medical Institutions | 11 | | |
| Barangay Hall | 4 | | |
| Military Institution | 1 | | |
| Sports Center/Gymnasium/Covered Court | 9 | | |
| Telecommunication Facilities | 1 | | |
| Transport Terminal | 0 | | |
| Warehouse | 12 | | |
| Power Plant/Substation | 0 | | |
| NGO/CSO Offices | 0 | | |
| Police Station | 2 | | |
| Water Supply/Sewerage | 4 | | |
| Religious Institutions | 13 | | |
| Bank | 0 | | |
| Factory | 85 | | |
| Gas Station | 0 | | |
| Fire Station | 0 | | |
| Other Government Offices | 8 | | |
| Other Commercial Establishments | 27 | | |
| Total | 12,038 | | |

Table 20. Building Features Extracted for Mercedes Floodplain

Table 21. Total Length of Extracted Roads for Mercedes Floodplain

| Floodplain | Road Network Length (km) | | | | | | |
|------------|--------------------------|------------------------|--------------------|---------------|--------|-------|--|
| | Barangay Road | City/Municipal Road | Provincial Road | National Road | Others | | |
| Mercedes | 57.93 | 22.69 | 0.00 | 6.33 | 0.00 | 86.95 | |

Table 22. Number of Extracted Water Bodies for Mercedes Floodplain

| Floodplain | Water Body Type | | | | | |
|------------|---|---|---|---|----|----|
| | Rivers/Streams Lakes/Ponds Sea Dam Fish Pen | | | | | |
| Mercedes | 8 | 0 | 1 | 0 | 84 | 93 |

A total of 9 bridges and culverts over small channels that are part of the river network were also extracted for the floodplain.

3.12.4 Final Quality Checking of Extracted Features

All extracted ground features were completely given the required attributes. All these output features comprise the flood hazard exposure database for the floodplain. This completes the feature extraction phase of the project.

Figure 31 shows the Digital Surface Model (DSM) of Mercedes floodplain overlaid with its ground features.



Figure 31. Extracted features for Mercedes Floodplain

CHAPTER 4: LIDAR VALIDATION SURVEY AND MEASUREMENTS OF THE MERCEDES RIVER BASIN

Engr. Louie P. Balicanta, Engr. Joemarie S. Caballero, Ms. Patrizcia Mae. P. dela Cruz, Engr. Dexter T. Lozano

The methods applied in this Chapter were based on the DREAM methods manual (Balicanta, et al., 2014) and further enhanced and updated in Paringit, et al. (2017).

4.1. Summary of Activities

The Data Validation and Bathymentry Component (DVBC) conducted a field survey in Culianan River from January 20 to February 1, 2015 with the following scope of work: control survey; cross-section survey and bridge as-built and water level marking of Culianan Bridge; LiDAR ground validation with an estimated length of 19.06 km; and manual bathymetric survey of the river starting from the upstream at Brgy. Salaan down to Brgy. Arena Blanco with an approximate distance of 6.68 km.



Figure 32. Extent of the Bathymetric survey (in blue line) in Mercedes River and the LiDAR data validation survey (in red)

4.2 Control Survey

The GNSS network used for Culianan River Basin is composed of a single loop and two baseline established on September 19 – 22, 2014 occupying the following reference points: ZGS-99, a second-order GCP, located off-road near the highway in Sinunoc, Zamboanga City; and ZS-177, a first-order benchmark located at the Rizal Park in Brgy. Zone IV, Zamboanga City.

Two control points were established along approach of bridges namely: ABO-1, located in Abong Bridge in Brgy. Dulian, Zamboanga City; and CUL-1, in Culianan Bridge in Brgy. Culianan, Zamboanga City. A NAMRIA established control point, namely ZGS-3508, in Brgy. Tumaga, also in Zamboanga City, was also occupied to use as marker during the survey.

The summary of reference and control points used in the survey is summarized in Table 23, while the GNSS network is illustrated in Figure 33.



Figure 33. GNSS Network covering Mercedes (Culianan) River

| Tuble 29. Else of references and control points asea in Merecaes (Sumanan) filver basis |
|---|
|---|

| Control Point | Order of | Geographic Coordinates (WGS 84) | | | | | | |
|---------------|----------------------------|---------------------------------|-------------------|--------------------------|-------------------------|---------------------|--|--|
| Name | Accuracy | Latitude | Longitude | Ellipsoid Height, (m) | Elevation in MSL (m) | Date Established | | |
| ZGS-99 | 2 nd Order, GCP | 6°55′34.07737″N | 122°00'58.23072"E | 81.427 | - | 2009 | | |
| ZS-177 | 1 st Order, BM | - | - | 80.002 | 12.311 | 2009 | | |
| ABO-1 | UP Established | - | - | - | - | 9-19-2014 | | |
| CUL-1 | UP Established | - | - | - | - | 9-20-2014 | | |
| ZGS-3508 | Used as Marker | - | - | - | - | 9-20-2014 | | |

(Source: NAMRIA, UP-TCAGP)

The GNSS set ups made in the location of the reference and control points are exhibited in Figures 34 to 38.



Figure 34. GNSS base receiver setup, Trimble® SPS 852 at ZGS-99 in Brgy. Sinunoc, Zamboanga City, Zamboanga Del Sur



Figure 35. GNSS receiver setup, Trimble® SPS 882 at ZS-177, located in Rizal Park in Brgy. Zone IV, Zamboanga City, Zamboanga Del Sur



Figure 36. GNSS receiver occupation, Trimble® SPS 852 at ABO-1 located along approach of Abong Bridge, in Brgy. Dulian, Zamboanga City, Zamboanga Del Sur



Figure 37. GNSS base receiver setup, Trimble® SPS 882 at CUL-1 along approach of Culianan Bridge in Brgy. Culianan, Zamboanga City, Zamboanga Del Sur



Figure 38. GNSS base receiver setup, Trimble® SPS 852 at ZGS-3508 along Tumaga Bridge in Brgy. Tumaga, Zamboanga City, Zamboanga Del Sur

4.3 Baseline Processing

GNSS Baselines were processed simultaneously in TBC by observing that all baselines have fixed solutions with horizontal and vertical precisions within +/- 20 cm and +/- 10 cm requirement, respectively. In cases where one or more baselines did not meet all of these criteria, masking is performed. Masking is done by removing/masking portions of these baseline data using the same processing software. It is repeatedly processed until all baseline requirements are met. If the reiteration yields out of the required accuracy, resurvey is initiated. Baseline processing result of control points in Mercedes (Culianan) River Basin is summarized in Table 24 generated by TBC software.

| Observation | Date of Observation | Solution Type | H. Prec. (Meter) | V. Prec. (Meter) | Geodetic Az. | Ellipsoid Dist. (Meter) | ΔHeight (Meter) |
|--------------------|------------------------|------------------|---------------------|---------------------|-----------------|-------------------------------|--------------------|
| ZGS-99 ABO-1 | 9-19-2014 | Fixed | 0.004 | 0.028 | 57°53'41" | 7493.070 | 37.518 |
| ZGS-99 ZS-177 | 9-19-2014 | Fixed | 0.004 | 0.019 | 109°39'22" | 7070.332 | -1.438 |
| ZGS-99 CUL-1 | 9-20-2014 | Fixed | 0.011 | 0.062 | 69°32'00" | 14392.717 | 19.213 |
| ZGS-99 ZGS-3508 | 9-20-2014 | Fixed | 0.006 | 0.020 | 83°43'43" | 6906.042 | 10.778 |
| ABO-1 ZS- 177 | 9-19-2014 | Fixed | 0.006 | 0.030 | 177°12'23" | 6368.267 | -38.883 |

Table 24. Baseline Processing Report for Mercedes (Culianan) River static survey

As shown in Table 24, a total of nine (9) baselines were processed with reference point ZGS-99 held fixed for coordinate values; and ZS-177 fixed for elevation values. All of them passed the required accuracy.

4.4 Network Adjustment

After the baseline processing procedure, network adjustment is performed using TBC. Looking at the Adjusted Grid Coordinates table of the TBC generated Network Adjustment Report, it is observed that the square root of the sum of the squares of x and y must be less than 20cm and z less than 10cm in equation from:

```
\sqrt{((x_e)^2+(y_e)^2)} <20cm and z_e < 10~cm
```

where:

xe is the Easting Error, ye is the Northing Error, and ze is the Elevation Error

For complete details, see the Network Adjustment Report shown in Table 25 to Table 27.

The five (5) control points, ZGS-99, ZS-177, ABO-1, CUL-1 and ZGS-3508 were occupied and observed simultaneously to form a GNSS loop. Coordinates of ZGS-99 and elevation values of ZS-177 were held fixed during the processing of the control points as presented in Table 25. Through these reference points, the coordinates and elevation of the unknown control points were computed.

| Point ID | Туре | East σ (Meter) | North σ (Meter) | Height σ (Meter) | Elevation σ (Meter) |
|-----------------|----------|-------------------|--------------------|---------------------|------------------------|
| ZGS-99 | Local | Fixed | Fixed | | |
| ZS-177 | Grid | | | | Fixed |
| Fixed = 0.00000 | 1(Meter) | | | | |

Table 25. Control Point Constraints

The list of adjusted grid coordinates, i.e. Northing, Easting, Elevation and computed standard errors of the control points in the network is indicated in Table 26. All fixed control points have no values for grid and elevation values.

| Point ID | Easting (Meter) | Easting Error (Meter) | Northing (Meter) | Northing Error (Meter) | Elevation (Meter) | Elevation Error (Meter) | Constraint |
|----------|--------------------|-----------------------------|---------------------|------------------------------|----------------------|-------------------------------|------------|
| BO-1 | 397667.079 | 0.006 | 769663.801 | 0.005 | 51.156 | 0.045 | |
| ZGS-99 | 391313.321 | ? | 765695.628 | ? | 13.851 | 0.035 | LL |
| ZS-177 | 397964.978 | 0.006 | 763304.232 | 0.005 | 12.311 | ? | е |

Table 26. Adjusted Grid Coordinates

With the mentioned equation, for horizontal and for the vertical; the computation for the accuracy are as follows:

| a. ZGS-99 |) | | |
|-----------|--------------------|---|--|
| h | orizontal accuracy | = | Fixed |
| v | ertical accuracy | = | cm < 10 cm |
| b. ZS-177 | , | | |
| h | orizontal accuracy | = | $\sqrt{((0.8)^2 + (0.7)^2)}$ |
| | | = | √(0.64 + 0.49) |
| | | = | 1.06 cm < 20 cm |
| v | ertical accuracy | = | Fixed |
| c ABO-1 | | | |
| h | orizontal accuracy | = | $\sqrt{((1.2)^2 + (0.9)^2)}$ |
| | , | = | √(1.44 + 0.81) |
| | | = | 1.50cm < 20 cm |
| v | ertical accuracy | = | Fixed |
| | | | |
| a. CUL-1 | orizontal accuracy | _ | $1/(1 \ 1)^2 + (1 \ 0)^2$ |
| n | | _ | $V((1.1)^{-} + (1.0)^{-})$ $V((1.21 + 1)^{-}$ |
| | | = | 1 49 cm < 20 cm |
| v | ertical accuracy | = | 8.3 cm < 10 cm |
| | , | | |
| e. ZGS-35 | 508 | | |
| h | orizontal accuracy | = | $V((1.1)^2 + (0.9)^2)$ |
| | | = | √(1.21 + 0.81) |
| | | = | 1.42 cm < 20 cm |
| v | ertical accuracy | = | 8.2 cm < 10 cm |

Following the given formula, the horizontal and vertical accuracy result of the two occupied control points are within the required accuracy of the project.

| Point ID | Latitude | Longitude | Ellipsoid | Height | Constraint |
|----------|-----------------|-------------------|-----------|--------|------------|
| ABO-1 | N6°57'43.70202" | E122°04'25.00864" | 118.918 | 0.045 | |
| ZGS-99 | N6°55'34.07737" | E122°00'58.23072" | 81.427 | 0.035 | LL |
| ZS-177 | N6°54'16.64514" | E122°04'35.11948" | 80.002 | ? | е |

| Table 27. A | Adiusted Geodetic C | Coordinates |
|-------------|---------------------|---------------|
| 10010 21.1 | iajaotea Ocoactie C | ooi chiinaceo |

The corresponding geodetic coordinates of the observed points are within the required accuracy as shown in Table 27. Based on the result of the computation, the accuracy condition is satisfied; hence, the required accuracy for the program was met.

The summary of reference and control points used is indicated in Table 28.

Table 28. Reference and control points used and its location (Source: NAMRIA, UP-TCAGP)

| | | Geograph | ic Coordinates (WGS 8 | UTM ZONE 51 N | | | |
|------------------|----------------------|-----------------|-----------------------|------------------------------|-----------------|----------------|-----------------|
| Control Point | Order of Accuracy | Latitude | Longitude | Ellipsoidal Height (m) | Northing (m) | Easting (m) | BM Ortho (m) |
| ZGS-99 | 2nd Order, GCP | 6°55'34.07737"N | 122°00'58.23072"E | 81.427 | 765695.6 | 391313.3 | 13.851 |
| ZS-177 | 1st Order, BM | 6°54′16.64514″N | 122°04'35.11948"E | 80.002 | 763304.2 | 397965 | 12.311 |
| ABO-1 | UP Established | 6°57'43.70202"N | 122°04'25.00864"E | 118.918 | 769663.8 | 397667.1 | 51.156 |
| CUL-1 | UP Established | 6°58'17.84390"N | 122°08'17.52714"E | 100.641 | 770698.8 | 404804.3 | 32.832 |
| ZGS-3508 | Used as Marker | 6°55'58.62095"N | 122°04'41.85531"E | 92.206 | 766435.6 | 398177.8 | 24.486 |

4.5 Cross-section and Bridge As-Built survey and Water Level Marking

Cross-section survey was done on September 20, 2014 along the downstream side of Culianan bridge Brgy. Salaan, Zamboanga City, Zamboanga Del Sur. A GNSS receiver Trimble® SPS 882 in GNSS PPK survey technique was used as shown in Figure 39. Control point CUL-1 was used as base station during the survey.

In addition to the cross-section survey, bridge as-built features determination was performed to get the distance of piers and abutments from the bridge approach. The bridge deck was measured using GNSS receiver Trimble[®] SPS 882 to get the high chord and meter tapes to get its low chord elevation.



Figure 39. (a) Culianan Bridge and (b) Cross-section and bridge as-built survey for Culianan Bridge

The cross-sectional line for the Culianan Bridge is about 120.29 m with 37 cross-section points. Figure 40 to Figure 42 show the summary of gathered cross-section location map, cross-section bridge in a diagram, and as-built data form.



Figure 40. Culianan bridge cross-section location map



51

| Bri | dge Na | me: Cl | JLIANAN BRIDGE | onuge De | | Da | te: | Septembe | r 20. 2014 |
|-----|--|------------------|-----------------------------|---------------------|--------------|------------------------------|---------------|--------------|------------------|
| Die | or Nan | nie. <u>- cc</u> | | | | Tim | | 10-49 am | 20,2014 |
| | ernan | ie: | | | | 100 | e | _10:46 am | |
| Loc | cation (| Brgy, Ci | ty, Region):Brgy. Culia | nan, Zamboa | anga Cit | τ γ | | | - |
| | ivey re | am: <u> </u> | VBC Zamboanga City Sur | vey ream | | | | . 6 | 2 |
| Flo | w cond | lition: | (low) normal | high | | Weather C | ond | tion: (fa | air) rainy |
| Lat | itude: | 6d58 | '18.25635" N | | | Longitude: | _1 | 22d08'17.52 | 775" E |
| | BAT | - | 0 | \sim | #BA2 | 1 | | | |
| BA1 | | | (III) | | Uns | BA4 | id: Reidaa | Approach R = | Pior IC = Low C |
| - | | | | | | Ab = | Abutin | ient D = | Deck HC = High C |
| | | Ab1 | | | Ab2 | | | | |
| | | | P | | н | | | | |
| | | | | | | | | | |
| 1 | | 22.022 | Deck (Please start your me | asurement from | the left si | de of the bank facing o | lown: | stream) | |
| lev | ation | | <u>s m (wist)</u> width: | 7.58 me | ters | Span (BA3-B/ | 42): | 39.78 | meters |
| | | | Station | | High | h Chord Elevation | | Low Cho | ord Elevation |
| 1 | ļ | | | | | | _ | | |
| 2 | | | | | | | | | |
| 3 | | | | | | | | | |
| 4 | | | | | | | | | |
| | | | Bridge Approach (Please) | tart your measureme | ent from the | left side of the bank facing | fownst | ream) | |
| Ĩ | | Statio | n(Distance from BA1) | Elevation | | Station(Distan | ice f | rom BA1) | Elevation |
| 1 | BA1 | | 0 | 31.064 | BA3 | 70.4 | 172 | 20 | 32.609 |
| 1 | BA2 | | 7.464 | 31.091 | BA4 | 117.150 | | ŝ | 33.981 |
| 1 | 1 | | | | | | | | |
| | Abu | tment: | Is the abutment sloping | ? Yes | (No;) | If yes, fill in the | follo | wing inform | ation: |
| | _ | | Station (D) | istance from | n RAIL | | | Elevatio | |
| | - | 61 | Station (D | istance from | II DAIJ | | | Lievatio | |
| | - | | | | | | | | |
| | A | bZ | | | | | | | |
| | | | PIEF (Please start your mea | surement from t | the left si | de of the bank facing o | lown: | stream) | |
| | Shape | | Number | of Piers: _0_ | | Height of colum | n fo | oting: | |
| | | | Station (Distance from | m BA1) | 1 | Elevation | | Pier V | Vidth |
| | | | | 1000 (2000 States) | | | | | |
| | Pier 1 | | | | | | | | |
| | Pier 1 Pier 2 | | | | | | | | |
| | Pier 1 Pier 2 Pier 3 | | | | | | | | |
| | Pier 1 Pier 2 Pier 3 Pier 4 | | | | | | | | |
| | Pier 1 Pier 2 Pier 3 Pier 4 Pier 5 | | | | | | | | |
| | Pier 1 Pier 2 Pier 3 Pier 4 Pier 5 Pier 6 | | | | | | | | |

Figure 42. The Culianan Bridge as-built survey data.



Figure 43. (a) Existing water level post near Culianan Bridge and (b) Water level marking

Water surface elevation of Culianan River was determined using Trimble[®] SPS 882 in PPK mode survey on January 21, 2015 at 11:00 A.M. The elevation referred to MSL was translated to the bridge pier using a Digital Level. This shall serve as a reference for flow data gathering and depth gauge deployment by the accompanying HEI, Ateneo de Zamboanga University.

4.6 Validation Points Acquisition Survey

Validation points acquisition survey was conducted on September 21, 2014 using a survey grade GNSS Rover receiver, Trimble[®] SPS 882, mounted on a pole which was attached on the side of the vehicle. It was secured with a cable tie to ensure that it was horizontally and vertically balanced. The antenna height was measured from the ground up to the bottom of the notch of the GNSS Rover receiver. The measured height of the bottom of the notch is 2.602 m from the ground. The survey was conducted using PPK technique on a continuous topography mode.

The activity started from the ZGS-3508 in Tumaga Bridge to Brgy. Manicahan with an approximate distance of 19.06 km with a total of 2,380 validation points covering the barangays of Calarian, Campo Islam, Baliwasan, Cawa-cawa, Sto. Nino, Sta. Catalina and Tumaga. Control point ZGS-3508 was used as base station for the survey.



Figure 44. (a) Ground validation set-up by: Trimble® SPS 882 mounted on a pole attached on the side of the vehicle



Figure 45. Validation acquisition points survey covering Mercedes (Culianan) River

4.7 River Bathymetric Survey

Bathymetric survey was done on January 21, 29 and 30, 2015 using Trimble[®] SPS 882 in GNSS PPK survey technique as shown in Figure 46. The survey started at the upstream part of the river in Brgy. Salaan, Zamboanga City with coordinates 6°58′16.76773″ 122°08′16.84301″, traversed down by foot and ended at the mouth of the river in Brgy. Arena Blanco, Zamboanga City with coordinates 6°55′47.99488″ 122°08′13.77668″. The control point CUL-1 was used as the GNSS base station all throughout the survey.



Figure 46. Bathymetric survey in Culianan River: (a) upstream and (b) downstream

The bathymetric line surveyed has an estimated length of 6.68 km with 269 bathynetric points covering Barangays Arena Blaco, Mercedes, Zambowood and Salaan in Zamboanga City as shown in Figure 47. Additionally, a CAD drawing was also produced to illustrate the Culianan riverbed profile as shown in Figure 48. An elevation drop of 18.7 m in MSL was observed within the approximate distance of 6.68 km. The highest elevation observed was 27.657 m in MSL located at the upstream part of the river, while the lowest elevation observed was 7.896 m in MSL located at the mouth of the river. Data gaps present were due to canopy cover along the banks of the river.



Figure 47. Bathymetric survey of Culianan River





CHAPTER 5: FLOOD MODELING AND MAPPING

Dr. Alfredo Mahar Lagmay, Christopher Uichanco, Sylvia Sueno, Marc Moises, Hale Ines, Miguel del Rosario, Kenneth Punay, and Neil Tingin

The methods applied in this Chapter were based on the DREAM methods manual (Lagmay, et al., 2014) and further enhanced and updated in Paringit, et al. (2017).

5.1 Data Used for Hydrologic Modeling

5.1.1 Hydrometry and Rating Curves

Rainfall, water level, and flow in a certain period of time, which may affect the hydrologic cycle of the Mercedes River Basin were monitored, collected, and analysed.

5.1.2 Precipitation

Precipitation data was taken from an automatic rain gauge (ARG) installed by the Department of Science and Technology – Advanced Science and Technology Institute (DOST-ASTI). The ARG was installed in the Cabonegro Repeater Station at Brgy. Bungulao, Zamboanga City (Figure 49). The precipitation data collection started from June 29, 2015 at 12:00 AM to July 4, 2015 at 11:00 PM with 10 minutes recording interval.

The total precipitation for this event in Cabonegro Repeater Station ARG was 44.6 mm. It has a peak rainfall of 13.2 mm. on July 2, 2015 at 08:00 AM. The lag time between the peak rainfall and discharge is 5 hours and 15 minutes.



Figure 49. Location map of Mercedes HEC-HMS model used for calibration

5.1.3 Rating Curves and River Outflow

A rating curve was developed at Culianan Bridge, Salaan, Zamboanga City (6°58'18.26"N, 122° 8'17.52"E). It gives the relationship between the observed water levels at Culianan Bridge and outflow of the watershed at this location.

For Culianan Bridge, the rating curve is expressed as Q = 2E-50e4.2552h as shown in Figure 51.



Culianan Bridge Cross-Section

Figure 50. Cross-Section Plot of Culianan Bridge



Figure 51. Hydrometry rating curve of Culianan Bridge
This rating curve equation was used to compute the river outflow at Culianan Bridge for the calibration of the HEC-HMS model shown in Figure 52. Peak discharge is 25.4 cubic meters per second at 1:15 PM, July 2, 2015.



Figure 52. Rainfall and outflow data at Mercedes used for modeling

5.2 RIDF Station

The Philippines Atmospheric Geophysical and Astronomical Services Administration (PAGASA) computed Rainfall Intensity Duration Frequency (RIDF) values for the Zamboanga City Rain Gauge. The RIDF rainfall amount for 24 hours was converted to a synthetic storm by interpolating and re-arranging the value in such a way certain peak value will be attained at a certain time. This station chosen based on its proximity to the Mercedes watershed. The extreme values for this watershed were computed based on a 59-year record.

| | | COMPUT | FED EXTRE | ME VALUE | S (in mm) | OF PRECI | PITATION | | |
|---------|---------|---------|-----------|----------|-----------|----------|----------|--------|--------|
| T (yrs) | 10 mins | 20 mins | 30 mins | 1 hr | 2 hrs | 3 hrs | 6 hrs | 12 hrs | 24 hrs |
| 2 | 15.5 | 23.3 | 28.4 | 36.9 | 45.6 | 50.7 | 60 | 66.1 | 77.3 |
| 5 | 21.4 | 31.6 | 38.3 | 50.4 | 61.2 | 38.2 | 82.5 | 91.5 | 107.8 |
| 10 | 25.3 | 37.1 | 44.8 | 59.4 | 71.6 | 79.8 | 97.5 | 108.3 | 127.9 |
| 15 | 27.5 | 40.2 | 48.5 | 64.4 | 77.4 | 86.4 | 105.9 | 117.8 | 139.3 |
| 20 | 29 | 42.3 | 51.1 | 68 | 81.5 | 91 | 111.8 | 124.4 | 147.3 |
| 25 | 30.2 | 44 | 53.1 | 70.7 | 84.7 | 94.5 | 116.3 | 129.5 | 153.4 |
| 50 | 33.9 | 49.1 | 59.2 | 79.1 | 94.4 | 105.4 | 130.4 | 145.3 | 172.3 |
| 100 | 37.5 | 54.2 | 65.3 | 87.4 | 104 | 116.2 | 144.3 | 161 | 191.1 |

Table 29. RIDF values for Zamboanga City Rain Gauge computed by PAGASA



Figure 53. Zamboanga City RIDF location relative to Mercedes River Basin



Figure 54. Synthetic storm generated for a 24-hr period rainfall for various return periods

5.3 HMS Model

The soil shapefile was taken before 2004 from the Bureau of Soils under the Department of Agriculture. The land cover dataset is from the National Mapping and Resource information Authority (NAMRIA). The soil and land cover of the Mercedes River Basin are shown in Figures 55 and 56, respectively.



Figure 55. Soil Map of Mercedes River Basin

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)



Figure 56. Land Cover Map of Mercedes River Basin (Source: NAMRIA)

For Mercedes, the soil classes identified were loam, clay, clay loam, hydrosols, and mountain soil. The land cover types identified were mangrove forests, grassland, cultivated areas, fishponds and closed canopy forests.



Figure 57. Stream Delineation Map of Mercedes River Basin

Using the SAR-based DEM, the Mercedes basin was delineated and further subdivided into subbasins. The model consists of 53 sub basins, 26 reaches, and 26 junctions as shown in Figure 58. The main outlet is at Culianan Bridge.

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)



Figure 58. The Mercedes river basin model generated using HEC-HMS

5.4 Cross-section Data

Riverbed cross-sections of the watershed were necessary in the HEC-RAS model setup. The cross-section data for the HEC-RAS model was derived from the LiDAR DEM data. It was defined using the Arc GeoRAS tool and was post-processed in ArcGIS.



Figure 59. River cross-section of Mercedes River generated through Arcmap HEC GeoRAS tool

5.5 Flo 2D Model

The automated modelling process allows for the creation of a model with boundaries that are almost exactly coincidental with that of the catchment area. As such, they have approximately the same land area and location. The entire area is divided into square grid elements, 10 meter by 10 meter in size. Each element is assigned a unique grid element number which serves as its identifier, then attributed with the parameters required for modelling such as x-and y-coordinate of centroid, names of adjacent grid elements, Manning coefficient of roughness, infiltration, and elevation value. The elements are arranged spatially to form the model, allowing the software to simulate the flow of water across the grid elements and in eight directions (north, south, east, west, northeast, northwest, southeast, southwest).

Based on the elevation and flow direction, it is seen that the water will generally flow from the northwest of the model to the southeast, following the main channel. As such, boundary elements in those particular regions of the model are assigned as inflow and outflow elements respectively.



Figure 60. Screenshot of subcatchment with the computational area to be modeled in FLO-2D GDS Pro

The simulation is then run through FLO-2D GDS Pro. This particular model had a computer run time of 15.90259 hours. After the simulation, FLO-2D Mapper Pro is used to transform the simulation results into spatial data that shows flood hazard levels, as well as the extent and inundation of the flood. Assigning the appropriate flood depth and velocity values for Low, Medium, and High creates the flood hazard map (Figure 61). Most of the default values given by FLO-2D Mapper Pro are used, except for those in the Low hazard level. For this particular level, the minimum h (Maximum depth) is set at 0.2 m while the minimum vh (Product of maximum velocity (v) times maximum depth (h)) is set at 0 sq.m./s.

The creation of a flood hazard map from the model also automatically creates a flow depth map depicting the maximum amount of inundation for every grid element (Figure 62). The legend used by default in Flo-2D Mapper is not a good representation of the range of flood inundation values, so a different legend is used for the layout. In this particular model, the inundated parts cover a maximum land area of 23 180 200.00 sq. m.



Figure 61. Generated 100-year rain return hazard map from FLO-2D Mapper



Figure 62. Generated 100-year rain return flow depth map from FLO-2D Mapper

There is a total of 8 609 872.07 cu.m. of water entering the model. Of this amount, 4 390 784.43 cu.m. is due to rainfall while 4 219 087.65 m3 is inflow from other areas outside the model. 2 476 688.75 cu.m. of this water is lost to infiltration and interception, while 2 389 605.22 cu.m. is stored by the floodplain. The rest, amounting up to 3 743 578.46 cu.m., is outflow.

5.6 Results of HMS Calibration

After calibrating the Mercedes HEC-HMS river basin model (see Annex 8: Mercedes Model Basin Parameters), its accuracy was measured against the observed values. Figure 63 shows the comparison between the two discharge data.



Figure 63. Outflow Hydrograph of Mercedes produced by the HEC-HMS model compared with observed outflow

Enumerated in Table 30 are the adjusted ranges of values of the parameters used in calibrating the model.

| Table 30. Range of Calibrated V | alues for Mercedes |
|---------------------------------|--------------------|
|---------------------------------|--------------------|

| Hydrologic Element | Calculation Type | Method | Parameter | Range of Calibrated Values |
|-----------------------|------------------|---------------------|----------------------------------|-------------------------------|
| | Loss | SCS Curve | Initial Abstraction (mm) | 25.98 – 99.80 |
| | LOSS | number | Curve Number | 60 – 98 |
| Basin | Transform | Clark Unit | Time of Concentration (hr) | 1.24 – 33.24 |
| | | Hydrograph | Storage Coefficient (hr) | 0.02 - 0.61 |
| | Deceflow | Decession | Recession Constant | 0.02 - 0.09 |
| | Basenow | Recession | Ratio to Peak | 0.3 |
| Reach | Routing | Muskingum- Cunge | Manning's Coefficient | 0.06 - 3211.50 |

Initial abstraction defines the amount of precipitation that must fall before surface runoff. The magnitude of the outflow hydrograph increases as initial abstraction decreases. The range of values from 25.98mm to 99.80mm means that there is a large amount of infiltration or rainfall interception by vegetation.

Curve number is the estimate of the precipitation excess of soil cover, land use, and antecedent moisture. The magnitude of the outflow hydrograph increases as curve number increases. The range of 60 to 98 for curve number is advisable for Philippine watersheds depending on the soil and land cover of the area (M. Horritt, personal communication, 2012). For Mercedes, the basin mostly consists of cultivated areas and brushlands and the soil consists of loam and clay.

Time of concentration and storage coefficient are the travel time and index of temporary storage of runoff in a watershed. The range of calibrated values from 1.24 hours to 33.24 hours determines the reaction time of the model with respect to the rainfall. The peak magnitude of the hydrograph also decreases when these parameters are increased.

Recession constant is the rate at which baseflow recedes between storm events and ratio to peak is the ratio of the baseflow discharge to the peak discharge. Recession constant of 0.02 to 0.09 indicates that the basin is moderately likely to quickly go back to its original discharge. Ratio to peak of 0.3 indicates a steeper receding limb of the outflow hydrograph.

| Accuracy measure | Value |
|------------------|-----------|
| RMSE | 23.078995 |
| r2 | 0.8145 |
| NSE | 0.59 |
| PBIAS | -24.98 |
| RSR | 0.64 |

Table 31. Summary of the Efficiency Test of Mercedes HMS Model

The Root Mean Square Error (RMSE) method aggregates the individual differences of these two measurements. It was computed as 23.078995 (m3/s).

The Pearson correlation coefficient (r2) assesses the strength of the linear relationship between the observations and the model. This value being close to 1 corresponds to an almost perfect match of the observed discharge and the resulting discharge from the HEC HMS model. Here, it measured 0.8145.

The Nash-Sutcliffe (E) method was also used to assess the predictive power of the model. Here the optimal value is 1. The model attained an efficiency coefficient of 0.59.

A positive Percent Bias (PBIAS) indicates a model's propensity towards under-prediction. Negative values indicate bias towards over-prediction. Again, the optimal value is 0. In the model, the PBIAS is -24.98.

The Observation Standard Deviation Ratio, RSR, is an error index. A perfect model attains a value of 0 when the error in the units of the valuable a quantified. The model has an RSR value of 0.64.

5.7 Calculated outflow hydrographs and discharge values for different rainfall return periods

5.7.1 Hydrograph using the Rainfall Runoff Model

The summary graph (Figure 64) shows the Mercedes outflow using the Zamboanga City Rainfall Intensity-Duration-Frequency curves (RIDF) in 5 different return periods (5-year, 10-year, 25-year, 50-year, and 100year rainfall time series) based on the Philippine Atmospheric Geophysical and Astronomical Services Administration (PAG-ASA) data. The simulation results reveal significant increase in outflow magnitude as the rainfall intensity increases for a range of durations and return periods.



Figure 64. Outflow hydrograph at Mercedes Station generated using Zamboanga City RIDF simulated in HEC-HMS

A summary of the total precipitation, peak rainfall, peak outflow and time to peak of the Mercedes discharge using the Zamboanga City Rainfall Intensity-Duration-Frequency curves (RIDF) in five different return periods is shown in Table 32.

| Table 32. Peak values of the Mercedes | s HECHMS Model outflow | using the Zamboa | nga City RIDF |
|---------------------------------------|------------------------|------------------|---------------|
| | | | |

| RIDF Period | Total Precipitation (mm) | Peak rainfall (mm) | Peak outflow (m 3/s) | Time to Peak |
|-------------|-----------------------------|--------------------|-------------------------|------------------------|
| 5-Year | 107.80 | 21.40 | 58.80 | 3 hours, 40 minutes |
| 10-Year | 127.90 | 25.30 | 78.60 | 3 hours, 30 minutes |
| 25-Year | 153.40 | 30.20 | 105.20 | 3 hours, 20 minutes |
| 50-Year | 172.30 | 33.90 | 125.8 | 3 hours, 20 minutes |
| 100-Year | 191.10 | 37.50 | 146.8 | 3 hours, 10 minutes |

5.8 River Analysis (RAS) Model Simulation

The HEC-RAS Flood Model produced a simulated water level at every cross-section for every time step for every flood simulation created. The resulting model will be used in determining the flooded areas within the model. The simulated model will be an integral part in determining real-time flood inundation extent of the river after it has been automated and uploaded on the DREAM website. The sample generated map of Mercedes River using the calibrated HMS base flow is shown in Figure 65.



Figure 65. Sample output of Mercedes RAS Model

5.9 Flow Depth and Flood Hazard

The resulting hazard and flow depth maps have a 10m resolution. Figure 66 to Figure 71 shows the 5-, 25-, and 100-year rain return scenarios of the Mercedes floodplain. The floodplain, with an area of 23.22 sq. km., covers the Zamboanga City. Table 33 shows the percentage of area affected by flooding per municipality.

| Municipality | Total Area | Area Flooded | % Flooded |
|-------------------|------------|--------------|-----------|
| Zamboanga City | 146.29 | 21.77 | 15% |

Table 33. Municipalities affected in Mercedes Floodplain



Figure 66. 100-year Flood Hazard Map for Mercedes (also known as Culianan) Floodplain



Figure 67. 100-year Flow Depth Map for Mercedes (also known as Culianan) Floodplain



Figure 68. 25-year Flood Hazard Map for Mercedes (also known as Culianan) Floodplain



Figure 69. 25-year Flow Depth Map for Mercedes (also known as Culianan) Floodplain



Figure 70. 5-year Flood Hazard Map for Mercedes (also known as Culianan) Floodplain



Figure 71. 5-year Flow Depth Map for Mercedes (also known as Culianan) Floodplain

5.10 Inventory of Areas Exposed to Flooding

Affected barangays in Mercedes river basin in Zamboanga City are listed below. For the said basin, 10 barangays are expected to experience flooding when subjected to to the three rainfall events.

For the 5-year return period, 1.36% of Zamboanga City with an area of 1496.293 sq. km. will experience flood levels of less than 0.20 meters. 0.16% of the area will experience flood levels of 0.21 to 0.50 meters while 0.07%, 0.03%, 0.03%, and 0.01% of the area will experience flood depths of 0.51 to 1 meter, 1.01 to 2 meters, 2.01 to 5 meters, and more than 5 meters, respectively. Listed in Table 34 are the affected areas in square kilometers by flood depth per barangay.

| iall Return Period |
|--------------------|
| -Year Rain |
| / during 5 |
| nga City |
| n Zamboar |
| ed Areas i |
| : 34. Affect |
| able |

| Affected Areas (in sq. km.) by | | | | Affec | ted Barangays | in Zamboanga | City | | | |
|-----------------------------------|-------------------|----------|----------|----------|---------------|--------------|------------|--------|----------|-----------|
| (in m.) | Arena Blan- co | Culianan | Lanzones | Lumayang | Lumbangan | Mercedes | Pasobolong | Salaan | Talabaan | Zambowood |
| < 0.21 | 1.3 | 0.44 | 0.81 | 1.28 | 0.047 | 6.69 | 1.35 | 3.57 | 0.0065 | 2.39 |
| 0.21 - 0.50 | 0.21 | 0.041 | 0.016 | 0.056 | 0.0011 | 1.11 | 0.17 | 0.27 | 0 | 0.26 |
| 0.51 - 1.00 | 0.0016 | 0.013 | 0.0078 | 0.011 | 0 | 0.33 | 0.07 | 0.18 | 0 | 0.19 |
| 1.01 - 2.00 | 0.0015 | 0.017 | 0.0085 | 0.013 | 0 | 0.14 | 0.025 | 0.084 | 0 | 0.096 |
| 2.01 - 5.00 | 0.00073 | 0 | 0.024 | 0.038 | 0 | 0.089 | 0.00048 | 0.19 | 0 | 0.037 |
| > 5.00 | 0 | 0 | 0.0061 | 0.017 | 0 | 0.01 | 0 | 0.14 | 0 | 0.0064 |
| | | | | | | | | | | |





For the 25-year return period, 1.20% of Zamboanga City with an area of 1496.293 sq. km. will experience flood levels of less than 0.20 meters. 0.22% of the area will experience flood levels of 0.21 to 0.50 meters while 0.12%, 0.06%, 0.03%, and 0.02% of the area will experience flood depths of 0.51 to 1 meter, 1.01 to 2 meters, 2.01 to 5 meters, and more than 5 meters, respectively. Listed in the table are the affected areas in square kilometers by flood depth per barangay.

Zambowood 0.0079 0.056 2.27 0.28 0.17 0.2 Talabaan 0.0065 0 0 0 0 0 Salaan 3.23 0.13 0.18 0.35 0.31 0.21 Pasobolong 0.0043 0.064 0.93 0.15 0.47 0 Affected Barangays in Zamboanga City Mercedes 0.012 0.15 5.92 0.82 0.27 1.2 Lumbangan 0.0019 0.047 0 0 0 0 Lumayang 0.068 0.015 0.038 0.011 0.044 1.24 Lanzones 0.0092 0.0073 0.018 0.023 0.021 0.8 Culianan 0.0036 0.041 0.28 0.17 0.02 0 Arena Blan-0.0014 0.00091 0.059 0.92 0.54 8 0 km.) by flood Areas (in sq. depth (in m.) 0.21 - 0.50 0.51 - 1.00 1.01 - 2.00 2.01 - 5.00 Affected < 0.21 > 5.00

Table 35. Affected Areas in Zamboanga City during 25-Year Rainfall Return Period





For the 100-year return period, 1.12% of Zamboanga City with an area of 1496.293 sq. km. will experience flood levels of less than 0.20 meters. 0.23% of the area will experience flood levels of 0.21 to 0.50 meters while 0.15%, 0.07%, 0.05%, and 0.03% of the area will experience flood depths of 0.51 to 1 meter, 1.01 to 2 meters, 2.01 to 5 meters, and more than 5 meters, respectively. Listed in Table 36 are the affected areas in square kilometers by flood depth per barangay.

Zambowood 0.0084 2.18 0.28 0.19 0.14 0.17 Talabaan 0.0065 0 0 0 0 0 Salaan 3.06 0.19 0.38 0.38 0.18 0.24 Table 36. Affected Areas in Zamboanga City during 100-Year Rainfall Return Period Pasobolong 0.0081 0.082 0.77 0.27 0.5 0 Affected Barangays in Zamboanga City Mercedes 0.015 5.55 1.190.18 1.03 0.4 Lumbangan 0.0024 0.046 0 0 0 0 Lumayang 0.073 0.021 0.013 0.034 0.064 1.21 Lanzones 0.0094 0.0053 0.018 0.017 0.79 0.04 Culianan 0.0074 0.084 0.023 0.22 0.17 0 Arena Blan-0.0014 0.00097 0.77 0.58 0.17 8 0 km.) by flood Areas (in sq. depth (in m.) 0.21 - 0.50 0.51 - 1.00 1.01 - 2.00 2.01 - 5.00 Affected < 0.21 > 5.00





87

Moreover, the generated flood hazard maps for the Mercedes Floodplain were used to assess the vulnerability of the educational and medical institutions in the floodplain. Using the flood depth units of PAG-ASA for hazard maps - "Low", "Medium", and "High" - the affected institutions were given their individual assessment for each Flood Hazard Scenario (5 yr, 25 yr, and 100 yr).

| Warning Level | Area | Covered in sq | . km. |
|---------------|--------|---------------|----------|
| | 5 year | 25 year | 100 year |
| Low | 3.73 | 5.96 | 6.48 |
| Medium | 1.53 | 3.02 | 4.18 |
| High | 1.41 | 1.98 | 2.33 |
| Total | 6.67 | 10.96 | 12.99 |

Table 37. Summary of the Accuracy Assessment in the Mercedes River Basin Survey

Of the 14 identified Education Institutes in Mercedes floodplain, 1 school was assessed to be exposed to the Low level flooding during a 5 year scenario. In the 25 year scenario, 2 schools were assessed to be exposed to the Low level flooding. For the 100 year scenario, 3 schools were assessed for Low level flooding. The educational institutions exposed to flooding in the Mercedes floodplain are found in Annex 12.

Seven (7) Medical Institutions were identified in Mercedes floodplain, none were assessed to be exposed to any of the flood hazard levels at any of the rainfall scenarios.

5.11 Flood Validation

In order to check and validate the extent of flooding in different river systems, a validation survey work was performed. Field personnel gathered secondary data regarding flood occurrence in the area within the major river system in the Philippines.

From the Flood Depth Maps produced by Phil-LiDAR 1 Program, multiple points representing the different flood depths for different scenarios were identified for validation.

The validation personnel went to the specified points identified in a river basin and gathered data regarding the actual flood level in each location. Data gathering was done through a local DRRM office to obtain maps or situation reports about the past flooding events and interviews from some residents with knowledge of or have had experienced flooding in a particular area. The flood validation data were obtained on September 24, 2016.

The actual data from the field were compared to the simulated data to assess the accuracy of the Flood Depth Maps produced and to improve on what is needed.

The flood validation consists of 128 points randomly selected all over the Mercedes floodplain. It has an RMSE value of 0.70.



Figure 75. Validation points for 5-year Flood Depth Map of Mercedes Floodplain



Figure 76. Flood map depth vs actual flood depth

| Actual Modeled | | ed Flood Depth (m) | | | | | |
|--------------------|--------|--------------------|-----------|-----------|-----------|--------|-------|
| Flood Depth (m) | 0-0.20 | 0.21-0.50 | 0.51-1.00 | 1.01-2.00 | 2.01-5.00 | > 5.00 | Total |
| 0-0.20 | 30 | 5 | 4 | 0 | 0 | 0 | 39 |
| 0.21-0.50 | 35 | 7 | 3 | 4 | 1 | 0 | 50 |
| 0.51-1.00 | 1 | 3 | 11 | 3 | 1 | 0 | 19 |
| 1.01-2.00 | 0 | 1 | 4 | 3 | 1 | 1 | 10 |
| 2.01-5.00 | 0 | 0 | 0 | 4 | 6 | 0 | 10 |
| > 5.00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 66 | 16 | 22 | 14 | 9 | 1 | 128 |

Table 38. Actual Flood Depth vs Simulated Flood Depth in Mercedes

The overall accuracy generated by the flood model is estimated at 44.53%, with 57 points correctly matching the actual flood depths. In addition, there were 55 points estimated one level above and below the correct flood depths while there were 12 points and 1 point estimated two levels above and below, and three or more levels above and below the correct flood. A total of 23 points were overestimated while a total of 48 points were underestimated in the modelled flood depths of Mercedes.

| | No. of Points | % |
|----------------|---------------|-------|
| Correct | 73 | 31.06 |
| Overestimated | 25 | 10.64 |
| Underestimated | 137 | 58.30 |
| Total | 235 | 100 |

Table 39. Summary of Accuracy Assessment in Mercedes

REFERENCES

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UP TCAGP 2016, Acceptance and Evaluation of Synthetic Aperture Radar Digital Surface Model (SAR DSM) and Ground Control Points (GCP). Quezon City, Philippines: UP Training Center for Applied Geodesy and Photogrammetry.

ANNEXES

Annex 1. Technical Specifications of the LIDAR Sensors used in the Mercedes Floodplain Survey





| Parameter | Specification |
|---------------------------------|---|
| Operational envelope (1,2,3,4) | 150-5000 m AGL, nominal |
| Laser wavelength | 1064 nm |
| Horizontal accuracy (2) | 1/5,500 x altitude, 1σ |
| Elevation accuracy (2) | < 5-20 cm, 1σ |
| Effective laser repetition rate | Programmable, 100-500 kHz |
| Position and orientation system | POS AV ™AP50 (OEM) |
| Scan width (FOV) | Programmable, 0-75 ° |
| Scan frequency (5) | Programmable, 0-140 Hz (effective) |
| Sensor scan product | 800 maximum |
| Beam divergence | 0.25 mrad (1/e) |
| Roll compensation | Programmable, ±37° (FOV dependent) |
| Vertical target separation dis- | <0.7 m |
| tance | |
| Range capture | Up to 4 range measurements, including 1st, 2nd, 3rd, and last |
| | returns |
| Intensity capture | Up to 4 intensity returns for each pulse, including last (12 bit) |

Table A1-1. Parameters and Specification of Sensor

| Image capture | 5 MP interline camera (standard); 60 MP full frame (optional) |
|-----------------------|---|
| Full waveform capture | 12-bit Optech IWD-2 Intelligent Waveform Digitizer |
| Data storage | Removable solid state disk SSD (SATA II) |
| Power requirements | 28 V, 800 W, 30 A |
| Dimensions and weight | Sensor: 630 x 540 x 450 mm; 65 kg; |
| | Control rack: 650 x 590 x 490 mm; 46 kg |
| Operating Temperature | -10°C to +35°C |
| Relative humidity | 0-95% non-condensing |

1 Target reflectivity ≥20%

2 Dependent on selected operational parameters using nominal FOV of up to 40° in standard atmospheric conditions with 24-km visibility

3 Angle of incidence ≤20°

4 Target size ≥ laser footprint5 Dependent on system configuration

Table A1-2. Parameters and Specifications of the D-8900 Aerial Digital Camera

| Parameter | Specification | | | |
|------------------------|--|--|--|--|
| Camera Head | | | | |
| Sensor type | 60 Mpix full frame CCD, RGB | | | |
| Sensor format (H x V) | 8, 984 x 6, 732 pixels | | | |
| Pixel size | 6μm x 6 μm | | | |
| Frame rate | 1 frame/2 sec. | | | |
| FMC | Electro-mechanical, driven by piezo technology (patented) | | | |
| Shutter | Electro-mechanical iris mechanism 1/125 to 1/500++ sec. f-stops: 5.6, 8, 11, 16 | | | |
| Lenses | 50 mm/70 mm/120 mm/210 mm | | | |
| Filter | Color and near-infrared removable filters | | | |
| Dimensions (H x W x D) | 200 x 150 x 120 mm (70 mm lens) | | | |
| Weight | ~4.5 kg (70 mm lens) | | | |
| Controller Unit | | | | |
| Computer | Mini-ITX RoHS-compliant small-form-factor embedded computers with AMD TurionTM 64 X2 CPU 4 GB RAM, 4 GB flash disk local storage IEEE 1394 Firewire interface | | | |
| Removable storage unit | ~500 GB solid state drives, 8,000 images | | | |
| Power consumption | ~8 A, 168 W | | | |
| Dimensions | 2U full rack; 88 x 448 x 493 mm | | | |
| Weight | ~15 kg | | | |
| Ima | ge Pre-Processing Software | | | |
| Capture One | Radiometric control and format conversion, TIFF or JPEG | | | |
| Image output | 8,984 x 6,732 pixels 8 or 16 bits per channel (180 MB or 360 MB per image) | | | |

Annex 2. NAMRIA Certificates of Reference Points used in the LIDAR Survey

1. ZGS-100

| | NATIONAL MAP | nment and Natural | | AUTHORITY | | |
|---|---|------------------------|---|---------------|-------------------|--------------------------------|
| | | | | | | August 29, 20 |
| | | CEF | TIFICATION | | | |
| To whom it may co | ncern: | | | | | |
| This is to certify | / that according to th | ne records on | file in this office, the requ | uested survey | inform | ation is as follow |
| | F | Province: ZAM | BOANGA DEL SUR | | | |
| | | Station N | ame: ZGS-100 | | | |
| | | Orde | :: 2nd | | | |
| Island: MINDAN Municipality: 74 | AO MBOANGA CITY | Barangay: MSL Eleva | MANICAHAN | | | |
| | | PRS | 92 Coordinates | | | |
| Latitude: 7º 1' | 26.72368" | Longitude: | 122º 11' 12.74401" | Ellipsoid | al Hgt: | 11.27000 m. |
| | | WGS | 84 Coordinates | | | |
| Latitude: 7º 1' | 23.30149" | Longitude: | 122° 11' 18.30044" | Ellipsoid | al Hgt: | 75.60300 m. |
| | | PTM / P | RS92 Coordinates | | | |
| Northing: 7767 | 12.542 m. | Easting: | 410158.521 m. | Zone: | 4 | |
| Northing: 776.4 | 440.68 | UTM / F Easting: | RS92 Coordinates 410.189.97 | Zone: | 51 | |
| canal with inscriptic pole 7 meters km p Requesting Party: Purpose: OR Number: T.N.: | on " ŹGS-100, ŻÒ09 ost 1916-ZC22 ENGR. CHRISTO Reference 8799780 A 2014-1902 | NAMRIA".Loc | ated at Manicahan Barar R Director / | UEL DM. BE | eters So EN, M | I NSA Gue esy Branch |
| | | | | | | |

2. ZGS-99

| CERTIFICATION | | |
|--|--|---|
| | | |
| | | |
| the records on file in this office, the req | uested survey inform | hation is as follow |
| Province: ZAMBOANGA DEL SUR | | |
| Station Name: ZGS-99 | | |
| Order: 2nd Pacapage CALAPIAN | | |
| MSL Elevation: | | |
| PRS92 Coordinates | | |
| Longitude: 122º 0' 52.66431" | Ellipsoidal Hgt | 8.14900 m. |
| WGS84 Coordinates | | |
| Longilude: 122° 0' 58.23072" | Ellipsoidal Hgt: | 72.23000 m. |
| PTM / PRS92 Coordinates | | |
| Easting: 391103.346 m. | Zone: 4 | |
| UTM / PRS92 Coordinates Easting: 391,141.46 | Zone: 51 | |
| Location Description | 1000000 1000 | |
| | | |
| ill, 10 m from the centerline and 50 m fr nail flushed at the center of a cement p C. | om the Airforce Bea outly on a concrete o | ch, in Brgy. Uppe pen canal with |
| OPHER CRUZ | | |
| | 1Anna/ | |
| | 1 the Day | |
| Directo | Mapping And Geo | desy Branch |
| | / - | - I |
| / | | |
| | | |
| | | |
| | | |
| | | |
| 00110 | | it internation (1940) |
| | the records on file in this office, the req Province: ZAMBOANGA DEL SUR Station Name: ZGS-99 Order: 2nd Barangay: CALARIAN MSL Elevation: PRS92 Coordinates Longitude: 122° 0° 52.66431° WGS84 Coordinates Longitude: 122° 0° 59.23072° PTM / PRS92 Coordinates Easting: 391103.346 m. UTM / PRS92 Coordinates Easting: 391,141.46 Location Description II, 10 m from the center of a cement pro- DPHER CRUZ | the records on file in this office, the requested survey inform Province: ZAMBOANGA DEL SUR Station Name: ZGS-99 Order: 2nd Barangay: CALARIAN MSL Elevation: PRS92 Coordinates Longitude: 122° 0° 52.66431° Ellipsoidal Hgt: WGS84 Coordinates Longitude: 122° 0° 59.23072° Ellipsoidal Hgt: PTM / PRS92 Coordinates Easting: 391103.346 m, Zone: 4 UTM / PRS92 Coordinates Easting: 391,141.46 Zone: 51 Location Description II, 10 m from the center of a cement pully on a concrete o DPHER CRUZ RDEL DM, BELEN, 1 Director Mapping And Geo |

Figure A2-1. ZGS-99

Annex 3. Base Processing Report of Control Points used in the LIDAR Survey

1. ZS-131

| From: | ZGS-100 | | | | |
|------------|--------------|-----------|-------------------|-----------|-------------------|
| Grid Local | | Global | | | |
| Easting | 410189.967 m | Latitude | N7°01'26.72367" | Latitude | N7°01'23.30149" |
| Northing | 776440.678 m | Longitude | E122°11'12.74401" | Longitude | E122°11'18.30044" |
| Elevation | 7.745 m | Height | 11.271 m | Height | 75.603 m |

| To: | ZS-131 | ZS-131 | | | | |
|------------|--------------|-----------|-------------------|-----------|-------------------|--|
| Grid Local | | | Global | | | |
| Easting | 414826.524 m | Latitude | N7°12'31.41328" | Latitude | N7°12'27.94616" | |
| Northing | 796844.403 m | Longitude | E122°13'42.74840" | Longitude | E122°13'48.28765" | |
| Elevation | 7.052 m | Height | 10.811 m | Height | 74.904 m | |

| Vector | | | | | |
|-------------------|-------------|-----------------|-------------|----|-------------|
| ΔEasting | 4636.557 m | NS Fwd Azimuth | 12°42'06" | ΔX | -2545.750 m |
| <u>ANorthing</u> | 20403.725 m | Ellipsoid Dist. | 20930.290 m | ΔY | -4593.707 m |
| <u>AElevation</u> | -0.693 m | <u>Alleight</u> | -0.460 m | ۸Z | 20260.657 m |

| Vector errors: | | | | | |
|---------------------------|---------|-------------------|----------|-----|---------|
| σ <u>AEasting</u> | 0.002 m | σ NS fwd Azimuth | 0°00'00" | σΔΧ | 0.005 m |
| σ <u>ANorthing</u> | 0.001 m | σ Ellipsoid Dist. | 0.001 m | σΔΥ | 0.008 m |
| σ <mark>ΔElevation</mark> | 0.009 m | σ <u>Alleight</u> | 0.009 m | σΔZ | 0.002 m |

Aposteriori Covariance Matrix (Meter*)

| | х | Y | Z |
|---|---------------|--------------|--------------|
| x | 0.0000227893 | | |
| Y | -0.0000323435 | 0.0000634026 | |
| z | -0.0000043665 | 0.0000093098 | 0.0000024763 |

Figure A3-1. ZS-131
2. BLLM-166

| 200 | 100 - BELMITO (12.33.14 FM-3.24.39 FM) (32) |
|------------------------|---|
| Baseline observation: | ZGS 100 BLLM166 (B2) |
| Processed: | 3/5/2015 5:24:48 PM |
| Solution type: | Fixed |
| Frequency used: | Dual Frequency (L1, L2) |
| Horizontal precision: | 0.004 m |
| Vertical precision: | 0.017 m |
| RMS: | 0.007 m |
| Maximum PDOP: | 1.981 |
| Ephemeris used: | Broadcast |
| Antenna model: | NGS Absolute |
| Processing start time: | 2/5/2015 12:55:34 PM (Local: UTC+8hr) |
| Processing stop time: | 2/5/2015 5:24:39 PM (Local: UTC+8hr) |
| Processing duration: | 04:29:05 |
| Processing interval: | 5 seconds |
| | |

ZGS 100 - BLLM166 (12:55:14 PM-5:24:39 PM) (S2)

Figure A3-2. BLLM-166

Vector Components (Mark to Mark)

| From: | ZGS 100 | | | | | | |
|-------------------|--------------|---------|-----------------|--------|-------------|----|-------------------|
| | Grid | | Local | | | G | ilobal |
| Easting | 410189.967 m | Latitud | N7°01'26. | 72367" | Latitude | | N7°01'23.30149" |
| Northing | 776440.678 m | Longitu | ude E122°11'12. | 74401" | Longitude | | E122°11'18.30044" |
| Elevation | 7.745 m | Height | t 11 | .271 m | Height | | 75.603 m |
| To: | BLLM166 | | | | | | |
| | Grid | | Local | | Giobal | | |
| Easting | 415179.269 m | Latitud | N7°09'33. | 60926" | Latitude | | N7°09'30.15553" |
| Northing | 791383.716 m | Longitu | ude E122°13'54. | 54820" | Longitude | | E122°14'00.09187" |
| Elevation | 120.669 m | Height | 124 | .333 m | n Helght | | 188.527 m |
| Vector | | | | | | | |
| ∆Easting | 4989.30 | 2 m N | S Fwd Azimuth | | 18°21'47" | ΔX | -3276.482 m |
| ΔNorthing | 14943.03 | 88 m El | lipsoid Dist. | 83 | 15758.784 m | ΔY | -4113.808 m |
| ∆Elevation | 112.92 | 23 m 🕰 | Height | | 113.062 m | ΔZ | 14855.907 m |

Standard Errors

| Vector errors: | | | | | | | |
|---------------------------|---------|-------------------|----------|-----|---------|--|--|
| σ ΔEasting | 0.002 m | σ NS fwd Azlmuth | 0°00'00" | σΔΧ | 0.005 m | | |
| σΔNorthing | 0.001 m | σ Ellipsoid Dist. | 0.001 m | σΔΥ | 0.007 m | | |
| $\sigma \Delta Elevation$ | 0.009 m | σΔHeight | 0.009 m | σΔΖ | 0.002 m | | |

3. ZGS-99A

| ZGS-99 - ZGS-99A | (9:00:34 AM | -1:46:19 PM | (\$1) |
|------------------|-------------|-------------|-------|
| F00-00 - F00-00H | | | |

| Baseline observation: | ZGS-99 ZGS-99A (B1) |
|------------------------|---------------------------------------|
| Processed: | 3/6/2015 1:27:43 PM |
| Solution type: | Fixed |
| Frequency used: | Dual Frequency (L1, L2) |
| Horizontal precision: | 0.001 m |
| Vertical precision: | 0.001 m |
| RMS: | 0.000 m |
| Meximum PDOP: | 4.130 |
| Ephemeria used: | Broadcast |
| Antenna model: | NGS Absolute |
| Processing start time: | 2/11/2015 9:00:34 AM (Local: UTC+8hr) |
| Processing stop time: | 2/11/2015 1:46:19 PM (Local: UTC+8hr) |
| Proceeding duration: | 04:45:45 |
| Proceesing Interval: | 5 seconds |
| | |

1

Figure A3-3. ZGS-99A

Vector Components (Mark to Mark)

| From: | ZGS-99 | | | | | | |
|-------------------|--------------|-------------------|-------------------|------------|--------|-------------------|--|
| | Grid | Local | | | Giobal | | |
| Easting | 391141.462 m | Latitude | N6°55'37.48971" | Latitude | | N6°55'34.07737" | |
| Northing | 765752.270 m | Longitude | E122°00'52.66432* | Longitude | | E122°00'58.23072* | |
| Elevation | 4.653 m | Height | 8.149 m | Height | | 72.230 m | |
| To: | ZGS-99A | | | | | | |
| | Grid | | Local | Giobal | | | |
| Easting | 391136.071 m | Latitude | N6°55'37.63895" | Latitude | | N6°55'34.22659" | |
| Northing | 765756.864 m | Longitude | E122°00'52.48834* | Longitude | | E122°00'58.05475* | |
| Elevation | 4.354 m | Height | 7.850 m | n Height | | 71.931 m | |
| Vector | | | | | | | |
| ΔEasting | -5.39 | 1 m NS Fwd Azir | muth | 310°19'07* | ΔX | 5.031 m | |
| ∆Northing | 4.59 | 4 m Ellipsoid Dis | Ł | 7.085 m | ΔY | 2.144 m | |
| ∆Elevation | -0.29 | 9 m AHeight | | -0.299 m | ΔZ | 4.515 m | |

Standard Errors

| Vector errors: | | | | | | | |
|----------------|---------|-------------------|----------|-----|---------|--|--|
| σ ΔEasting | 0.000 m | σ NS fwd Azimuth | 0°00'11" | σΔΧ | 0.000 m | | |
| σ ΔNorthing | 0.000 m | σ Ellipsoid Dist. | 0.000 m | σΔY | 0.001 m | | |
| σ ΔElevation | 0.001 m | σ ΔHeight | 0.001 m | σΔZ | 0.000 m | | |

Aposteriori Covariance Matrix (Meter*)

| | x | Y | z |
|---|---------------|--------------|-------------|
| x | 0.000002239 | | |
| Y | -0.0000001250 | 0.0000004533 | |
| z | -0.000000277 | 0.000000071 | 0.000000770 |

4. BVA-1

BVA-1 - BVA-2 (2:54:04 PM-5:12:34 PM) (S1)

| Baseline observation: | BVA-1 BVA-2 (B1) |
|------------------------|--------------------------------------|
| Processed: | 3/6/2015 3:31:41 PM |
| Solution type: | Fixed |
| Frequency used: | Dual Frequency (L1, L2) |
| Horizontal precision: | 0.001 m |
| Vertical precision: | 0.002 m |
| RMS: | 0.000 m |
| Maximum PDOP: | 2.093 |
| Ephements used: | Broadcast |
| Antenna model: | NGS Absolute |
| Processing start time: | 2/6/2015 2:54:04 PM (Local: UTC+8hr) |
| Processing stop time: | 2/6/2015 5:12:34 PM (Local: UTC+8hr) |
| Processing duration: | 02:18:30 |
| Processing interval: | 5 seconds |
| | |

Vector Components (Mark to Mark)

| From: | BVA-1 | BVA-1 | | | | | | |
|------------|--------------|-------|-----------------|-------------------|------------|----|-------------------|--|
| | Grid | Local | | al | Global | | | |
| Easting | 418087.142 m | Latit | tude | N7°15'19.31910" | Latitude | | N7°15'15.84241" | |
| Northing | 801995.112 m | Long | gitude | E122°15'28.78739" | Longitude | | E122°15'34.32212" | |
| Elevation | 78.652 m | Heig | ght | 82.446 m | Height | | 146.526 m | |
| To: | BVA-2 | | | | | | | |
| | Grid | | Local | | Global | | ilobal | |
| Easting | 418085.472 m | Latit | tude | N7°15'19.25198" | Latitude | | N7°15'15.77529" | |
| Northing | 801993.053 m | Long | gitude | E122°15'28.73303" | Longitude | | E122°15'34.26776" | |
| Elevation | 78.729 m | Heig | ght | 82.524 m | n Height | | 146.603 m | |
| Vector | | | | | | | | |
| ∆Easting | -1.67 | '0 m | NS Fwd Azimuth | | 218°57'49" | ΔX | 1.230 m | |
| ∆Northing | -2.05 | i9 m | Ellipsoid Dist. | | 2.652 m | ΔY | 1.175 m | |
| ∆Elevation | 0.07 | 7 m | ΔHeight | | 0.077 m | ΔZ | -2.036 m | |

Standard Errors

| Vector errors: | | | | | | | |
|----------------|---------|-------------------|----------|-----|---------|--|--|
| σ ΔEasting | 0.000 m | σ NS fwd Azimuth | 0°00'28" | σΔΧ | 0.001 m | | |
| σΔNorthing | 0.000 m | σ Ellipsoid Dist. | 0.000 m | σΔΥ | 0.001 m | | |
| σ ΔElevation | 0.001 m | σ∆Height | 0.001 m | σΔΖ | 0.000 m | | |

Figure A3-4. BVA-1

| Data Acquisition Component Sub- Team | Designation | Name | Agency/ Affiliation |
|--|--|-----------------------------------|--|
| PHIL-LIDAR 1 | Program Leader | ENRICO C. PARINGIT, D.ENG | UP-TCAGP |
| Data Acquisition Component Leader | Data Component Project Leader – I | ENGR. CZAR JAKIRI S. SARMIENTO | UP-TCAGP |
| Survey Supervisor | Chief Science Research Specialist (CSRS) | ENGR. CHRISTOPHER CRUZ | UP-TCAGP |
| LiDAR Operation | Senior Science Research Specialist (SSRS) | LOVELY GRACIA ACUNA | UP-TCAGP |
| LiDAR Operation | Senior Science Research Specialist (SSRS) | JASMINE ALVIAR | UP-TCAGP |
| LiDAR Operation | Senior Science Research Specialist (SSRS) | ENGR. IRO NIEL ROXAS | UP-TCAGP |
| | Research Associate (RA) | ENGR. RENAN PUNTO | UP-TCAGP |
| LiDAR Operation | RA | KRISTINE JOY ANDAYA | UP-TCAGP |
| LiDAD Operation | RA | JONATHAN ALMALVEZ | UP-TCAGP |
| LIDAR Operation | RA | SANDRA POBLETE | UP-TCAGP |
| Ground Survey | RA | FRANK NICOLAS ILEJAY | UP-TCAGP |
| LiDAR Operation | Airborne Security | ERWIN DELOS SANTOS | PILIPPINE AIR FORCE (PAF) |
| LiDAR Operation | Airborne Security | JAYCO MANZANO | PILIPPINE AIR FORCE (PAF) |
| LiDAR Operation | Pilot | CAPT. SHERWIN CESAR ALFONSO | ASIAN AEROSPACE COR- PORATION (AAC) |
| LiDAR Operation | Pilot | CAPT. BRYAN DONGUINES | AAC |
| LiDAR Operation | Pilot | CAPT. ANTON DAYO | AAC |

Annex 4. The LIDAR Survey Team Composition

Table A-4.1. The LiDAR Survey Team Composition



Annex 5. Data Transfer Sheet for Mercedes Floodplain

Figure A-5.1. Transfer Sheet for Mercedes Floodplain-A

| | | LOCATION | Z:\DAC\RAW DATA | Z:\DAC\RAW DATA | Z:\DAC\RAW DATA | Z:\DAC\RAW DATA | Z:\DAC\RAW DATA | Z:IDACIRAW DATA |
|----------------------------------|--------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|
| | PLAN | KML | NA | NA | NA | NA | NA | NA |
| | FLIGHT | Actual | 53 | 89 | NA | NA | NA | NA |
| | OPERATOR | (OPLOG) | NA | NA | NA | NA | NA | NA |
| | TION(S) | 3ase Info (.txt) | 1KB | 1KB | 1KB | 1KB | 1KB | 1KB |
| | BASE STA | BASE STATION(S) | 95.8 | 133 | 133 | 153 | 171 | 171 |
| | | NA | NA | NA | NA | NA | NA | |
| RANGE | | 5.63 | 24.7 | 5.13 | 22.6 | 7.88 | 12.6 | |
| MISSION LOG FILE/CASI LOGS | | NA | NA | NA | 274 | 69 | 139 | |
| RAW MAGES/CASI | | A N | NA | NA | 30 | 8.73 | 15.3 | |
| | POS | | 91 | 253 | 101 | 281 | 173 | 192 |
| | LOGS | | 4.08 | 11 | 3.37 | 11.6 | 60.9 | 6.75 |
| AC NC | CHO | (ML (swath) | NA | NA | NA | NA | NA | NA |
| WVd | NAM | Dutput LAS | 518 | 2.28 | 506 | 2.09 | 546 | 1.1 |
| | SENSOR | | PEGASUS | PEGASUS | PEGASUS | PEGASUS | PEGASUS | PEGASUS |
| | MISSION NAME | | 1BLK75BS146A | 1BLK75FG147A | 1BLK75AS147B | 1BLK75CSDE148B | 1BLK75HI151A | 1BLK75CS151B |
| | ON ANOI I | LIGHT NU. | 23390P | 23392P | 23394P | 23398P | 23408P | 23410P |
| | LATE - | NAIE | May 25, 2016 | May 26, 2016 | May 26, 2016 | May 27, 2016 | May 30, 2016 | May 30, 2016 |

Received from

righter

Figure A-5.2. Transfer Sheet for Mercedes Floodplain-B

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)

Annex 6. Flight Logs for the Flight Missions

1. Flight Log for 2535P Mission



Figure A-6.1. Flight Log for 2535P Mission

Flight Log No.: 255 5 Aircraft Type: Cesnna T206H 6 Aircraft Identification: $RP - CO0.2^{10}$ 18 Total Flight Time: $q \neq 0/$ ature over Printed Name Alwiqur Lidar Operator 12 Airport of Arrival (Airport, City/Province): # 1239 18 17 Landing: Signature over Printed Name Culpure II Pilot-in-Command 4 Type: VFR 2 ALTM Model: V2005US 3 Mission Name: 184755304 Albuco 8 Co-Pilot: 8 Dougaines 9 Route: 12 Airport of Departure (Airport, City/Province): 15 Total Engine Time: イ ナル Sneesful pright Acquisition Flight Certified by Signature over Printed Name (PAF Representative) Ef Junter Zow boanga + 4 421 Choudun 14 Engine Off: forthy Acquisition Flight Approved by over Printed Name UDAR Operator: J. AIVIOV (End User Representative) **MM Data Acquisition Flight Log** 21012 Feb. 8 , 2015 1 21 Problems and Solutions: 0833 A Engine On: Remarks: Weather Date: Pilot:

2. Flight Log for 2545P Mission

Figure A-6.2. Flight Log for 2545P Mission

3. Flight Log for 2557P Mission



Figure A-6.3 Flight Log for 2557P Mission

4. Flight Log for 23394P Mission



Figure A-6.4. Flight Log for 23394P Mission

Annex 7. Flight Status Reports

Zamboanga-Zamboanga Sibugay Mission February 5,8 and 11 2015; May 26, 2016

| Table A-7. | 1 | Flight | Status | Report |
|------------|---|--------|--------|---------|
| 100107171 | _ | | otatab | 1.cpoit |

| FLIGHT NO | AREA | MISSION | OPERATOR | DATE FLOWN | REMARKS |
|--------------|---|--------------|----------------------------|---------------|--|
| 2535P | BLK75E | 1BLK75E36A | J. ALVIAR | Feb. 5, 2015 | FOR COMPLETION AND SOME GAP FILLING (TER- RAIN) |
| 2545P | BLK75C BLK75D BLK75E BLK75FS | 1BLK75C39A | J. ALVIAR | Feb. 7, 2015 | ABNORMAL PROGRAM TER- MINATION (AVPOS) |
| 2557P | BLK75C BLK75D BLK75GS- BLK75FS- SACOL IS. | 1BLK75S42A | J. ALVIAR | Feb. 11, 2015 | SURVEY 6 DESCENDED TO 1000 DUE TO CLOUDS; RETURNED TO 1100M FOR SURVEY OVER SACOL; GAPS DUE TO CLOUDS, DESCENDED TO 1000M TO FILL UP VOIDS IN SACOL AND BLK 75EFG; ADDED 1 SMALL LINE (COR- RIDOR 18), DESCENDED TO 800M; CORRIDOR 16 WHICH SHOULD COVER GAP IN BLK75E, UP TO ALL |
| 23394P | BLK75AS | 1BLK75AS147B | I. ROXAS and S. POBLETE | May 26, 2016 | COMPLETED BLK 75AS |

LAS/SWATH BOUNDARIES PER MISSION FLIGHT

Flight No.: 2535P

Area: BLK75E

Mission Name: 1BLK75E36A

Parameters: Altitude: 1100m; Scan Frequency: 30; Scan Angle: 50



LAS/SWATH

Figure A-7.1. Swath for Flight No. 2535P

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)

| Flight No. : | 2545P |
|----------------------|---|
| Area: | BLK 75C |
| Mission Name: 1BLK75 | C39A |
| Parameters: | Altitude: 1100m; Scan Frequency: 30; Scan Angle: 50 |



Figure A-7.2. Swath for Flight No. 2545P

Flight No. :2557PArea:BLK 75C, D, E, GS, FS, Sacol islandMission Name:1BLK75S42Parameters:Altitude: 800-1200m; Scan Frequency: 30; Scan Angle: 50



Figure A-7.3. Swath for Flight No. 2557P

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)

Flight No.:23394PArea:BLK75ASMission Name:1BLK75AS147BParameters:Altitude: 1000m; Scan Frequency: 30; Scan Angle: 50



LAS/SWATH

Figure A-7.4. Swath for Flight No. 23394P

Annex 8. Mission Summary Reports

Figure A-8.1. Mission summary report for Blk75E

| Flight Area | Zamboanga |
|--|--|
| Mission Name | Blk75E |
| Inclusive Flights | 2535P, 2545P |
| Mission Name | 1BLK75E36A, 1BLK75C39A |
| Range data size | 56.9 GB |
| Base data size | 15.3 MB |
| POS | 491 MB |
| Image | 85.3 GB |
| Transfer date | March 13 2015 |
| | |
| Solution Status | |
| Number of Satellites (>6) | Yes |
| PDOP (<3) | Yes |
| Baseline Length (<30km) | Yes |
| Processing Mode (<=1) | Yes |
| | |
| Smoothed Performance Metrics(in cm) | |
| RMSE for North Position (<4.0 cm) | 1.08 |
| RMSE for East Position (<4.0 cm) | 1.42 |
| RMSE for Down Position (<8.0 cm) | 2.94 |
| | |
| Boresight correction stdev (<0.001deg) | 0.000223 |
| IMU attitude correction stdev (<0.001deg) | 0.000328 |
| GPS position stdev (<0.01m) | 0.0061 |
| | |
| Minimum % overlap (>25) | 96.73% |
| Ave point cloud density per sq.m. (>2.0) | 5.11 |
| Elevation difference between strips (<0.20m) | Yes |
| | |
| Number of 1km x 1km blocks | 522 |
| Maximum Height | 498.00 m |
| Minimum Height | 65.50 m |
| | |
| Classification (# of points) | |
| Ground | 369,443,876 |
| Low vegetation | 268,989,359 |
| Medium vegetation | 403,829,240 |
| High vegetation | 815,604,498 |
| Building | 37,951,116 |
| Orthophoto | Yes |
| Processed by | Engr. Analyn Naldo, Engr. Cherlou Prado, Alex John Escobido |



Figure A-8.1 Solution Status



Figure A-8.2 Smoothed Performance Metric Parameters



Figure A-8.3 Best Estimated Trajectory



Figure A-8.4 Coverage of LiDAR data

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)



Figure A-8.5 Image of data overlap



Figure A-8.6 Density map of merged LiDAR data



Figure A-8.7 Elevation difference between flight lines

| Flight Area | Zamboanga |
|---|--|
| Mission Name | Sacol |
| Inclusive Flights | 2557P |
| Mission Name | 1BLK75S42A |
| Range data size | 20.5 GB |
| Base data size | 8.47 MB |
| POS | 255 MB |
| Image | 34.9 GB |
| Transfer date | March 3 2015 |
| | |
| Solution Status | |
| Number of Satellites (>6) | Yes |
| PDOP (<3) | Yes |
| Baseline Length (<30km) | No |
| Processing Mode (<=1) | No |
| | |
| Smoothed Performance Metrics(in cm) | |
| RMSE for North Position (<4.0 cm) | 1.07 |
| RMSE for East Position (<4.0 cm) | 1.72 |
| RMSE for Down Position (<8.0 cm) | 3.35 |
| | |
| Boresight correction stdev (<0.001deg) | 0.000189 |
| IMU attitude correction stdev (<0.001deg) | 0.001474 |
| GPS position stdey (<0.01m) | 0.0028 |
| | |
| Minimum % overlap (>25) | 93.75% |
| Ave point cloud density per sq.m. (>2.0) | 4.29 |
| Elevation difference between strips (<0.20m) | Yes |
| | |
| Number of 1km x 1km blocks | 183 |
| Maximum Height | 422.16 m |
| Minimum Height | 67.62 m |
| | |
| Classification (# of points) | |
| Ground | 102,448,806 |
| Low vegetation | 102,238,659 |
| Medium vegetation | 104,811,352 |
| High vegetation | 138,074,781 |
| Building | 1,942,211 |
| Orthophoto | Yes |
| Processed by | Engr. Irish Cortez, Engr. Melanie Hingpit, Alex Escobido |



Figure A-8.8 Solution Status



Figure A-8.9 Smoothed Performance Metric Parameters



Figure A-8.10 Best Estimated Trajectory



Figure A-8.11 Coverage of LiDAR data



Figure A-8.12 Image of data overlap



Figure A-8.13 Density map of merged LiDAR data



Figure A-8.14 Elevation difference between flight lines

| Flight Area | Zamboanga Reflights |
|---|--|
| Mission Name | Blk75AS |
| Inclusive Flights | 23394P |
| Range data size | 5.13 GB |
| POS data size | 101 MB |
| Base data size | 133 MB |
| Image | n/a |
| Transfer date | July 14, 2016 |
| | |
| Solution Status | |
| Number of Satellites (>6) | Yes |
| PDOP (<3) | Yes |
| Baseline Length (<30km) | No |
| Processing Mode (<=1) | Yes |
| | |
| Smoothed Performance Metrics (in cm) | |
| RMSE for North Position (<4.0 cm) | 0.9 |
| RMSE for East Position (<4.0 cm) | 1.1 |
| RMSE for Down Position (<8.0 cm) | 3.4 |
| | |
| Boresight correction stdev (<0.001deg) | n/a |
| IMU attitude correction stdev (<0.001deg) | n/a |
| GPS position stdev (<0.01m) | n/a |
| | |
| Minimum % overlap (>25) | 27.08 |
| Ave point cloud density per sq.m. (>2.0) | 2.98 |
| Elevation difference between strips (<0.20 m) | Yes |
| | |
| Number of 1km x 1km blocks | 60 |
| Maximum Height | 588.90 m |
| Minimum Height | 77.48 m |
| | |
| Classification (# of points) | |
| Ground | 31,359,118 |
| Low vegetation | 14,011,685 |
| Medium vegetation | 34,188,233 |
| High vegetation | 107,683,623 |
| Building | 2,927,347 |
| | |
| Orthophoto | No |
| Processed by | Ben Joseph J. Harder, Engr. Christy Lubiano, Engr. Jeffrey Delica |

Table A-8.3 Mission summary report for Blk75AS



Figure A-8.15 Solution Status



Figure A-8.16 Smoothed Performance Metric Parameters



Figure A-8.17 Best Estimated Trajectory



Figure A-8.18 Coverage of LiDAR data



Figure A-8.19 Image of data overlap



Figure A-8.20 Density map of merged LiDAR data



Figure A-8.21 Elevation difference between flight lines

| Annex 9 | . Mercedes N | Model Bas | in Paramet | ers | | | | | | |
|---------|--------------------------------|------------------|-------------------|----------------------------------|--------------------------------|----------------|--------------------------------|-----------------------|----------------|------------------|
| | | | | Table A-9.1. M | lercedes Mode | el Basin Parar | neters | | | |
| | SCS C | urve Numbe | er Loss | Clark Unit Hy Transfi | ydrograph orm | | Å | ecession Bas | eflow | |
| Number | Initial Abstraction (mm) | Curve Number | Impervious (%) | Time of Concentration (HR) | Storage Coefficient (HR) | Initial Type | Initial Discharge (M3/S) | Recession Constant | Threshold Type | Ratio to Peak |
| W1060 | 89.4762765 | 65.24625 | 0 | 33.2352 | 0.6102 | Discharge | 0.0170781 | 0.0850453 | Ratio to Peak | 0.3 |
| W1050 | 99.8023455 | 60 | 0 | 5.33168 | 0.0978903 | Discharge | 0.0023982 | 0.0177778 | Ratio to Peak | 0.3 |
| W1040 | 99.8023455 | 60 | 0 | 7.12128 | 0.13075 | Discharge | 0.0042494 | 0.0177778 | Ratio to Peak | 0.3 |
| W1030 | 99.8023455 | 60 | 0 | 6.17512 | 0.11337 | Discharge | 0.0027858 | 0.0177778 | Ratio to Peak | 0.3 |
| W1020 | 99.8023455 | 60 | 0 | 7.1932 | 0.13207 | Discharge | 0.002686 | 0.0177778 | Ratio to Peak | 0.3 |
| W1010 | 99.8023455 | 60 | 0 | 9.144 | 0.1678887 | Discharge | 0.0055049 | 0.0261333 | Ratio to Peak | 0.3 |
| W1000 | 99.8023455 | 60 | 0 | 6.64904 | 0.12208 | Discharge | 0.0030129 | 0.0118519 | Ratio to Peak | 0.3 |
| 066M | 99.6826545 | 60.06125 | 0 | 6.1552 | 0.11301 | Discharge | 0.003054 | 0.0177778 | Ratio to Peak | 0.3 |
| W980 | 64.8163035 | 77.77375 | 0 | 8.9952 | 0.16515 | Discharge | 0.0087509 | 0.0177778 | Ratio to Peak | 0.3 |
| W970 | 85.140198 | 66.94625 | 0 | 12.8256 | 0.23548 | Discharge | 0.0086802 | 0.0177778 | Ratio to Peak | 0.3 |
| 096M | 34.5417345 | 93.1525 | 0 | 5.15568 | 0.0946588 | Discharge | 0.0038322 | 0.0177778 | Ratio to Peak | 0.3 |

0.3 0.3 0.3 0.3 0.3 0.3 0.3

Ratio to Peak

0.0026143 0.0035329 0.0023997

> Discharge Discharge

> > 0.0516956

2.81568 2.82496 4.3912 1.49448

97.5 97.5

25.983828 25.983828

97.5

25.983828

Ratio to Peak

0.0177778 0.0177778 0.0177778 0.0261333 0.0261333 0.0261333 0.0177778 0.0177778 0.0177778

0.00067037

Discharge Discharge

0.0269706 0.0865201 0.0724862

1.46896 4.7124 3.94808

00000000

97.5

25.983828

W950

92.79125

34.0738515

W940 W930 W920 W910 W900 W890

Ratio to Peak Ratio to Peak

> 0.0021405 0.0024559 0.000146408 0.0011116

Discharge Discharge

0.0518658 0.0806226 0.0170781

Discharge

0.0274384

Discharge Discharge

0.0507525 0.6102

2.76432 33.2352

0

65.24625

W1060

97.5

25.983828 89.4762765

W880

89.29375 97.5

40.081977 25.983828

Ratio to Peak

| | SCS CL | Irve Numbe | r Loss | Clark Unit Hy Transfo | /drograph orm | | Ř | ecession Bas | eflow | |
|-----|-------------------------------|-----------------|-------------------|----------------------------------|--------------------------------|--------------|--------------------------------|-----------------------|----------------|------------------|
| | Initial bstraction (mm) | Curve Number | Impervious (%) | Time of Concentration (HR) | Storage Coefficient (HR) | Initial Type | Initial Discharge (M3/S) | Recession Constant | Threshold Type | Ratio to Peak |
| | 99.8023455 | 60 | 0 | 5.33168 | 0.0978903 | Discharge | 0.0023982 | 0.0177778 | Ratio to Peak | 0.3 |
| | 25.983828 | 97.5 | 0 | 3.12456 | 0.0573674 | Discharge | 0.0014054 | 0.0177778 | Ratio to Peak | 0.3 |
| | 25.983828 | 97.5 | 0 | 4.46288 | 0.0819383 | Discharge | 0.000353486 | 0.0177778 | Ratio to Peak | 0.3 |
| | 25.983828 | 97.5 | 0 | 3.82056 | 0.0701454 | Discharge | 0.0025556 | 0.0177778 | Ratio to Peak | 0.3 |
| I I | 30.474054 | 94.88625 | 0 | 4.69288 | 0.086162 | Discharge | 0.0036296 | 0.0177778 | Ratio to Peak | 0.3 |
| 1 | 25.983828 | 97.5 | 0 | 6.2492 | 0.11474 | Discharge | 0.0026233 | 0.0177778 | Ratio to Peak | 0.3 |
| I | 25.983828 | 97.5 | 0 | 3.274 | 0.0601103 | Discharge | 0.00026173 | 0.0177778 | Ratio to Peak | 0.3 |
| | 25.983828 | 97.5 | 0 | 2.98528 | 0.0548098 | Discharge | 0.0017654 | 0.0177778 | Ratio to Peak | 0.3 |
| | 25.983828 | 97.5 | 0 | 3.46144 | 0.0635522 | Discharge | 0.0024804 | 0.0177778 | Ratio to Peak | 0.3 |
| | 27.2659725 | 96.75375 | 0 | 7.75112 | 0.14231 | Discharge | 0.00736 | 0.0177778 | Ratio to Peak | 0.3 |
| | 25.983828 | 97.5 | 0 | 4.52408 | 0.0830624 | Discharge | 0.0025993 | 0.0177778 | Ratio to Peak | 0.3 |
| | 25.983828 | 97.5 | 0 | 5.86728 | 0.10772 | Discharge | 0.0057761 | 0.0177778 | Ratio to Peak | 0.3 |
| | 25.983828 | 97.5 | 0 | 3.27296 | 0.0600909 | Discharge | 0.0011221 | 0.0177778 | Ratio to Peak | 0.3 |
| | 25.983828 | 97.5 | 0 | 3.7292 | 0.0684681 | Discharge | 0.0025476 | 0.0177778 | Ratio to Peak | 0.3 |
| | 33.7038975 | 93.5775 | 0 | 5.34456 | 0.0981256 | Discharge | 0.00664 | 0.0177778 | Ratio to Peak | 0.3 |
| | 48.794031 | 85.9125 | 0 | 6.42424 | 0.11795 | Discharge | 0.0036005 | 0.0177778 | Ratio to Peak | 0.3 |
| | 39.1988025 | 89.83375 | 0 | 5.27096 | 0.0967748 | Discharge | 0.008066 | 0.0177778 | Ratio to Peak | 0.3 |
| | 25.983828 | 97.5 | 0 | 3.75648 | 0.0689691 | Discharge | 0.0040182 | 0.0177778 | Ratio to Peak | 0.3 |
| | 25.983828 | 97.5 | 0 | 1.24272 | 0.0228171 | Discharge | 6.17E-05 | 0.0177778 | Ratio to Peak | 0.3 |
| | 80.5284675 | 68.6425 | 0 | 7.20248 | 0.13224 | Discharge | 0.0058303 | 0.0177778 | Ratio to Peak | 0.3 |
| | 25.983828 | 97.5 | 0 | 2.17104 | 0.0398601 | Discharge | 0.0012008 | 0.0177778 | Ratio to Peak | 0.3 |
| | 36.1339875 | 92.34375 | 0 | 3.15808 | 0.0579824 | Discharge | 0.0024177 | 0.0177778 | Ratio to Peak | 0.3 |
| | 27.336699 | 96.8125 | 0 | 4.05248 | 0.0744029 | Discharge | 0.002874 | 0.0261333 | Ratio to Peak | 0.3 |
| | 32.9966325 | 93.9375 | 0 | 3.72744 | 0.0684355 | Discharge | 0.002502 | 0.0830131 | Ratio to Peak | 0.3 |

| | SCS CI | urve Numbe | r Loss | Clark Unit Hy Transfo | /drograph orm | | R | ecession Bas | eflow | |
|--------|--------------------------------|-----------------|-------------------|----------------------------------|--------------------------------|--------------|--------------------------------|-----------------------|----------------|------------------|
| Number | Initial Abstraction (mm) | Curve Number | Impervious (%) | Time of Concentration (HR) | Storage Coefficient (HR) | Initial Type | Initial Discharge (M3/S) | Recession Constant | Threshold Type | Ratio to Peak |
| W640 | 53.9534385 | 83.29125 | 0 | 5.56528 | 0.10218 | Discharge | 0.0036472 | 0.0177778 | Ratio to Peak | 0.3 |
| W630 | 99.8023455 | 60 | 0 | 2.60632 | 0.0478523 | Discharge | 0.000317887 | 0.0177778 | Ratio to Peak | 0.3 |
| W620 | 91.897299 | 62.8325 | 0 | 7.82472 | 0.14366 | Discharge | 0.0059426 | 0.0177778 | Ratio to Peak | 0.3 |
| W610 | 92.205594 | 63.86 | 0 | 8.396 | 0.15415 | Discharge | 0.0024017 | 0.0177778 | Ratio to Peak | 0.3 |
| W600 | 93.6001755 | 62.22125 | 0 | 8.3048 | 0.15247 | Discharge | 0.0035409 | 0.0177778 | Ratio to Peak | 0.3 |
| W590 | 99.8023455 | 60 | 0 | 8.6 | 0.1579 | Discharge | 0.0025 | 0.0177778 | Ratio to Peak | 0.3 |
| W580 | 99.8023455 | 60 | 0 | 8.3472 | 0.15326 | Discharge | 0.0027742 | 0.0261333 | Ratio to Peak | 0.3 |
| W570 | 98.806734 | 60.3575 | 0 | 14.232 | 0.2613 | Discharge | 0.0088707 | 0.038416 | Ratio to Peak | 0.3 |
| W560 | 86.8031775 | 66.60375 | 0 | 16.632 | 0.30536 | Discharge | 0.0099934 | 0.0177778 | Ratio to Peak | 0.3 |
| W550 | 99.8023455 | 60 | 0 | 9.208 | 0.16906 | Discharge | 0.0022959 | 0.038416 | Ratio to Peak | 0.3 |
| W540 | 92.321658 | 62.68 | 0 | 11.52 | 0.21151 | Discharge | 0.007167 | 0.0177778 | Ratio to Peak | 0.3 |
| | | | | | | | | | | |

| | | Muskin | gum Cunge Ch | annel Routing | J. J | | |
|-----------------|--------------------------|---------------|--------------|----------------|--|-------|---------------|
| Reach Number | Time Step Method | Length (m) | Slope | Manning's n | Shape | Width | Side Slope |
| R70 | Automatic Fixed Interval | 241.42 | 0.0555019 | 241.42 | Trapezoid | 30 | 1 |
| R90 | Automatic Fixed Interval | 1084.3 | 0.0245221 | 1084.3 | Trapezoid | 30 | 1 |
| R110 | Automatic Fixed Interval | 1153.3 | 0.039488 | 1153.3 | Trapezoid | 30 | 1 |
| R130 | Automatic Fixed Interval | 3211.5 | 0.0556812 | 3211.5 | Trapezoid | 30 | 1 |
| R140 | Automatic Fixed Interval | 987.7 | 0.0544809 | 987.7 | Trapezoid | 30 | 1 |
| R150 | Automatic Fixed Interval | 647.7 | 0.0512279 | 647.7 | Trapezoid | 30 | 1 |
| R160 | Automatic Fixed Interval | 206.57 | 0.0408191 | 206.57 | Trapezoid | 30 | 1 |
| R190 | Automatic Fixed Interval | 1140.1 | 0.0086207 | 1140.1 | Trapezoid | 30 | 1 |
| R210 | Automatic Fixed Interval | 1664.4 | 0.0405305 | 1664.4 | Trapezoid | 30 | 1 |
| R230 | Automatic Fixed Interval | 795.27 | 0.011228 | 795.27 | Trapezoid | 30 | 1 |
| R260 | Automatic Fixed Interval | 513.85 | 0.0111499 | 513.85 | Trapezoid | 30 | 1 |
| R270 | Automatic Fixed Interval | 1834.4 | 0.0184486 | 1834.4 | Trapezoid | 30 | 1 |
| R280 | Automatic Fixed Interval | 823.14 | 0.0038411 | 823.14 | Trapezoid | 30 | 1 |
| R310 | Automatic Fixed Interval | 304.85 | 0.0001 | 304.85 | Trapezoid | 30 | 1 |
| R320 | Automatic Fixed Interval | 446.27 | 0.0581721 | 446.27 | Trapezoid | 30 | 1 |
| R330 | Automatic Fixed Interval | 258.99 | 0.0901284 | 258.99 | Trapezoid | 30 | 1 |
| R380 | Automatic Fixed Interval | 517.7 | 0.0001 | 517.7 | Trapezoid | 30 | 1 |
| R390 | Automatic Fixed Interval | 548.7 | 0.15237 | 548.7 | Trapezoid | 30 | 1 |
| R410 | Automatic Fixed Interval | 322.13 | 0.0497242 | 322.13 | Trapezoid | 30 | 1 |
| R420 | Automatic Fixed Interval | 841.54 | 0.0292951 | 841.54 | Trapezoid | 30 | 1 |
| R430 | Automatic Fixed Interval | 1100.5 | 0.0359817 | 0.055 | Trapezoid | 30 | 1 |
| R460 | Automatic Fixed Interval | 720.12 | 0.0106701 | 0.055 | Trapezoid | 30 | 1 |
| R480 | Automatic Fixed Interval | 926.69 | 0.0079047 | 0.055 | Trapezoid | 30 | 1 |
| R490 | Automatic Fixed Interval | 1085.7 | 0.0102168 | 0.055 | Trapezoid | 30 | 1 |
| R520 | Automatic Fixed Interval | 840.83 | 0.0209252 | 0.055 | Trapezoid | 30 | 1 |
| R530 | Automatic Fixed Interval | 6254.1 | 0.0069262 | 0.055 | Trapezoid | 30 | 1 |

Annex 10. Mercedes Model Reach Parameters

Annex 11. Mercedes Field Validation Points

| Point Number | Validation Coordinates | | Model | Validation | _ | _ | Rain Return / |
|-----------------|------------------------|------------|---------|------------|-------|------------------|---------------|
| | Lat | Long | Var (m) | Points (m) | Error | Event/Date | Scenario |
| 1 | 6.976665 | 122.143505 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year |
| 2 | 6.976443 | 122.145085 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year |
| 3 | 6.977991 | 122.143201 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year |
| 4 | 6.97558 | 122.143046 | 0.07 | 0 | 0.07 | Not Defined | 5 -Year |
| 5 | 6.959618 | 122.13433 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year |
| 6 | 6.95924 | 122.135899 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year |
| 7 | 6.961229 | 122.136953 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year |
| 8 | 6.976423 | 122.134849 | 2.4 | 0 | 2.4 | Not Defined | 5 -Year |
| 9 | 6.971876 | 122.132071 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year |
| 10 | 6.976897 | 122.128723 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year |
| 11 | 6.978754 | 122.132458 | 1.04 | 0.4 | 0.64 | Not Defined | 5 -Year |
| 12 | 6.963961 | 122.1384 | 0.09 | 0 | 0.09 | Not Defined | 5 -Year |
| 13 | 6.959974 | 122.14538 | 0.12 | 0 | 0.12 | Not Defined | 5 -Year |
| 14 | 6.97573 | 122.133466 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year |
| 15 | 6.976993 | 122.147619 | 0.04 | 0.5 | -0.46 | 24-09-2016 | 5 -Year |
| 16 | 6.977125 | 122.147955 | 0.03 | 0.2 | -0.17 | 24-09-2016 12:00 | 5 -Year |
| 17 | 6.976631 | 122.148146 | 0.1 | 0.2 | -0.1 | 24-09-2016 12:00 | 5 -Year |
| 18 | 6.977236 | 122.148097 | 0.03 | 0.3 | -0.27 | 24-09-2016 12:00 | 5 -Year |
| 19 | 6.977328 | 122.148079 | 0.03 | 0.3 | -0.27 | 24-09-2016 12:00 | 5 -Year |
| 20 | 6.979267 | 122.147259 | 0.03 | 0.1 | -0.07 | 24-09-2016 | 5 -Year |
| 21 | 6.985896 | 122.125847 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year |
| 22 | 6.935078 | 122.136338 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year |
| 23 | 6.937477 | 122.136629 | 0.98 | 0 | 0.98 | Not Defined | 5 -Year |
| 24 | 6.958621 | 122.147919 | 0.05 | 0 | 0.05 | Not Defined | 5 -Year |
| 25 | 6.959433 | 122.148016 | 0.05 | 0 | 0.05 | Not Defined | 5 -Year |
| 26 | 6.960551 | 122.147955 | 0.25 | 0 | 0.25 | Not Defined | 5 -Year |
| 27 | 6.96012 | 122.14699 | 0.39 | 0 | 0.39 | Not Defined | 5 -Year |
| 28 | 6.963291 | 122.146748 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year |
| 29 | 6.957424 | 122.148369 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year |
| 30 | 6.955897 | 122.148411 | 0.04 | 0 | 0.04 | Not Defined | 5 -Year |
| 31 | 6.954823 | 122.148533 | 0.09 | 0 | 0.09 | Not Defined | 5 -Year |
| 32 | 6.953963 | 122.148341 | 0.06 | 0 | 0.06 | Not Defined | 5 -Year |
| 33 | 6.958259 | 122.148559 | 0.11 | 0 | 0.11 | Not Defined | 5 -Year |
| 34 | 6.959304 | 122.150327 | 0.07 | 0 | 0.07 | Not Defined | 5 -Year |
| 35 | 6.959021 | 122.149355 | 0.05 | 0 | 0.05 | Not Defined | 5 -Year |
| 36 | 6.958224 | 122.149578 | 0.07 | 0 | 0.07 | Not Defined | 5 -Year |
| 37 | 6.956278 | 122.147747 | 0.04 | 0 | 0.04 | Not Defined | 5 -Year |
| 38 | 6.954977 | 122.146799 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year |
| 39 | 6.956702 | 122.149089 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year |
| 40 | 6.957809 | 122.15122 | 0.12 | 0 | 0.12 | Not Defined | 5 -Year |
| 41 | 6.956317 | 122.150502 | 0.06 | 0 | 0.06 | Not Defined | 5 -Year |
| 42 | 6.95563 | 122.149202 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year |

Table A-11.1. Mercedes Field Validation Points
| Point Number | Validation Coordinates | | Model Var (m) | Validation | Error | Event/Date | Rain Return / Scenario | |
|-----------------|------------------------|------------|------------------|-------------|-------|-------------|---------------------------|--|
| Number | Lat | Long | vai (iii) | r onnto (m) | | | | |
| 43 | 6.957007 | 122.149818 | 0.05 | 0 | 0.05 | Not Defined | 5 -Year | |
| 44 | 6.954257 | 122.150001 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 45 | 6.953566 | 122.149583 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 46 | 6.954442 | 122.151587 | 0.43 | 0 | 0.43 | Not Defined | 5 -Year | |
| 47 | 6.960753 | 122.141674 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 48 | 6.958233 | 122.143733 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 49 | 6.958525 | 122.144438 | 0.09 | 0 | 0.09 | Not Defined | 5 -Year | |
| 50 | 6.956174 | 122.139885 | 1.01 | 0 | 1.01 | Not Defined | 5 -Year | |
| 51 | 6.956328 | 122.141591 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 52 | 6.953001 | 122.141358 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 53 | 6.947972 | 122.142702 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 54 | 6.946268 | 122.142414 | 0.16 | 0 | 0.16 | Not Defined | 5 -Year | |
| 55 | 6.945994 | 122.140669 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 56 | 6.943915 | 122.142858 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 57 | 6.94408 | 122.140836 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 58 | 6.952821 | 122.149529 | 0.25 | 0 | 0.25 | Not Defined | 5 -Year | |
| 59 | 6.942131 | 122.142963 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 60 | 6.952642 | 122.150789 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 61 | 6.951375 | 122.149419 | 0.18 | 0 | 0.18 | Not Defined | 5 -Year | |
| 62 | 6.949184 | 122.150419 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 63 | 6.950001 | 122.15117 | 0.06 | 0 | 0.06 | Not Defined | 5 -Year | |
| 64 | 6.950089 | 122.152264 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 65 | 6.948201 | 122.152621 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 66 | 6.952477 | 122.146069 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 67 | 6.952422 | 122.147321 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 68 | 6.951106 | 122.147332 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 69 | 6.950606 | 122.148442 | 0.06 | 0 | 0.06 | Not Defined | 5 -Year | |
| 70 | 6.949852 | 122.145655 | 0.11 | 0 | 0.11 | Not Defined | 5 -Year | |
| 71 | 6.947785 | 122.148927 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 72 | 6.945411 | 122.147364 | 0.07 | 0 | 0.07 | Not Defined | 5 -Year | |
| 73 | 6.945059 | 122.151743 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 74 | 6.943398 | 122.150438 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 75 | 6.938752 | 122.142516 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 76 | 6.939455 | 122.143878 | 0.26 | 0 | 0.26 | Not Defined | 5 -Year | |
| 77 | 6.935419 | 122.144819 | 0.07 | 0 | 0.07 | Not Defined | 5 -Year | |
| 78 | 6.936236 | 122.141962 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 79 | 6.934196 | 122.143523 | 0.06 | 0 | 0.06 | Not Defined | 5 -Year | |
| 80 | 6.933027 | 122.142687 | 0.07 | 0 | 0.07 | Not Defined | 5 -Year | |
| 81 | 6.939857 | 122.146849 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 82 | 6.941786 | 122.146858 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 83 | 6.938288 | 122.153636 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 84 | 6.937655 | 122.149076 | 0.04 | 0 | 0.04 | Not Defined | 5 -Year | |
| 85 | 6.939285 | 122.149639 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 86 | 6.939583 | 122.151442 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 87 | 6.935978 | 122.150372 | 0.3 | 0 | 0.3 | Not Defined | 5 -Year | |
| 88 | 6.941308 | 122.139958 | 0.42 | 0 | 0.42 | Not Defined | 5 -Year | |

| Point | Validation Coordinates | | Model | Validation | Error | Event/Date | Rain Return / | |
|--------|------------------------|------------|-----------|------------|-------|-------------|---------------|--|
| Number | Lat | Long | vai (iii) | | | | Scenario | |
| 89 | 6.938397 | 122.138509 | 0.32 | 0 | 0.32 | Not Defined | 5 -Year | |
| 90 | 6.940123 | 122.137204 | 0.27 | 0 | 0.27 | Not Defined | 5 -Year | |
| 91 | 6.966029 | 122.14016 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 92 | 6.964448 | 122.139866 | 0.07 | 0 | 0.07 | Not Defined | 5 -Year | |
| 93 | 6.963469 | 122.141059 | 0.3 | 0 | 0.3 | Not Defined | 5 -Year | |
| 94 | 6.967778 | 122.145041 | 0.56 | 0 | 0.56 | Not Defined | 5 -Year | |
| 95 | 6.965845 | 122.14422 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 96 | 6.964424 | 122.144334 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 97 | 6.964484 | 122.145935 | 0.26 | 0 | 0.26 | Not Defined | 5 -Year | |
| 98 | 6.96575 | 122.145511 | 0.66 | 0 | 0.66 | Not Defined | 5 -Year | |
| 99 | 6.967131 | 122.145999 | 0.53 | 0 | 0.53 | Not Defined | 5 -Year | |
| 100 | 6.971625 | 122.146374 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 101 | 6.94163 | 122.138121 | 0.12 | 0 | 0.12 | Not Defined | 5 -Year | |
| 102 | 6.942931 | 122.136408 | 0.2 | 0 | 0.2 | Not Defined | 5 -Year | |
| 103 | 6.968223 | 122.139693 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 104 | 6.972438 | 122.142737 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 105 | 6.965251 | 122.141832 | 0.08 | 0 | 0.08 | Not Defined | 5 -Year | |
| 106 | 6.996449 | 122.118734 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 107 | 6.989367 | 122.122751 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 108 | 6.986279 | 122.122634 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 109 | 6.94912 | 122.155436 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 110 | 6.946171 | 122.15846 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 111 | 6.948526 | 122.157406 | 0.44 | 0 | 0.44 | Not Defined | 5 -Year | |
| 112 | 6.983564 | 122.133331 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 113 | 6.984256 | 122.130329 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 114 | 6.933099 | 122.138495 | 0.05 | 0.3 | -0.25 | 11-11-2013 | 5 -Year | |
| 115 | 6.932495 | 122.138721 | 0.2 | 0.5 | -0.3 | 30-11-2013 | 5 -Year | |
| 116 | 6.9325 | 122.138608 | 0.24 | 0.1 | 0.14 | 30-11-2013 | 5 -Year | |
| 117 | 6.978198 | 122.145875 | 0.04 | 0 | 0.04 | Not Defined | 5 -Year | |
| 118 | 6.982306 | 122.138333 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 119 | 6.997796 | 122.11279 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 120 | 6.9948 | 122.113754 | 0.08 | 0 | 0.08 | Not Defined | 5 -Year | |
| 121 | 6.950482 | 122.129556 | 0.06 | 0 | 0.06 | Not Defined | 5 -Year | |
| 122 | 6.950052 | 122.131003 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 123 | 6.952973 | 122.129661 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 124 | 6.952719 | 122.131538 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 125 | 6.953282 | 122.132497 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 126 | 6.951705 | 122.131995 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 127 | 7.001533 | 122.11137 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 128 | 6.994564 | 122.109631 | 0.04 | 0 | 0.04 | Not Defined | 5 -Year | |
| 129 | 6.997674 | 122.108713 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 130 | 6.955529 | 122.158841 | 0.19 | 0 | 0.19 | Not Defined | 5 -Year | |
| 131 | 6.958985 | 122.158215 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 132 | 6.964046 | 122.158299 | 1.03 | 0 | 1.03 | Not Defined | 5 -Year | |
| 133 | 6.979925 | 122.134648 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 134 | 6.979183 | 122.133613 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |

| Point Number | Validation Coordinates | | Model Var (m) | Validation Points (m) | Error | Event/Date | Rain Return / Scenario | |
|-----------------|------------------------|------------|------------------|--------------------------|-------|---------------------------|---------------------------|--|
| | Lat | Long | | | | | | |
| 135 | 6.979485 | 122.127717 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 136 | 6.980868 | 122.126401 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 137 | 6.983293 | 122.124213 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 138 | 6.967503 | 122.136075 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 139 | 6.971353 | 122.137853 | 5.51 | 1 | 4.51 | Not Defined | 5 -Year | |
| 140 | 6.955852 | 122.131395 | 0 | 0.3 | -0.3 | Not Defined | 5 -Year | |
| 141 | 6.966973 | 122.138063 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 142 | 6.965798 | 122.135711 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 143 | 6.965036 | 122.136111 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 144 | 6.958537 | 122.146235 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 145 | 6.958625 | 122.146771 | 0.06 | 0 | 0.06 | Not Defined | 5 -Year | |
| 146 | 6.980178 | 122.130518 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 147 | 6.982058 | 122.131628 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 148 | 6.973729 | 122.145516 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 149 | 6.973954 | 122.146803 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 150 | 6.973325 | 122.143263 | 0.16 | 0 | 0.16 | Not Defined | 5 -Year | |
| 151 | 6.974004 | 122.142061 | 0.1 | 0 | 0.1 | Not Defined | 5 -Year | |
| 152 | 6.976519 | 122.141733 | 0.06 | 0 | 0.06 | Not Defined | 5 -Year | |
| 153 | 6.978902 | 122.140837 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 154 | 6.974436 | 122.141442 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 155 | 6.962057 | 122.137346 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 156 | 6.962605 | 122.140661 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 157 | 6.959574 | 122.137314 | 0.05 | 0 | 0.05 | Not Defined | 5 -Year | |
| 158 | 6.961916 | 122.134126 | 0.2 | 0 | 0.2 | Not Defined | 5 -Year | |
| 159 | 6.971787 | 122.141462 | 0.37 | 0 | 0.37 | Not Defined | 5 -Year | |
| 160 | 6.970341 | 122.140569 | 0.51 | 0 | 0.51 | Not Defined | 5 -Year | |
| 161 | 6.971906 | 122.140463 | 0.5 | 0 | 0.5 | Not Defined | 5 -Year | |
| 162 | 6.963814 | 122.136105 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 163 | 6.942524 | 122.133858 | 0.06 | 0 | 0.06 | Not Defined | 5 -Year | |
| 164 | 6.969298 | 122.14762 | 0.14 | 0 | 0.14 | Not Defined | 5 -Year | |
| 165 | 6.968217 | 122.139697 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 166 | 6.972709 | 122.147659 | 0.11 | 0 | 0.11 | Not Defined | 5 -Year | |
| 167 | 6.940994 | 122.135066 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 168 | 6.94293 | 122.136413 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 169 | 6.972387 | 122.139033 | 0.76 | 0 | 0.76 | Not Defined | 5 -Year | |
| 170 | 6.974624 | 122.138792 | 0.08 | 0 | 0.08 | Not Defined | 5 -Year | |
| 171 | 6.975167 | 122.140635 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 172 | 6.973312 | 122.140772 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 173 | 6.93899 | 122.135254 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 174 | 6.938003 | 122.135391 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 175 | 6.961319 | 122.135267 | 0.03 | 0 | 0.03 | Not Defined | 5 -Year | |
| 176 | 6.993646 | 122.115714 | 1.14 | 1.2 | -0.06 | Not Defined | 5 -Year | |
| 177 | 6.991944 | 122.117007 | 1.78 | 1.2 | 0.58 | Not Defined | 5 -Year | |
| 178 | 6.94236 | 122.136286 | 0.09 | 0.7 | -0.61 | Not Defined | 5 -Year | |
| 179 | 6.932817 | 122.138572 | 0.3 | 0.4 | -0.1 | Ruby/ December 06,2014 | 5 -Year | |

| Point | Validation Coordinates | | Model | Validation | Error | Event/Date | Rain Return / | |
|--------|------------------------|------------|---------|------------|-------|---------------------------|---------------|--|
| Number | Lat | Long | Var (m) | Points (m) | LIIO | Lvent/Date | Scenario | |
| 180 | 6.978675 | 122.134152 | 1.51 | 0.3 | 1.21 | Ruby/ December 06,2014 | 5 -Year | |
| 181 | 6.977465 | 122.144019 | 0.45 | 0.3 | 0.15 | Ruby/ December 06,2014 | 5 -Year | |
| 182 | 6.979123 | 122.14496 | 0.7 | 0.2 | 0.5 | Ruby/ December 06,2014 | 5 -Year | |
| 183 | 6.934351 | 122.139277 | 0.03 | 0 | 0.03 | Ruby/ December 06,2014 | 5 -Year | |
| 184 | 6.933169 | 122.139119 | 0.54 | 0 | 0.54 | Ruby/ December 06,2014 | 5 -Year | |
| 185 | 6.9368 | 122.135257 | 0.04 | 0 | 0.04 | Ruby/ December 06,2014 | 5 -Year | |
| 186 | 6.964494 | 122.139094 | 0.93 | 0 | 0.93 | Ruby/ December 06,2014 | 5 -Year | |
| 187 | 6.978336 | 122.137671 | 2.18 | 0 | 2.18 | Ruby/ December 06,2014 | 5 -Year | |
| 188 | 6.953255 | 122.158881 | 0.81 | 0 | 0.81 | Ruby/ December 06,2014 | 5 -Year | |
| 189 | 6.950491 | 122.159461 | 0.03 | 0 | 0.03 | Ruby/ December 06,2014 | 5 -Year | |
| 190 | 6.938185 | 122.144237 | 0.14 | 0 | 0.14 | Ruby/ December 06,2014 | 5 -Year | |
| | | | | RMSE | 0.48 | | | |

Annex 12. Educational Institutions Affected in Mercedes Floodplain

| Zamboanga City | | | | | | | |
|----------------|-------------------------------------|-------------------|---------|----------|--|--|--|
| Derengeu | Puilding Name | Rainfall Scenario | | | | | |
| Багапдау | Building Name | 5-year | 25-year | 100-year | | | |
| Lumbangan | Salaan Elementary School | None | None | None | | | |
| Mampang | Arena Blanco East Elementary School | None | None | None | | | |
| Mampang | Arena Blanco National High School | None | None | None | | | |
| Mampang | Arena Blanco West Elementary School | None | None | None | | | |
| Mercedes | Mercedes Central School | None | Low | Low | | | |
| Mercedes | Mercedes National High School | Low | Low | Low | | | |
| Mercedes | MERCEDES SCHOOL | None | None | None | | | |
| Pasobolong | Culianan Learning Center | None | None | None | | | |
| Pasobolong | Culianan National High School | None | None | Low | | | |
| Salaan | Buenakapok Elementary School | None | None | None | | | |
| Salaan | Pasobolong Elementary School | None | None | None | | | |
| Salaan | Salaan Elementary School | None | None | None | | | |
| Tugbungan | Arena Blanco National High School | None | None | None | | | |
| Zambowood | Zambowood Elementary School | None | None | None | | | |

Table A-12.1 Educational Institutions Affected in Mercedes Floodplain

Annex 13. Medical Institutions Affected in Mercedes Floodplain

| Zamboanga City | | | | | | | | |
|----------------|---|-------------------|---------|----------|--|--|--|--|
| D | Duilding Name | Rainfall Scenario | | | | | | |
| Barangay | | 5-year | 25-year | 100-year | | | | |
| Lumayang | Salaan Health Center | None | None | None | | | | |
| Mercedes | Mercedes Health Center | None | None | None | | | | |
| Pasobolong | Culianan Health Center | None | None | None | | | | |
| Salaan | LANZONES HEALTH CENTER | None | None | None | | | | |
| Salaan | Mancao Medical Clinic | None | None | None | | | | |
| Salaan | Minadanao Central Sanitarium General Hospital | None | None | None | | | | |
| Salaan | Pasobolong Health Center | None | None | None | | | | |

Table A-13.1 Medical Institutions Affected in Mercedes Floodplain